

USARTL-TR-77-53

FOR FURTHER TRAN

REMOTELY PILOTED VEHICLE (RPV)
STRUCTURAL COMPONENTS INVESTIGATION

Sam Yao, Dale P. Abildskov
FIBER SCIENCE, INC.
245 E. 157th Street
Gardena, Calif. 90248

THIS DOCUMENT IS BEST QUALITY FRACTICABLE.
THE COPY FURNISHED TO DDC CONTAINED A
SIGNIFICANT NUMBER OF PAGES WHICH DO NOT
REPRODUCE LEGIBLY.

February 1978

Final Report for Period June 1976 - May 1977

DDC FILE COPY

 ∞

Approved for public release; distribution unlimited.



78 06 08

8 036

Prepared for

APPLIED TECHNOLOGY LABORATORY

U. S. ARMY RESEARCH AND TECHNOLOGY LABORATORIES (AVRADCOM)

Fort Eustis, Va. 23604

APPLIED TECHNOLOGY LABORATORY POSITION STATEMENT

This report provides a reasonable insight into the advantages of the use of Spacewind for lightly loaded structures. The lack of fatigue test data, however, precludes the painting of a complete picture of the properties of Spacewind. Results of this contract are being integrated with other R&D efforts at the Applied Technology Laboratory to provide a comprehensive approach to the R&D required for development of future Army RPV aircraft systems.

Edward H. Dean, Structures Technical Area, Technology Applications Division, served as project engineer for this effort.

DISCLAIMERS

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

When Government drawings, specifications, or other data are used for any purpose other than in connection with a definitely related Government procurement operation, the United States Government thereby incurs no responsibility nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission, to manufacture, use, or sell any patented invention that may in any way be related thereto.

Trade names cited in this report do not constitute an official endorsement or approval of the use of such commercial hardware or software.

DISPOSITION INSTRUCTIONS

Destroy this report when no longer needed. Do not return it to the originator.

DISCLAIMER NOTICE

THIS DOCUMENT IS BEST QUALITY PRACTICABLE. THE COPY FURNISHED TO DDC CONTAINED A SIGNIFICANT NUMBER OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.

UNCLASSIFIED SECURITY CHASSIFICATION OF THIS PAGE (When Date Entered) READ INSTRUCTIONS BEFORE COMPLETING FORM 19 REPORT DOCUMENTATION PAGE 3. RECIPIENT'S CATALOG NUMBER 2. GOVT ACCESSION NO. USARTLHTR-77-53 TITLE (and Subtitle) ERIOD COVERED Final rept REMOTELY PILOTED VEHICLE (RPV) STRUCTURAL COMPONENTS INVESTIGATION Jun 76- May 277 CONTRACT OR GRANT NUMBER(s) Sam/Yao DAAJ02-76-C-0040 15 Dale P/Abildskov 9. PERFORMING ORGANIZATION NAME AND ADDRESS Fiber Science, Inc. 62209A 1F262209AH76 245 E. 157th Street 00 176 EK Gardena, CA 90248 11. CONTROLLING OFFICE NAME AND ADDRESS Feb Applied Technology Laboratory, U.S. Army Research and Technology Laboratories (AVRADCOM) 79 Fort Eustis, VA 23604 14. MONITORING ACENCY NAME & ADDRESS(II different from Controlling Office) 15. SECURITY CLASS. (of this to Unclassified 154. DECLASSIFICATION DOWN GRADING 16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited. 17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, If different from Report) 18. SUPPLEMENTARY NOTES 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Spacewind Structures RPV Structure Open-Weave Structure Filament-Wound Structure

ABSTRACT (Continue on reverse side if necessary and identify by block number)

The mechanical properties of the open-weave filament-wound material called "Spacewind" were evaluated both analytically and experimentally.

As a demonstration of the feasibility of using Spacewind, the body and wing for the AQUILA remotely piloted vehicle were designed, fabricated, tested, and proven successful.

DD 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

388 573

PM

SUMMARY

The mechanical properties of Spacewind, an open-weave filament-wound material, were evaluated both analytically and experimentally.

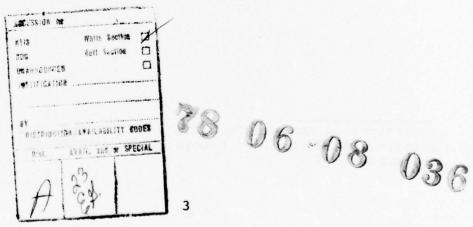
A computer program was developed for calculating the composite properties of a spacewind laminate based on the fiber and resin properties, fiber orientation, and fiber coverage ratio. The calculated values agree quite well with experimental values for graphite. However, poor correlation was found with S-glass and Kevlar 49. The test specimens failed in buckling, which accounts for the difference between calculated and measured strengths.

The test specimens were sandwich wall flexural panels having either Nomex honeycomb or PVC foam core material, and tubular tensile specimens. The sandwich wall panels were tested in flexure and for impact (ball drop).

The PVC foam core specimens were found to have higher impact resistance than the honeycomb and gave a much smoother surface. Graphite/epoxy faces proved to have much higher impact resistance than either glass or Kevlar 49.

Tubular tensile specimens, except for those made of graphite, were found to be unstable due to a lack of hoop strength and gave nonrealistic results.

As a demonstration of the feasibility of using Spacewind, the body and wing for the AQUILA remotely piloted vehicle were designed, fabricated, and tested. The body and wing sustained the ultimate design loads with no signs of failure. Spacewind filament-wound structural elements were proven to be practical. All of the objectives of the program were met.



PREFACE

This report was prepared by Fiber Science, Inc. in accordance with Contract DAAJ02-76-C-0040, issued by the Eustis Directorate, U.S. Army Air Mobility Research and Development Laboratory, Fort Eustis, Virginia*. Mr. Eddie Dean was the U.S. Army program technical monitor.

The activities reported herein cover the period from June 1976 to May 1977. The Fiber Science project engineer was Mr. Sam Yao

^{*}Redesignated Applied Technology Laboratory, U.S. Army Research and Technology Laboratories (AVRADCOM), 1 September 1977.

TABLE OF CONTENTS

	Page
Summary	3
Preface	4
List of Illustrations	6
List of Tables	7
Introduction	8
Material Property Studies	10
Test Result Analysis	18
Analytical Results	20
RPV Structural Component Design	30
Fabrication Development	38
Fabrication Sequence	39
RPV Structural Component Testing	42
RPV Structural Component Cost Analysis	44
Conclusions	46
Appendix A - Computer Program and Print Out	47

LIST OF ILLUSTRATIONS

Figure		Page
1	Flexural Test Specimen	10
2	Tensile Test Specimen	13
3	Thornel 300/Epoxy, Tensile Strength vs Winding Angle	21
4	Kevlar 49/Epoxy, Tensile Strength vs Winding Angle	22
5	S-Glass/Epoxy, Tensile Strength vs Winding Angle	23
6	Thornel 300/Epoxy, Modulus vs Winding Angle	24
7	Kevlar 49/Epoxy, Modulus vs Winding Angle	25
8	S-Glass/Epoxy, Modulus vs Winding Angle	26
9	Correlation of Calculated and Measured Flexural Strength for Glass	27
10	Correlation of Calculated and Measured Flexural Strength for Graphite	28
11	Correlation of Calculated and Measured Flexural Strength for Kevlar 49	29
12	Wing Geometry	31
13	Fuselage Geometry	32
14	Fuselage Attachment for Wing	34
15	Wing Attachment for Fuselage	35
16	Control Surface Attachments	36
17	Test Setup	43

LIST OF TABLES

<u>Table</u>		Page
1	Reinforcing Fibers	11
2	Flexural Specimen Configurations	12
3	Flexural Specimen Test Results	14
4	Tensile Specimen Configurations	15
5	Tensile Specimen Test Results	16
6	Impact Test Results	17

INTRODUCTION

This report is concerned with a filament winding technique developed by Fiber Science and called Spacewind. The name is descriptive -- spaces are left between filament wound strands. The final structure might have large spaces and appear to be made of a fish net. It might have smaller spaces and appear to be made of a loosely woven fabric.

Spacewind is suitable mainly for lightly loaded structures. It is intended to minimize weight by leaving out material. It also reduces strength in some nonlinear fashion as material is left out.

One purpose of this contract was to devise an analytical model of how strength changes as the Spacewind parameters of open spaces and winding angle change. Another purpose was to verify the analytical model by specimen testing. Both the analytical model and specimen tests were to be verified by fabricating the fuselage and one wing of an RPV model and then subjecting the model to dead weight loading.

Filament winding is a well-known process. However, it has developed a unique vocabulary that is not so well known. The few definitions that follow will clarify some of the later text.

Strand

A general term indicating an essentially continuous length of filamentary material, whether large or small, twisted or untwisted.

Band Width

A single strand might be wound or several strands might be gathered and wound at one time. Band width is the width of the total number of strands wound at one time.

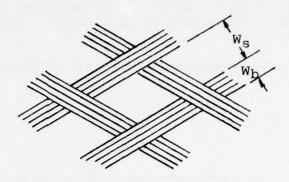
Winding Angle

Strands are wound onto a rotating mandrel by traversing from end to end of the mandrel. The angle between a strand and the mandrel axis is the winding angle. It is both + and - with reference to cartesian coordinates since the band direction changes.

F.C.R.

Fiber Coverage Ratio is the ratio of mandrel surface area covered with strands

going in one direction to the amount not covered, as sketched below.



$$F.C.R. = \frac{W_b}{W_b + W_s}$$

Fiber Volume

A second ratio, unrelated to F.C.R., is the ratio of fiber volume to the total volume of fiber and resin. It is typically given as a percentage rather than a ratio.

MATERIAL PROPERTY STUDIES

Mechanical properties of Spacewind panels and tubes were measured in order to verify analytical results. Sandwich panels using Spacewind faces and both honeycomb and PVC foam cores were tested in flexure. Spacewind tubes were tested in tension.

The flexural specimen size and configuration is shown in Figure 1.

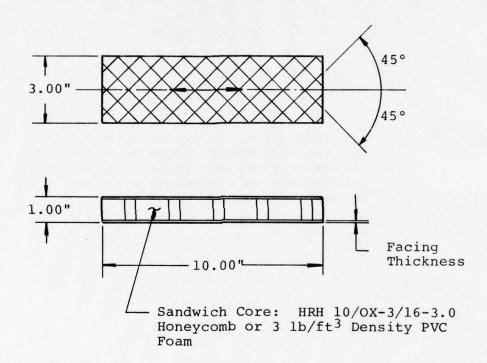


Figure 1. Flexural Test Specimen

Selected specimens had a half-inch-diameter hole drilled through both faces, exactly at the panel center, to give an evaluation of the effect of a cutout. The facing materials used are given in Table 1. The resin system was APCO 2434/APCO 2347 7.5 phr (Applied Plastics Company, El Segundo, California).

Table 1. Reinforcing Fibers

Fiber Description	Band Width (inch)*	Facing Thickness (inch)**
S-2 glass, 12 end roving	.65	.012
Kevlar 49, 1420 denier	.44	.012
Thornel 300, 3000 filament strand	. 44	.012

^{*100} percent coverage with 8 rovings

Core materials were either Nomex honeycomb (HRH 10/OX-3/16-3.0) or PVC foam, both at 3 lb/cu. ft. density. The honeycomb is over-expanded, giving a rectangular cell instead of hexagonal. Over-expanding permits bending in one direction.

Samples made are given in Table 2. Three specimens of each configuration were made and tested.

Panels were tested according to Federal Test Method Standard No. 406, Method 1032. Facing stresses were calculated by:

$$F = \frac{P_B a_B}{4t (d+t_c)b}$$

where F = facing stress

 P_B = total force, applied at 2 points located a distance of $a_B/4$ from each reaction

^{**50} percent fiber volume

Table 2. Flexural Specimen Configurations

Fiber/Core	Fiber Coverage	Without	With
Material	Ratio	Cutout	Cutout
Glass/Nomex	1.00	x	
Glass/Nomex	.75	х	
Glass/Nomex	.50	х	
Glass/Nomex	.25	x	
Glass/Nomex	.50		х
Kevlar 49/Nomex	1.00	х	
Kevlar 49/Nomex	.75	х	
Kevlar 49/Nomex	.50	х	
Kevlar 49/Nomex	.25	х	
Kevlar 49/Nomex	.50		Х
Kevlar 49/PVC Foam	.50	х	
Graphite/Nomex	1.00	х	
Graphite/Nomex	.75	х	
Graphite/Nomex	.50	х	
Graphite/Nomex	.25	х	
Graphite/Nomex	.50		Х
Graphite/PVC Foam	.50	х	
		MAN SEE	

a = span length

t = facing thickness

d = total sandwich thickness

t_c = core thickness

b = sandwich width

Results are given in Table 3.

Tensile strength and elongation at various winding angles was measured with a tubular specimen (Figure 2).

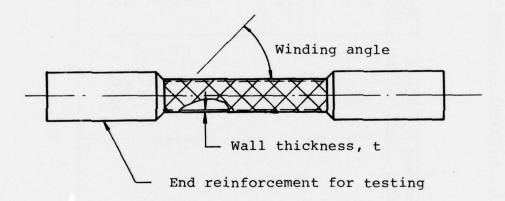


Figure 2. Tensile Test Specimen

The same fibers used for flexural panels were used for tensile specimens. Wall thicknesses were .014 inch for S-2 glass and .012 inch for Kevlar 49 and Thornel 300.

The samples made are given in Table 3. Three specimens of each configuration were made and tested.

Table 3. Flexural Specimen Test Results

Failure Mode	Q	D .06	45° C	45° C	0	D .06	Q				D .06		Δ	Ω	D .06	D .06		2 °06	
Failure Strain (In./In.)	.011	800.	600.	.007	.007	.004	.011	.010	800.	.007	.007	.010	600.	.011	600.	600.	.007	900.	
Modulus (106 PSI)	1.4	1.2	. 48	.34	.72	2.8	1.2	68.	.55	.34	.72	1.2	3.1	1.4	1.2	99.	1.1	2.1	
Stress (10 ³ PSI)	16.6	8.8	4.3	2.3	4.65	11.8	12.3	8.4	4.3	2.35	5.0	11.9	17.0	11.6	9.0	4.7	7.6	12.0	
Fiber Coverage Ratio	1.00	.75	•	.25		.50	1.00	•	•	•	.50		1.00	.62	.50	.25	.50	.50	
Construction	S-2 Glass/Nomex	S-2 Glass/Nomex	S-2 Glass/Nomex	S-2 Glass/Nomex	S-2 Glass/Nomex*	S-2 Glass/Foam	Kevlar 49/Nomex	Kevlar 49/Nomex	Kevlar 49/Nomex	Kevlar 49/Nomex	Kevlar 49/Nomex*	Kevlar 49/Foam	Graphite/Nomex	Graphite/Nomex	Graphite/Nomex	Graphite/Nomex	Graphite/Nomex*	Graphite/Foam	

Note:

C denotes Compression D denotes Delamination * with cutout in specimen

Table 4. Tensile Specimen Configurations

Fiber	Fiber Coverage	Fiber Angle
Material	Ratio	(Degrees)
S-2 Glass	1.00	20
	.25	20
	1.00	45
	.50	45
	.25	45
Kevlar 49	1.00	45
	.25	45
Thornel 300	1.00	45
	.25	45

Samples were tested according to Federal Test Method Standard No. 406, Method 1011, with one exception. The wall is supposed to be machined to 60 percent of the original wall thickness over a length of 2-1/4 inches to assure failure in the gage length. Spacewind samples are thicker at crossover points than between these points. Machining would hit only the crossovers and complicate the analysis.

Results are given in Table 5.

Inpact damage resistance was evaluated with a dropping ball test according to Federal Test Method Standard No. 406, Method 1074, with two exceptions: A 2.2-pound (2-1/2-inch diameter) steel ball was used instead of a .5-pound ball. The drop height was varied between 6 and 18 inches instead of 1 and 20 feet. The results, given in Table 6, are only comparative and do not have a design value.

Table 5. Tensile Specimen Test Results

Failure Mode	Shear	Shear	Shear	Shear	Shear	Shear	Shear	Tensile			
Failure Strain (In./In.)	.028	.10	.045	.030	.11	.030	.057	.025			
Modulus (106 PSI)	3.0	.95	1.5	.41	.21	.95	.179	1.5			
Ratio Stress (PSI)	87,500	53,300	22,500	15,400	5,200	16,000	7,500	20,000	Could	Test	
Ratio	1.00	.25	1.00	.50	.25	1.00	.25	1.00	.25		
Fiber	Glass	Glass	Glass	Glass	Glass	Kevlar	Kevlar	Graphite 1.00	Graphite .25		
Angle (Deg)	20	20	45	45	45	45	45	45	45		

Table 6. Impact Test Results

ht (In.)	18	1" fracture	Delam., 5" fracture in 3 directions	Dent, 2" fracture in 2 directions	Dent, delam., skin to edges	Dent, delam., small fractures	8" delam.	Dent, small delam. opposite side	
Drop Height (In.	12	No damage	3" fracture, delam.	Dent	Dent, delam., 6" fracture	Dent, delam.	6" delam.	Larger dent	
	9	No damage	No damage	Small dent	No damage	Small Dent	No damage	Small dent	
	Construction	S-2 glass, 1.00 coverage with honeycomb	S-2 glass, .50 coverage with honeycomb	S-2 glass, .50 coverage with foam	Kevlar, .50 coverage with honeycomb	Kevlar, .50 coverage with foam	Graphite, .50 coverage with honeycomb	Graphite, .50 coverage with foam	

TEST RESULT ANALYSIS

Flexural test results are given in Table 3. Samples with foam cores were two to three times stronger than those with honeycomb cores. All samples except those at 1.00 ratio coverage (plus .62 for graphite) failed by skin buckling. The foam core gives 100% support to the windings to prevent buckling, whereas honeycomb gives much less support because it provides much less bonding surface. Foam core is preferred over honeycomb for this reason. It is also preferred for manufacturing convenience, as will be discussed later.

Cutouts had no effect on strength except possibly with graphite. The reason why graphite might respond to a cutout is not clear. Very probably there is no real difference between any of the cutout and plain panel pairs for statistical reasons. It is not unusual for the standard deviation to equal 20 percent of an average composed of only three test results. This point cannot be verified because of the few samples tested. Any future program should include samples for a statistical base line.

Tensile test results are given in Table 5. The samples were to be composed of only wound strands without any facing sheet or core material. The result was to fail all samples except 1.00 ratio coverage graphite in shear.

Flexural samples failed because of a face buckling instability. Tensile samples failed because of what might be called a lateral support instability. Since lateral support instability is not a recognized engineering term, it needs some explanation: The tubular tensile specimens are supported internally in the grip areas during test. The gage length has no support at all. The specimen wants to neck down as it is stretched, just as a scissors jack gets narrower as it goes higher. The winding angle changes as the specimen necks down, but the only restraint is the resin between strands. Resin shear strength is the lowest of all mechanical properties of composites. Specimens failed at a very low strength because only resin is being loaded.

If lateral support is given, for example by adding a core substrate or by winding a thick wall at 1.00 ratio coverage, the failure mechanism becomes tension rather than resin shear. Samples with a foam core to prevent lateral instability should be included in any future program.

Impact damage normally is measured by some type of pendulum device, such as an Izod test. Spacewind is not suitable for Izod testing because only the crossover points would be hit and the actual force would be much greater than the programmed force. A standard dropping ball test was used for this reason. Results are given in Table 6, page 17.

Foam core again gives more support than honeycomb core and is preferred. Delamination size is only a rough gage of impact damage.

ANALYTICAL RESULTS

A computer program was written to predict Spacewind mechanical properties. It is presented in Appendix A. The program assumed a failure mode of tension or compression. Test samples failed because of an instability, which indicates that the program should be valid only for stiffness, Poisson's ratio and coefficient of thermal expansion.

Figures 3 through 8 give calculated strength and stiffness of S-glass, Kevlar 49 and Thornel 300 Spacewind as a function of winding angle and fiber coverage ratio. Figures 9, 10 and 11 give correlations between calculated and measured results for flexural strength.

Graphite correlation is quite good, indicating that buckling failure of specimens occurred only very shortly before a tension or compression failure would have occurred.

Glass correlation is poor. All samples failed by buckling because of the low glass modulus, resulting in premature failures. Buckling is a function only of bond strength to the core. Plain winding resin was used as the adhesive for these samples. A better adhesive might delay buckling enough to improve correlation.

Kevlar correlates poorly also, in spite of its high tensile modulus. Tensile and compressive modulus normally are the same for fibers, but Kevlar is an exception. Relatively low compressive loads will cause Kevlar to split axially, leaving two or more filament fractions bunched together. Buckling failure follows immediately. Kevlar is demonstrating this splitting, or fibrilation, in the flexural buckling observed in test panels. However, the fiber compressive strength used to predict the composite properties appears to be too low.

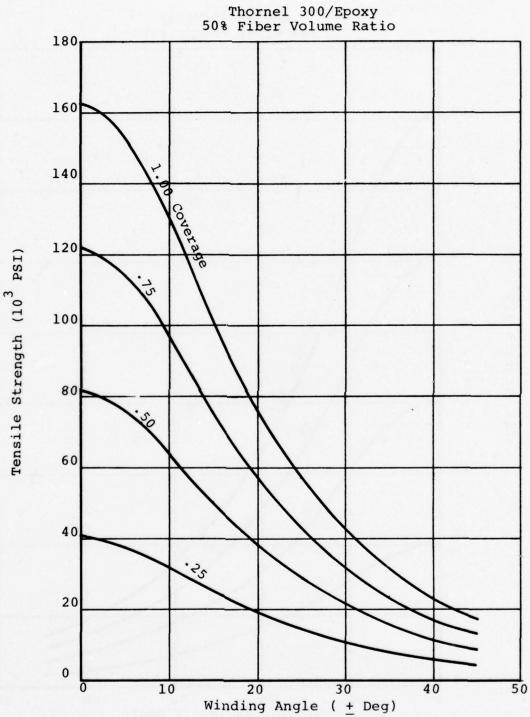


Figure 3. Thornel 300/Epoxy, Tensile Strength vs Winding Angle

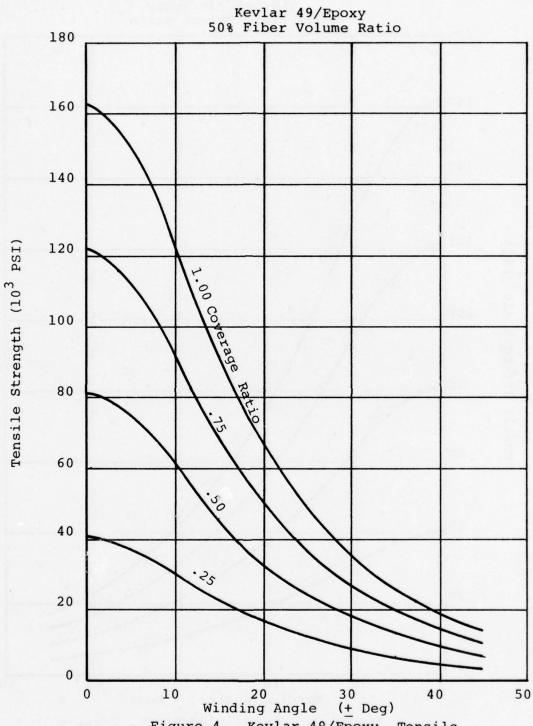
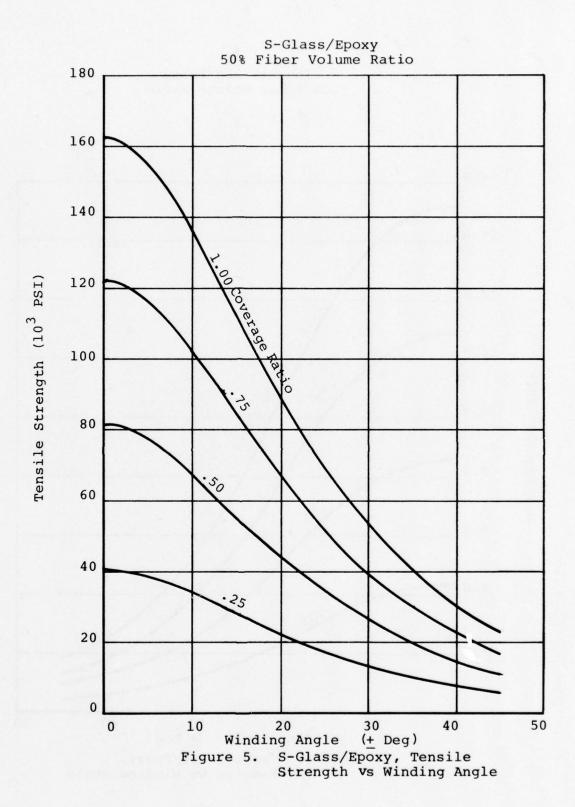


Figure 4. Kevlar 49/Epoxy, Tensile Strength vs Winding Angle



Thornel 300/Epoxy 50% Fiber Volume Ratio

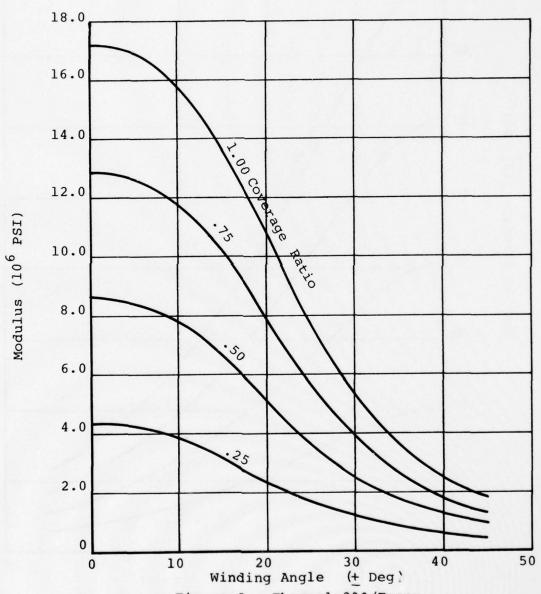


Figure 6. Thornel 300/Epoxy, Modulus vs Winding Angle

Kevlar 49/Epoxy 50% Fiber Volume Ratio

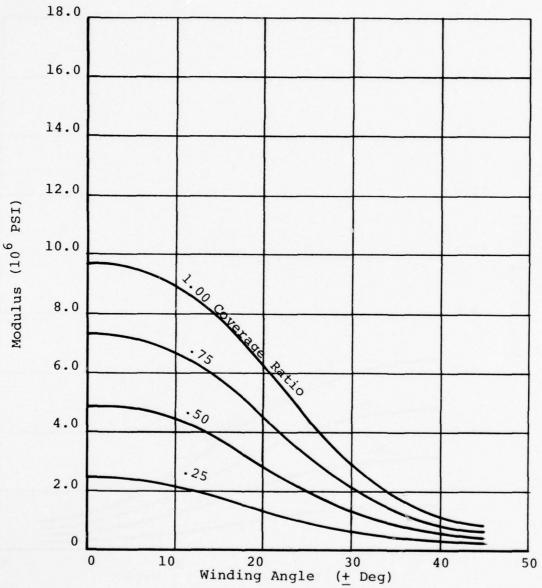


Figure 7. Kevlar 49/Epoxy, Modulus vs Winding Angle

S-Glass/Epoxy 50% Fiber Volume Ratio

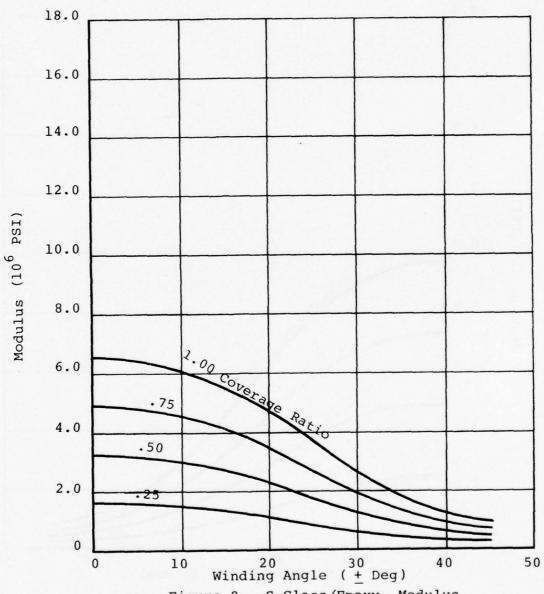


Figure 8. S-Glass/Epoxy, Modulus vs Winding Angle

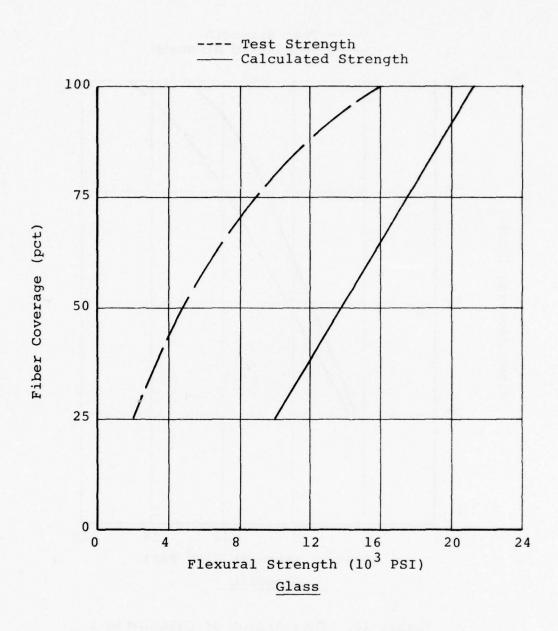
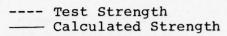


Figure 9. Correlation of Calculated & Measured Flexural Strength for Glass



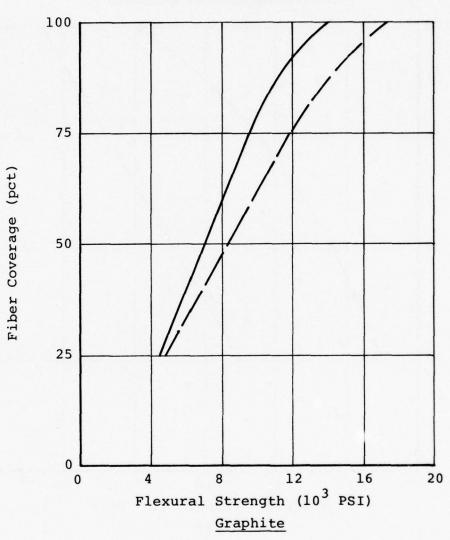


Figure 10. Correlation of Calculated & Measured Flexural Strength for Graphite

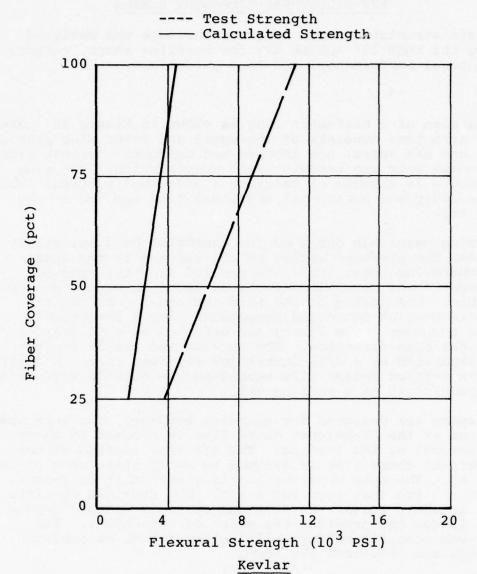


Figure 11. Correlation of Calculated & Measured Flexural Strength for Kevlar

RPV STRUCTURAL COMPONENT DESIGN

A basic structure of the wing and fuselage was designed using the XMQM-105 AQUILA RPV for baseline shape, weight, structural performance, and cost guidelines.

Wing

The design of a half-span wing is shown in Figure 12. The wing structure consists of the upper and lower wing panels, fore and aft spars, and inboard and outboard closeout ribs. All components are sandwich wall construction. The wing structure is capable of carrying a 350-pound vertical load and a 200-pound horizontal retrieval load applied at the wing tip.

The wing panel was designed for chordwise bending, mainly to beam the pressure acting on the surface to the spar. The chordwise shear loads are carried from the sandwich facings to the metallic attachment spool through a bonded surface. The facing of the sandwich panel consists of .014-inch-thick Spacewind broadgoods with a 25-percent fiber coverage. The fibers are oriented at + 60 degrees from the span direction. The outside and inside facings are separated by a 3/16-inch-thick PVC foam core. A sheet of 1-mil-thick Tedlar film bonded on the outside surface of the panel acts as a surface veil.

The spars are designed for spanwise bending. The fore spar located at the 25-percent chord line is assumed to carry 100-percent of the loading. The aft spar located at the 70-percent chord line is assumed to carry 50-percent of the loading. The spar construction is essentially an I-beam. There are two spar caps and a web. The spar cap consists of a graphite longo. An aluminum spool is wrapped around with longos and provides the point of attachment. The spar web consists of Style 1581 glass fabric as sandwich facings and 3/16-inch PVC foam.

The closeout rib consists of glass fabric sandwich facings and PVC foam core.

Fuselage

The design of the fuselage is shown in Figure 13. The structure consists of a shell and two main bulkheads. The shell consists of graphite/epoxy facings and 3/16-inchthick PVC foam core. The sandwich facing is Spacewind

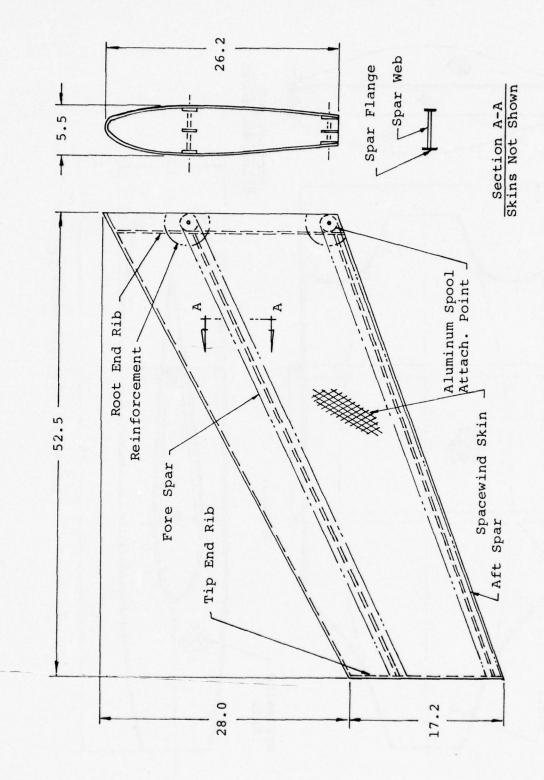
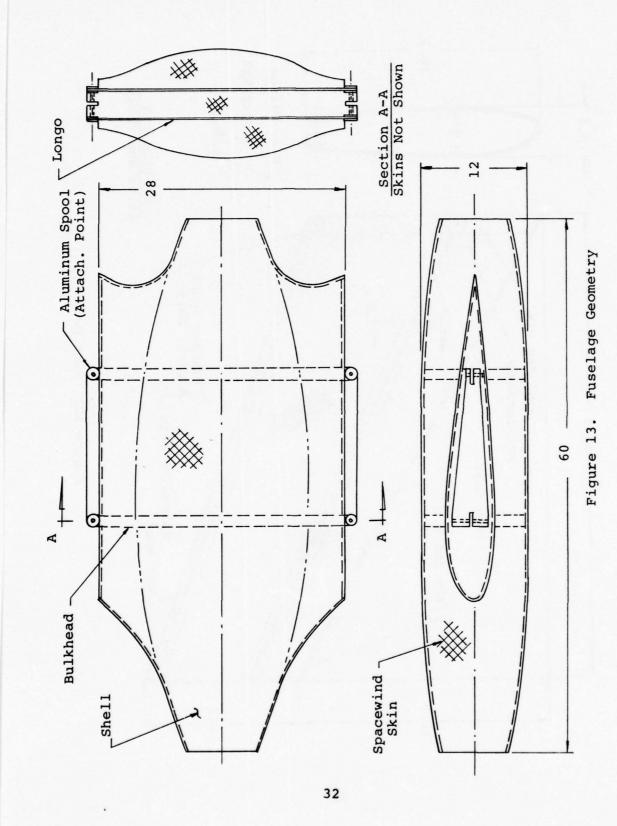


Figure 12. Wing Geometry



.014-inch-thick broadgoods with a 25-percent fiber coverage. The fibers are oriented at + 45 degrees from the body axis. A sheet of Style 104 glass fabric is laminated on the outside of the shell as a surface veil.

The bulkheads are designed to carry the wing bending moment. The bulkhead consists of Spacewind graphite/epoxy facings and 3/4-inch-thick Spacewind broadgoods with 25-percent fiber coverage. The fibers are oriented at + 45 degrees from the spanwise axis. Aluminum attachment spools at the upper and lower corners of both ends are wrapped with graphite longos. The longos tie the spool at one side to the spool at the other side of the fuselage to form a continuous beam element.

There is an end rib on the stub wing of each side of the fuselage. The rib is designed to distribute the fore and aft loads to the fuselage. Also, the rib is used as a link to tie the fore and aft bulkheads together at the attachment points to resist the loads in the chordwise direction.

The accessory mounting structure consists of partial bulk-heads and intercostals. A shelf on the top of the structure provides the support for the accessory package.

The cutout and holes in Spacewind structures do not pose significant design problems. The opening is normally reinforced to carry the load.

Attachments

The wing to fuselage attachment was actually fabricated. Other attachments, such as payload, engine mount and control surfaces, were not fabricated. However, all attachments are based on one of three principles:

- 1. Use longos wrapped around spools.
- Use a metal plate with attached bracket bonded to a vehicle surface.
- 3. Use a composite bulkhead bonded inside the fuselage.

The first attachment concept was used to join the wing and fuselage. The fuselage connection is made with graphite longitudinal (longo) fibers wrapped at two places on a set of aluminum spools as sketched in Figure 14.

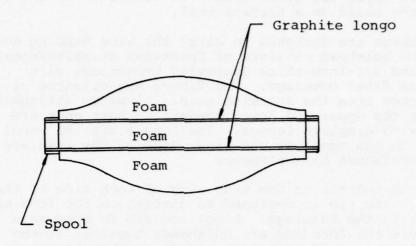


Figure 14. Fuselage Attachment for Wing

PVC foam is filled between the longos and on top and bottom as sketched and then Spacewind face sheets are bonded on. This assembly is a frame which is bonded inside the fuselage with the spools exposed on either side of the wing stub.

The wing matching joint is made by wrapping longos around a set of spools matched to the fuselage. Dummy spools are used at the wing tip end for winding, but then are cut off. The longos are bonded to the top and bottom inside skins as sketched in Figure 15.

Flanges on a wing spool go over the top of the mating fuselage spool and a single 1/4-inch bolt joins the two. In this manner, a load applied to one wing transfers to the opposite wing. Counter-acting loads, as normally would be experienced, are taken in tension and compression by the longos and transferred by shear through the fuselage bulkhead bond and longo bonds to the wings.

The payload attachment is a shelf made of foam core and

Spacewind faces, bonded horizontally at the proper nose position. The camera is bolted to this shelf and shoots through a hole cut in the shelf.

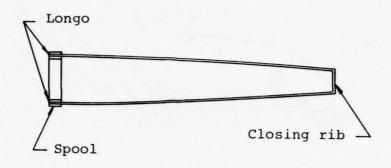


Figure 15. Wing Attachment for Fuselage

The engine mount is a similar shelf, this time called a fire wall, bonded vertically in the proper aft location. Mounting holes would have to be reinforced with a solid insert in the wall.

Control surfaces are simple elevons, pivoting at two places. Both places can utilize metal brackets which bond between the outer skin and core as sketched in Figure 16.

All attachments are designed the same as for standard composites.

Fatigue

Fatigue tests were not performed as part of this contract. However, previous experience with materials used in this contract indicates that fatigue life should be good and similar to conventional composites.

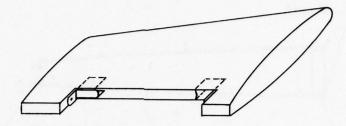


Figure 16. Control Surface Attachments

Damage Tolerance

Impact testing of panels with and without 1/2-inch-diameter holes indicates the hole has little or no effect. One can assume that ballistic damage would approximate this size hole and also have little or no effect.

Environmental Extremes

Environmental testing was not performed as part of this contract. Prior experience with the materials used indicate the normally assumed environmental conditions for aircraft, such as -50°F to +140°F temperature capability, can be met. It might be important to seal out moisture by using a Tedlar surface veil on both sides of the sandwich wall.

Weight

A weight analysis of a half-span wing was performed. The weight is 3.82 pounds. The weight breakdown is as follows:

<u>Item</u>	Material	Weight (lb)
Surface veil	Tedlar film	.12
Wing panel - skins - core - filler	Graphite/epoxy PVC foam Syntactic foam	.60 .80 .10
Longo spools	Aluminum	.20
Forward spar - caps - web	Graphite/epoxy Glass fabric-PVC foam	.30
Aft spar - caps - web	Graphite/epoxy Glass fabric-PVC foam	.18
Corner ties	Glass/epoxy	.62
Ribs	Glass fabric-PVC foam	.12
Bond liner	Ероху	$\frac{.12}{3.82}$

FABRICATION DEVELOPMENT

A model RPV fuselage and one wing were designed and fabricated to demonstrate techniques and feasibility. Design details are given on pages 30 through 37.

The procedure for all fabrication is to wind onto a cylindrical mandrel whatever coverage ratio and winding angle is needed. The mandrel is covered with a sheet of plastic. The winding and plastic sheet are cut axially and removed from the mandrel. The plastic sheet acts as a carrier and is removed after the Spacewind sheet is laminated into a mold.

Initial samples made as described above had quite a rough exterior surface because of the Spacewind configuration. The model was made with an exterior layer of 1-mil-thick bondable Tedlar film to give a good surface. It also gave better resin filleting at Spacewind crossover points.

Style 104 glass cloth was also evaluated as an outside surfacing material. It is better than Tedlar in that it will conform more readily to extreme changes in contour. However, it is also heavier and should be used only when Tedlar cannot conform to the desired contour.

Both honeycomb and PVC foam core materials were evaluated. Over expanded honeycomb will bend in one direction but not two. Extensive slitting and patching is necessary to fit it over compound contours. PVC foam can be thermally formed to most contours and is preferred for this reason. Structural reasons mentioned earlier also give a preference to foam over honeycomb.

A detailed fabrication sequence is given in the following section.

FABRICATION SEQUENCE

The basic structure of a left wing and fuselage of the AQUILA RPV was fabricated to the Spacewind specifications. The fabrication procedures were as follows:

Wing Panel

- 1. Prepare mold surface for bonding.
- 2. Apply a 1-mil-thick bondable Tedlar film on the mold half. Draw a vacuum between the film and the mold surface. Rub out wrinkles and remove the trapped air.
- 3. Laminate a Spacewind outside skin on top of the Tedlar film with the skin carrier film facing up. Work the spacewind skin to conform to the mold surface. Remove the skin carrier film.
- 4. Install the pre-formed PVC foam core.
- 5. Laminate the Spacewind inside skin on top of the foam core with skin carrier film facing up. Work spacewind skin to conform to the shape.
- 6. Apply a vacuum bag. Draw a vacuum and rub out.
- 7. Cure.
- 8. Remove vacuum bag and the inside skin carrier film.
- 9. Trim to size.

Fuselage Shell

Repeat steps to fabricate wing panels, except replace Tedlar film with one ply of Style 104 E-glass fabric/epoxy laid into the mold wet and rubbed out as a contact layup.

Fuselage Bulkhead, Spar Web and Rib

- Apply a release film on the surface table. Draw a vacuum and rub out the wrinkles.
- 2. Laminate the sandwich facing on the release film.
- 3. Install the sandwich core.

- 4. Laminate the sandwich facing.
- Apply a vacuum bag. Draw a vacuum and rub out the wrinkles.
- 6. Cure.
- 7. Remove the vacuum bag and release film.
- 8. Trim to size.

Spar Longo

- 1. Prepare the aluminum spools for bonding.
- 2. Rig the aluminum spools in the winding fixture.
- 3. Wind longos around the grooves of the aluminum spools.
- 4. Remove the winding from the fixture.
- 5. Cut the longo to length.
- 6. Install the longo to the inside surface of the wing panel while it is supported on the wing mold. Align the spool and the longo per the drawing location.
- 7. Apply a vacuum bag and rub out.
- 8. Cure.
- 9. Remove the vacuum bag.

Bulkhead Longo

- 1. Prepare the aluminum spools for bonding.
- 2. Rig up the spools on the bulkhead.
- 3. Wind the longo around the groove of the spool.
- 4. Apply the vacuum bag and rub out.
- 5. Cure.
- 6. Remove the vacuum bag.

Wing Assembly

- 1. Place the lower wing panel on the mold.
- Apply adhesive to all the bonding surfaces -- leading and trailing edges, fore and aft spar web locations.
- Apply the adhesive to the upper and lower edges of the spar webs.
- 4. Install the spar webs to the lower wing panel.
- 5. Install the upper wing panel. Use weights to hold the wing panel down.
- 6. Cure.
- 7. Apply a cap ply to the leading edge split line.
- 8. Install inboard and outboard ribs.
- 9. Cure.

Fuselage Assembly

- 1. Place the lower shell in the mold.
- Apply adhesive to all the bonding surfaces -- edges of shell, fore and aft bulkhead locations.
- Apply adhesive to the upper and lower edges of the bulkheads.
- 4. Install the bulkheads in the lower shell.
- Install the upper shell. Use weights to hold the shelf half in place.
- 6. Cure.
- 7. Bond end ribs on both sides.
- 8. Final cure.

RPV STRUCTURAL COMPONENT TESTING

The Spacewind fuselage and wing assembly successfully passed the structural test of 700 pounds total wing load without any sign of failure. The test was set up as depicted in Figure 17. Loading was accomplished using 25-pound bags of lead shot placed on the upper surface of the left wing and the simulated right wing. The wings were loaded simultaneously and symetrically by placing weights uniformly spaced along the 25-percent chord of both wings. 350-pound loads were applied to each wing. The deflection of the wing tip was 1.03 inches under full load.

Thumb pressure tests on the wing surface and fuselage shell were conducted. The wing surface was found to be much stiffer than that of the existing AQUILA wing. No comparison was made on the fuselage because the existing AQUILA fuselage was not available.

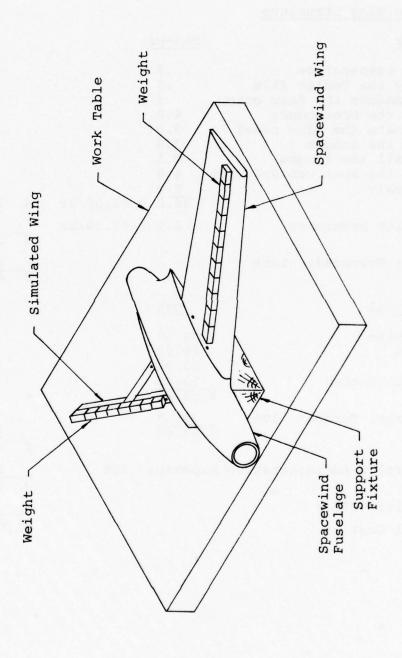


Figure 17. Test Setup

RPV STRUCTURAL COMPONENT COST ANALYSIS

The cost estimate for production of Spacewind RPV structural components is shown below.

Basic Wing Structure

Labor	Man-hr		
Mold preparation Apply the Tedlar film Thermoform the foam core Wind the broadgoods Laminate the wing panel Wind the longos Install the longos Fab. the spar web and rib Assembly	8.0	\$6.00/hr	\$ 156.00
Quality Assurance	4.0 @	\$7.00/hr	$\frac{28.00}{$184.00}$
Labor Overhead: 125%			\$ 414.00
Material	Cost		
Graphite Resin Foam Miscellaneous	\$200.00 50.00 30.00 50.00 \$330.00		
Material Burden: 10%	$\frac{33.00}{$363.00}$		363.00 \$ 777.00
General & Administrative	Expense:	25%	194.00 \$ 971.00
Profit: 10%			97.00
Total Cost			\$1,068.00

Basic Fuselage Structure

Labor	Man-hr	
Mold preparation Apply the Tedlar film Thermoform the foam core Wind the broadgoods Laminate the shell Wind the longo Install the longo Fabricate the bulkheads Assembly	.5 1.0 4.0 3.0 2.0 2.5 4.0 8.0 25.5 @ \$6.00/hr	\$ 153.00
Quality Assurance	4.0 @ \$7.00/hr	28.00 \$ 181.00
Labor Overhead: 125%		226.00 \$ 407.00
Material	Cost	
Resin Foam Miscellaneous	\$200.00 50.00 30.00 50.00 \$330.00	
Material Burden: 10%	33.00 3363.00	363.00 \$ 770.00
General & Administrative	expense: 25%	193.00 \$ 963.00
Profit: 10%		96.00
Total Cost		\$1,059.00

CONCLUSIONS

The model RPV structure fabricated withstood all required loads, was of allowable weight, and presented no manufacturing problems. It was totally successful.

There were problems in sample testing. Hindsight indicates tensile test samples should have had a foam core to represent more nearly the end application.

Flexural panels failed predominately by buckling. Better adhesion between the core and Spacewind face and a stiffer core will retard or eliminate buckling.

Correlation between the computer model and test results was good for graphite, fair for Kevlar, and poor for glass. The computer model assumes that failure was caused by tension, compression or shear. Samples failed by an instability mechanism. There is reasonable doubt whether correlation problems are caused by computer model errors or test result errors. Since the scale model RPV sustained all required loads and since it was designed according to analytical methods, the evidence favors the computer model being reasonably accurate.

APPENDIX A COMPUTER PROGRAM AND PRINT OUT

```
PROGRAM SHPROP (INPUT, OUT PUT, TAPE 5= INPUT, TAPE 6= OUT PUT)
   DIMENSION HEAD(16)

1 REAU(5,2)(HEAD(I),I=1,16)

2 FORMAT(16A5)
   It (EOF,5) 11,4

4 READ(5,5) VF,UF,UR,RMOF,RHOR,EF,EFT,GF,ER,FTU,FCU,FSU,AF,AFT,AR

5 FORMAT(5F10.4/4E10.3,8F10.0/3E10.3)
        CK=.25
VR=1.-VF
HF=VF*RHOF/(VF*RHOF+VR*RHOR)
        WP=1.-WF
FT=FTU
        FC=FCU
FTU=FTU*VF
         FCU=FCU+VF
   6 CC= .25
 RHO=(VF*RHOF+(1.-VF)*RHOR)*CK
WRITE(6,10)HEAD
10 FORMAT(1H1,16A5)
   WRITE (6,8) CK
8 FORMAT (5x,22HFIBER COVERAGE RATIO =F5.3/)
HRITE(6,11)

11 FORMAT(5X,16HFIRER PROPERTIES, 22X,16HRESIN PROPERTIES, 22X,20HCOMPO

1SITE PROPERTIES/)

WKITL(6,12) VF, EF, VZ, EZ, RHO, WF, EFT, WR, AR, FTU, RHOF, GF, RHOR, UR, FCU, FT

1. AF, FSU, FSU, FC, AFT, UF

12 FORMAT(5X,5HVF = F6.4,8X,4HEF = E1C.3,5X,5HVR = F6.4,8X,4HER = E10.3

1.5X,4HRHO=F6.4/5X,5HMF = F6.4,8X,4HET=E10.3,5X,5HMR = F6.4,8X,4HBR

2R = C1C.3,5X,4HFTU=F9.1/5X,5HRHOF=F6.4,8X,4HGF = E10.3,5X,5HRHOR=F6.

34,8X,4HUR = F6.4,9X,4HFCU=F9.1/5X,5HFTU = F9.1,5X,4HAF = E10.3,5X,5HF

4SU = F9.1,24X,4HFSU=F9.1/5X,5HFCU = F9.1,5X,4HAFT=E10.3/5X,5HFF

5.4/)

WRITE(6,15)

15 FORMAT(123H ALPHA EX EY GXY
                                                                                                  EY FYCU
 15 FORMATCIZAH
                                         ALPHA EX
                                                                                                                                                            UXY
                                                                                                                               GXY
      1 UYX FXTU
2 AY/1
                                                                                                                                       FXY
                                                                                FXCU
         A=( .
 20 CUNTINUE
A=A/57.29578
S1=SIN(A)
S2=S1**2
        S3=S1*S2
S4=S2**2
        C1=COS(A)
C2=C1**2
         C3=G1 *C2
        C4=C2++2
         SZA=SIN(Z. *A)
        C2A = COS(2. + A)
UL T = UF + VF + UR + (1. - VF)
        SVF=SQRT(VF)
EL=EF*VF+(1.-VF)*ER
        EC=EFT
C=SVF
```

```
ET=((C*EC+(1.-C)*ER)*ER)/(C*ER+(1.-2.*UR**2)*(1.-C)*(G*EC+(1.-C)*
 UTL=ULT+cT/EL
  U=1.-ULT*UTL
 1)
 823 =1./U*((ET-EL*UTL-2.*U*GLT)*S1*C3-(EL-EL*UTL-2.*U*GLT)*S3*C1
1)
EX=(B11-312**2/B22)*CK
 EY=(822-812**2/811)*CK
 UYX=8.2/811
GXY=833*CK
  THERMAL EXPANSION CALCULATIONS
 THERMAL EXPANSION LALCULATIONS

E1=5L/(C4+EL*S4/ET+.25*(EL/GLT-2.*ULT)*S2A*S2A)

E2=EL/(S4+EL*C4/LT+.25*(EL/GLT-2.*ULT)*S2A*S2A)

612=EL/(1.*2.*ULT+EL/ET-(1.*2.*ULT+EL/ET-EL/GLT)*G2A*C2A)

U12=E1/EL*(ULT-.25*(1.*2.*ULT+EL/ET-EL/GLT)*S2A*S2A)

U21=U12*E2/E1

B1=S2A*(2.*ULT+EL/ET-.5*EL/GLT-C2*(1.*2.*ULT+EL/ET-EL/GLT))

82=S2A*(2.*ULT+EL/ET-.5*EL/GLT-S2*(1.*2.*ULT+EL/ET-EL/GLT))

E1R=EL/(EL/C1-B1*B1*C12/EL)
 E1R=EL/(EL/c2-B1*B1*B1*B1/EL/E)

U21B=E20/FL*(U21*EL/F2*B1*B2*G12/EL)

U123=c1R/FL*(U12*EL/F1*B1*B2*G12/FL)

U123=c1R/FL*(U12*EL/F1*B1*B2*G12/FL)

G12R=EL*(1,-U12*U21)/(FL*(1,-U12*U21)/G12-B1*F1/FL*(B1*U21*B2)-92*
G12-E2-E1(R2-U12-WE1)/IEL-(11--U12-U12)/G12-B1-E.

HE2/FL (R2-U12-WE1))

AL = (AK*(1.-VF)*ER*AF*VF*EF)/EL

B=SQRT(VF3.1-15926)

AD=AR*(1.-2.*B)+2.*AFT*3-UR*(AFT-AR)*(1.-2.*B)

E0=LR*EFT/(LFT*(1.-2.*B)+2.*ER*B)
 AT=(AU+LU+B+AR+ER+(1.-B))/ET
A1=AL+C2+AT+S2
 A2=AL*S2+AT*C2
A12=2.*(AT-AL)*S1*C1
 A18=A1-A12*B1*G12/EL
A28=A2-A12*B2*G12/EL
  STRENGTH CALCULATIONS
  PSI=U
  U1=1./(8.*PSI)*(EL+=T+UTL*EL+JLT*ET)
 U1=1./(0.*P51)*(P51*GLT-.5*(UTL*EL+)UT*ET))
U2=1./(2.*P51)*(P51*GLT-.5*(UTL*EL+ULT*ET))
U3=1./(2.*P51)*(EL+ET)
U4=1./(d.*P51)*(EL+ET-(UTL*EL+ULT*ET)-4.*P51*GLT)
u11L=5.*U1+U2+U3+U4
 Q12L=U1-U2-U4
Q22L=3.*U1+U2-U3+U4
  Q66L=U1+U2-U4
 Q11M=3. #U1+U2-U3+U4
Q1cM=U1-U2-U4
```

```
Q224=3.+U1+U2+U3+U4
      Q66H=U1+U2-U4
Q11H=3.*U1+U2+U3*COS(2.*A)+U4*COS(4.*A)
Q12H=U1-U2-U4*COS(4.*A)
Q22N=3.*U1+U2-U3*COS(2.*A) )+U4*COS(4
                                                  1+U4*COS(4.*A)
      Q66N=U1+U2-U4+COS(4.+A)
       RU12=012N
       R022=Q22N
      RQ66=Q66N
      FXCU=FCU+ (RQ11+RQ22-RQ12+RQ12) / (011L+RQ22-0,2L+RQ12)+CK
      FYCU=FCU*(RQ11*RQ22-RQ12*R412)/(922M*RQ11-Q12M*RQ12)*CK
A=.785398-A
      711N=3.*U1*U2+U3*COS(2.*A)*U4*COS(4.*A)
Q12N=U1-U2-U4*COS(4.*A)
Q22N=3.*U1*U2-U3*COS(2.*A) )*U4*COS(4
Q66N=U1*U2-U4*COS(4.*A)
                                                  ) +U4*COS (4.*A)
       R011=011N
       R012=012N
       R02_=022N
      RQ66=Q66N
FSCU=FCU*(RQ11*PQ22-RQ12*RQ12)/(Q11L*RQ22-Q12L*RQ12)*CK
       A=.785398-A
       ET=0.
      ULT=0.
      UTL=..
      UTL=..
PSI=1.
U1=1./(8.*P5I)*(EL+ET+UTL*EL+ULT*ET)
U2=1./(2.*P5I)*(EL+ET)
U3=1./(2.*P5I)*(EL+ET)
U4=1./(8.*P5I)*(EL+ET)
U4=1./(8.*P5I)*(EL+ET)
U1:=3.*U1+U2+U3+U4
U1:=3.*U1+U2-U4
U2:=3.*U1+U2-U3+U4
U2:=3.*U1+U2-U4
U3:=3.*U1+U2-U4
      Q11M=3. *U1+U2-U3+U4
Q12M=U1-U2-U4
      Q22M=3.*U1+U2+U3+U4
Q66M=U1+U2-U4
      Q11N=3. + J1+U2+U3+COS(2. +A)+U4+COS(4.+A)
      Q12x=U1-U2-U4*LOS(4.*A)
Q22N=3.*U1+U2-U3*COS(2.*A )+U4*COS(4.*A)
Q66N=U1+U2-U4*COS(4.*A)
      RQ11=Q11N
      R012=012N
       RO22=022N
      RQ66=Q66N
FXTU=FTU*(RQ11*RQ22-RQ12*RQ12)/(Q11L*RQ22-Q12L*RQ12)*CK
      FYTU=FTU+(RQ11+RQ22-R912+R012)/(Q22M+RQ11-Q12M+RQ12)+CK
      A= . 785398-A
      Q11N=3.*U1+U2+U3*COS(2.*A)+U4*COS(4.*A)
      Q12N=U1-U2-U4*LOS(4.*A)
Q22N=3.*U1+U2-U3*COS(2.*A
Q664=U1+U2-U4*CCS(4.*A)
                                                  )+U++COS(4.+A)
      R011=011N
      R012=012N
      RQ22=Q22N
      ROF = 066N
      KGC0=G000
FSTU=FTU*(R011*9Q22-3012*3Q12)/(01_L*3022-012L*RQ12)*CK
FXY=FSTU/((1.+(F5TU/FSCU)**2+FSTU/FSCU)**.5)/2.
      A=.785398-A
A=A*57.295827
HRITE(6,5J)A,EX,EY,GXY,UXY,UYX,FXTU,FYTU,FXCU,FYCU,FXY,413,428
 52 FORMAT (1X,F7.2, 3E12.3, 4F6.4, 5F10.1, 2E12.3)
      A=A+1.
IF (A-46.) 20,100,100
100 GK=GK+CC
IF(GK-1.)6,6,145
1J5 GO TO 1
110 STOP
```

MATERIAL PROPERTY COMPUTER OUTPUT NOMENCLATURE

AF Fiber thermal expansion coefficient, in/in/F°

AFT Fiber Transverse thermal expansion coefficient, in/in/F°

ALPHA Winding angle relative to "x" axis, deg.

AR Resin thermal expansion coefficient, in/in/F°

AX Composite thermal expansion coefficient in x-direction, in/in/F°

AY Composite thermal expansion coefficient in y-direction, in/in/F°

EF Fiber modulus, psi

EFT Fiber transverse modulus, psi

ER Resin modulus, psi

EX Composite modulus in x-direction, psi

EY Composite modulus in y-direction, psi

FCU Fiber or composite compressive strength, psi

FSU Resin or composite shear strength, psi

FTU Fiber or composite tensile strength, psi

FXCU Composite compressive strength in x-direction, psi

FXTU Composite tensile strength in x-direction, psi

FXY Composite shear strength, psi

FYCU Composite compressive strength in y-direction, psi

FYTU Composite tension strength in y-direction, psi

GF Fiber shear modulus, psi

GXY Composite shear modulus, psi

RHO Composite density, 1b/in³

RHOF Fiber density, lb/in³

UF Fiber Poisson's ratio

UR Resin Poisson's ratio

UXY Composite Poisson's ratio

UYX Composite Poisson's ratio

VF Fiber volume ratio

VR	Resin	volume	ratio
WF	Fiber	weight	ratio
WR	Resin	weight	ratio

Fig. Style Fig.		יייי שמו רשונים							1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	200			
EX EX EX EXT		,6,000	EFF = 3.400 EFT = 3.500 GF = 3.500 AF =-2.400 AFT = 2.960		.5600 .3931 .0412	•	11 11 11		RHO= .0131 FTU= 162500 FCU= 167500 FSU= 8000	000			
4.106F*16 5.408F*10 1.27F*10		*	EY	GXY	UXY	UYX		FYTU	FXCU	FYCU	FXY	AX	AY
4.2966***16 5.3467***16 1.266***16 3.46***16		95+56	485540	.274F+0	285	. 00.36	40625.0	-	6875.	341.7	5.3		7.427F-0
4.2796666 5.956464, 1.3707605 .4652 .0004 39702, 4.57046 4.2796666 5.956264, 1.3707605 .4652 .0004 39702, 4.57046 4.279666 5.956264, 1.3707605 .4652 .0004 39702, 4.57046 4.279666 5.956264, 1.4997605 .1552 .0004 39702, 4.57046 4.279666 5.956264, 1.4997605 .1557 .0004 39702, 4.57046 4.279666 6.956264, 1.4997605 .1557 .0004 39702, 4.57046 4.279666 6.956264, 2.337665 .1557 .0004 39702, 4.57046 4.279666 6.956264, 2.290666 .15702 .15702 .0004 39702, 4.57046 4.279666 6.956264, 2.290666 .15702 .15702 .0004 39702, 4.57046 4.279666 6.956264, 2.290666 .15702 .15702 .0004 39702, 4.57046 4.270666 6.956264, 2.20066 .15702 .10004 30004		5E+16	.497E+0	.286E+0	.3.55	. 00 39	40520.6	1.5	6857	342.5	1345.6		DAE
4.253 26.00 5.50 26.00 1.45 26.00		6E+16	5.534E+64			2400.	40210.4	5.3	2680 3.0	344.8	1111.9		7.352E-0
4.2518e16 5.662E014 1.562E05 762 0105 39154 35.7 26565.6 554.0 1338 4.2518e16 5.62565.8 354.0 1.557.9 4.2518e16 5.579Ee14 1.562E05 762 0105 375.9 4.2518e16 5.579Ee14 1.562E04 1.562E0 4.2518e16 5.275E04 1.575.9 4.2518e16 5.275E04 1.5762E04 1.5762E		90+36	5.595E+04	1.378E+05		.0061	39762.9	13.2	26706.6	348.6	1182.6		7.261E-09
4.271EFF 6 5.93EFF 4 1.687E+5 1.1528 4.015 38155,4 35.7 25355,3 351.0 1338.4 4.271EFF 6 5.93EFF 4 1.687E+5 1.1528 4.014 351.0 1.1528 4.014 351.0 1.1528 4.014 351.0 1.1528 4.014 351.0 1.1528 4.014 351.0 1.1528 4.014 351.0 1.1528 4.014 351.0 1.1528 4.014 3.015		3E+C6	5.682E+04	1.459E+05		.008	39011.9	23.5	56566.6	354.0	1257.9		7.135E-
4.111E(10 6.791E(10) 4.101E(10) 1.1579 (1179.3 5110.4 51010.1 5170.2 5170.4 517			5.793E+u4	1.562E+15		.0105	38155.4	36.7	26355.3	361.0	1338.4	-1.594E-07	6.979E-0
19.99E+66 6.99E+94 2.19Fe+95 1.3677 102.2 4401.8 94.7 55201.6 391.4 1519.0 3.949E+66 6.99E+94 2.47845 1.367.2 349.7 55201.6 391.4 1519.0 3.949E+66 6.99E+94 2.47845 1.367.3 3216.9 1.301.3 1.301		15+16	5.930E+04			.0135	3/154.3	55.0	26726.0	369.5	1424.3		6.5 ABE-0
3.095E 0.6 6.096E+04 2.197E+05 1.5977 0.20, 335555 120.2 2.774.0 6.046.0 1.131.3 1.30.5 2.00 6.096E+04 2.137E+05 1.9112 0.313 3.216.0 1.40.0 2.017E+05 1.9112 0.313 3.216.0 1.40.0 2.017E+05 1.9112 0.313 3.216.0 1.40.0 2.017E+04 3.018E+04 2.017E+05 1.0912 0.318.0 1.40.0 2.017E+0 1.9112 0.318.0 1.40.0 2.017E+0 1.40.0 2.017E+05 2.018E+04 3.018E+04		75+66	6.281F+04	2.001E+05		0212	34810.8	94.7	25281.6	391.4	1614.1		6.361E-0
3.7276-66 7.208-44 2.0377-65 1.7072 .0333 32165-8 148.8 24413.2 449-9 1.051.3 3.7276-66 7.208-44 2.0377-66 2.0378-8 1.051.3 3.7276-66 7.208-44 2.0377-66 2.0576-7 1.051.3 3.7276-66 7.208-64 7.008-7 1.051.3 3.708-8 2.057-6 7.208-9 1.051.3 3.708-9 1.051.3 2.056-6 7.208-9 1.051.3 2.056-6 7.208-9 1.051.3 2.056-6 7.208-9 1.051.3 2.056-6 7.208-9 1.051.3 2.056-6 7.208-9 1.051.3 2.056-6 7.208-9 1.051.3 2.056-9 1.051.3 2		95+16	6.496E+04	2.188E+05		.026.	33515.5	120.2	24744.8	404.8	1719.0	-1.029E-36	6.118E-0
3,756Eff6 7,307Eff4 2,617Eff5 1,9812 .0373 31788.1 180,7 2339.9 455.7 1951.5 3,756Eff6 7,307Eff4 2,817Eff5 2,15.5 .0513 28199.1 255.2 455.2 177.1 475.6 2218.0 3,15.5 1951.5 3,15.5 1951		5E+06	6.738E+u4	2.393E+05	-	.0313	32167.8	148.8	24113.2	419.9	1831.3	-1.277E-06	5.863E-0
3.596E+06 7.307E+04 3.135E+05 2.1557 .05438 22934,48 215:9 2556.1 4555.4 2160.2 3.596E+06 7.997E+04 3.135E+05 2.7429 .0568 26627 6 296.5 2761.7 475.8 2218.0 3.305.6 2.7429 .0568 26627 6 296.5 2761.7 475.8 2218.0 3.305.6 2.7429 .0568 26627 6 296.5 2776.7 496.1 2505.6 3.345.6 6 2.0521 3.245.6 6 20.0521 3.245.6 6 20.052.4 3.666.6 6 2.052.4 3.666.6 6 2.052.4 3.666.6 6 2.052.4 3.666.6 6 2.052.4 3.666.6 6 2.052.4 3.666.6 6 2.052.4 3.666.6 6 2.052.4 3.666.6 2.052.4 3.666.6 2.052.4 3.666.6 2.066.2 2.066.2 2.066.4 6.066.6 2.066.2 2.067.4		7E+06	7.008E+04	2.617E+65	-	.0373	30788.1	180.7	23389.8	436.7	1951.5	-1.528E-06	5.600E-
3.494E+06 6 7.692E+04 3.835E+05 2.5255 .0573 265278 1 342.0 19779-5 522.3 2552.5 2.5253.7 2522.5 2.5252.7 2.5252.5 2.5252.7 2.5252.5 2.5252.7		6E+C6	7.307E+04	2.857E+05	~ (.0438	29394.8	215.9	22582.0	455.4	2.180.2	-1.778E-06	5.331E-0
3.149 CE-10 8.33 EE-14 3.066 EE 15 2.524 5.10573 25278.1 342.1 19779.5 522.3 2523.7 2289.4 444.2 17752.6 640.1 3571.1 548.6 2692.9 2.822 64.6 3.96 11.0 2.643 6.1053 2269.4 444.2 17752.6 640.1 3571.7 2.822 64.6 1.0 2.		45400	7.0025414	3.1136+05	v 0	. 150.	26627.6	206.5	20761.7	473.0	2365.6		4. 7915-0
2.90ec+6. 0.002E+04 3.991E+05 2.509 .0764 23663.5 331.2 10771.1 540.6 2692.0 2.66E+06 9.74E+06 4.26E+06 9.0083 2260.4 4.44.2 1752.0 976.9 2075.0 2.66E+06 9.74E+04 4.501E+05 4.901E+05 2.504.0 1101 1673.0 077.4 3167.2 2.19E+06 1.02E+05 4.901E+05 2.504.0 1101 1772.5 675.1 377.7 2.19E+06 1.20E+05 5.858E+05 2.501 1133. 1087.5 675.4 177.7 177.2 675.1 377.7 2.19E+06 1.20E+05 2.501 1132. 1087.5 655.6 177.2 675.1 377.7 777.7 777.7 777.7 777.1 777.7 777.1 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7 777.7		5E+06	8.381E+u4	3.666E+05	, ~	. 0673	25278.1	342.0	19779.5	522.3		481E-0	4.524E-0
2.062E+16 4.26E+16 2.629 .1068 2.299.4 444.2 1775.8 576.9 2073.8 2.50ZE+16 1.02E+16 4.50E+15 2.6436 .1088 2.643.6 51.0 1.6773.9 607.4 3167.2 2.50ZE+16 1.02E+16 4.50E+16 2.6436 .1081 662.6 1.4773.8 675.1 1.492.9 2.30ZE+16 1.14E+16 5.55BE+16 2.520 .135.2 1.081.7 662.6 1.4773.8 675.1 377.7 2.01E+16 5.55BE+16 2.520 .1467 1.081.7 665.6 1.346.9 775.1 377.7 1.79G+16 1.20FE+16 5.55BE+16 2.520 1.467 1.706.7 779.4 477.3 775.7 775.		4E+66	8.802E+04	3.961E+05	~	1929	23963.5	391.2	18771.1	548.6		-2.690E-06	4.262E-0
2.6612-66 9.744-6104 4.58012-605 2.6645 6.1068 21463.6 59110 16779.0 607.4 3.167.2 2.5012-66 1.0832-05 2.56476 1.0808 21463.6 59110 16779.0 607.4 3.167.2 2.5492-66 1.0832-05 5.2572-05 2.5610 1.135. 12026-4 561.7 1572-5 571.7 172.6 172.6 2.353.7 172.6 1.0812-0 1.2077-05 5.8912-05 2.5510 1.135. 12020-7 626.6 1.4773.6 672.1 3493.6 2.2011-6 1.1277-0 1.2077-05 5.8912-0 2.5510 1.135. 12020-7 626.6 1.276-4 6.2252-0 1.2077-0 2.4531 1.166.7 1206.7 769.4 1.2801.7 712.6 3.727-5 1.0801-4 6.1276-4 6.2252-6 6.2252-6 1.135. 1202.7 769.4 1.2072-6 6.2252-0 6.2252-0 1.1207-0 1.136.2 1.111.6 1.		2E+06	9.256E+04	4.26 6E+05	~	.0863	2269u.4	2.444	17752.8	576.9		-2.883E-06	4.00 SE-0
2.349Ee+6 1.032E+0 5.961Ee+0 2.6510 1.133 10087.6 626.6 14772.6 676.1 3427.6 2.349Ee+6 1.032E+0 5.951Ee+0 5.22Ee+0 5.251Ee+0 5.22Ee+0 5.251Ee+0 6.251Ee+0 6.22Ee+0 5.22Ee+0 5.251Ee+0 6.22Ee+0 5.22Ee+0 5.251Ee+0 7.251.7 772.6 679.4 12949.1 752.7 3975.5 1.952Ee+0 1.276Ee+0 6.22Ee+0 5.25Ee+0 7.452.7 17068.7 769.4 12949.1 772.6 3777.5 1.276Ee+0 1.276Ee+0 6.22Ee+0 7.2752.7 17068.7 76949.1 772.7 772.7 772.7 772.7 1.276Ee+0 1.276Ee+0 6.22Ee+0 7.2752.7 17068.7 76949.1 772.7 772.7 772.7 772.7 1.276Ee+0 1.2509Ee+0 7.216Ee+0 7.216Ee		1E+66	9.744E+04	4.580E+05	~	9960	21463.6	591.0	16739.0	4.709		-3.058E-06	3.756E-0
2.20156.6 1.2076.0 5.5566.0 2.557 1.161 1.132 1.101 1.0 1.0 1.207.0 1.		2E+16	027E+0	4.961E+05	20	1262	10160.7	561.7	15742.5	675.1		-3.213E-06	3.516E-0
2.059E+00 1.207E+05 5.891E+05 2.5224 .1467 17066.7 769.4 12949.1 752.7 3975.5 1.795E+06 1.207E+05 6.525E+05 2.5371 .162 1109.9 931.5 1130.2 795.4 4237.7 1.799E+06 1.207E+05 6.556E+05 2.5371 .162 1109.9 931.5 1130.3 9849.8 94.6 94.5 1.799E+06 1.508E+05 6.556E+05 2.2572 .1929 14310.9 1018.5 10552.9 889.3 4802.9 1.568E+06 1.597E+05 7.536E+05 2.202 12493.5 11314.3 996.9 951.9 94.5 951.4 951.2 996.9 951.5 1.464E+06 1.597E+05 7.556E+05 2.0048 .2278 11911.3 1314.3 951.4 1053.9 996.9 951.6 1.397E+06 1.597E+05 7.556E+05 2.0048 .2278 11201.1 9193.2 995.4 1155.8 951.4 1053.9 951.4 1193.8 951.4 1053.9 951.4 1193.8 951.4 1105.8 951.4		15+16	43E+0	5.558E+05		133	18087.5	695.8	13840.7	712.6		-3.461E-06	3.062E-0
1.9926		96+00	1.207E+05	5.891E+05	8	.1467		769.4	12949.1	752.7		-3.552E-06	2.849E-0
1.568E+66 1.336E+65 6.68E+65 2.3527 .1766 15179.8 931.5 1133.3 840.9 4553.7 1668E+66 1.346E+66 1.456E+66 1		5E+06	1.2766+45	6.225E+05	2	.1612	6	847.6	12102.7	4.567	237.	-3.620E-06	2.645E-0
1.66 E 6 1.69 E 6 1.69 E 6 1.65 E 6 1.69 E 6 1.6		90+36	.349E+C	6.558E+05	'n	1766		930.5	1130 3.8	6.048	513.		2.452E-0
1.664er6 1.697er6 7.536er6 2.0954 .2285 12713.7 1210.1 9193.2 995.7 5416.1 1.664er6 1.697er6 7.556er6 2.0954 .2285 12713.7 1210.1 9193.2 995.7 5416.1 1.264er6 1.699er6 9.756er6 2.0048 .2272 1198.3 1114.3 6581.4 1155.6 1.65.6 1.709er6 0.155er6 1.2786 2.026er6 0.156er6 1.2786 2.024 1115.6 6.156er6 2.024er6 0.156er6 1.7366 .3364 100.34 1663.5 6992.2 1115.6 6331.0 1.115er6 2.125er6 9.003er6 1.7366 .3364 9443.6 1793.1 6535.4 1325.7 700.2 9.756er6 9.003er6 1.7366 .3364 9443.6 1793.1 6535.4 1325.7 700.2 9.756er6 9.499er6 1.7465 3.3862 8380.9 2.774.2 5720.0 1408.3 7560.5 8.014er6 2.528er0 9.499er0 5.1465 3.3862 8380.9 2.274.2 5720.0 1408.3 7560.5 8.014er6 2.528er0 9.499er0 5.1463 3.3862 8380.9 2.274.2 5720.0 1408.3 7560.5 8.014er6 2.528er0 9.499er0 5.1463 3.7869.4 2226.5 5356.4 1577.9 810.8 8.014er6 2.528er0 9.728er0 1.2786 8.014er0 2.528er0 9.728er0 1.2786 8.014er0 2.528er0 9.7022.0 2.285.5 4413.1 1873.6 8820.4 6.166er0 3.3178er0 2.1028er0 6.1289 8.004.8 5203.8 4139.1 1872.6 8820.1 7.2468 8.014er0 2.528er0 3.3178er0 2.1058er0 3.004.8 5841.9 3322.0 3885.8 2314.9 8920.1 5.004.8		A + + + + + + + + + + + + + + + + + + +	426E+U	7.215F+05	•	2102		1111.6	9849.8	0.000	104.		2.092F-0
1.367Ec06 1.69 E+05 7.050E+05 2.0040 .2470 11901.3 1134.3 0503.4 1053.9 5776.4 1.277Fec06 1.777Fec0 1.777F		97+34	1.597E+05	7.536E+05	10	.2285		1210.1	9193.2	1.566		-3.662E-06	1.927E-0
1.277E 6 1.789E 6 5 1.9142 .2662 11200.2 1124, 6 012.2 1115.8 6 6.62.4 11.93E 6 6.62.4 11.93E 6 1.879E 6 1.894E 1 1.994E 1 1.9142 .2662 11200.2 1124, 6 012.2 1115.8 6 6.62.4 11.93E 6 1.994E 1 1.994E 1 1.994E 1 1.994E 1 1.995 1 1.9	_	7E+06	1.69 E+05	7.850E+05	N	.2478		1314.3	8581.4	1053.9		-3.614E-06	1.769E-0
1.115E+6 2.006E+05 0.73E+05 1.0516 3324 100334 1653.5 6992.2 1251.5 0531.0 11.15E+6 2.026E+05 0.73E+05 1.0516 3324 100334 1653.5 6992.2 1251.5 0531.0 11.043E+0 2.25E+05 9.00E+15 1.6516 3324 100334 1653.5 6992.2 1251.5 0516.2 13.25.7 100.2 13.25.7 100.2 13.25.7 100.2 13.25.7 100.2 13.25.7 100.2 13.25.7 100.2 13.25.7 100.2 13.25.7 100.2 13.25.7 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.4 100.2 13.25.2 10.2 13.2 13.2 13.2 13.2 13.2 13.2 13.2 13		7E+06	1.789E+05	8.155E+05	-	.2682		1454.4	012.	1115.8		-3.541E-06	1.621E-0
1.043E46 2.125E405 9.003E435 1.6506 3364 9443.6 1793.1 6536.4 1325.7 7000.2 9.756E465 2.351E405 9.256E405 1.5671 3364 9443.6 1793.1 6536.4 1325.7 7000.2 9.156E405 9.256E405 9.499E465 1.8613 .3882 8380.9 2.074.2 972.8 1408.3 7650.5 9.152E405 9.928E405 1.8613 .3882 8380.9 2.074.2 972.8 1408.3 7650.5 0.014E465 2.679E405 9.728E405 1.8612 0.4450 700.2 0.226.5 6.7013.5 1772.6 8420.4 7.514E465 2.6679E405 1.012E405 1.3336 .4450 700.2 0.2355.5 47013.5 1772.6 8420.4 7.499E405 1.028E405 1.028E405 1.028E405 1.028E405 1.028E405 1.028E405 1.028E405 1.028E405 1.028E405 1.006E405 1.0043E405 1.006E405 1.0047 6.6808 5497.2 3332.7 3649.8 2244.2 90890.1 5.838E405 1.006E405 1.006E406 1.0047 6.6808 5497.2 3332.7 3649.8 2244.2 90890.1 5.838E405 1.006E405 1.006E406 1.0047 6.6808 5497.2 33554.3 3429.8 2382.0 9160.1 5.456E405 4.5676.0 1.006E406 1.0047 6.6808 5497.2 3354.3 3429.8 2382.0 9160.1 5.456E405 4.5676.0 1.006E406 1.0047 6.6808 6.457.7 4035.4 3429.8 2382.0 9160.1 5.456E405 4.5676.0 1.006E406 1.0047 6.6808 6.457.7 4035.4 3432.7 2686.0 9226.1 9224.1 5.456.6 4.546.6 4.546.6 4.546.6 4.546.6 5.456.6 4.546.6 4.546.6 5.456.6 4.546.7 4.5496.4 2.856.7 2.858.1 9224.1		3E+15	1.894E+U5	8.45UE+U5		3124		1540.7	6 99 2 2	1251.5		-3.444E-UD	1. 34 7F -D
9.756E+65 2.251E+65 9.259E+65 1.5671 .3616 8096.7 1929.9 6113.4 1404.5 7352.4 9.756E+65 2.352E+6 9.259E+65 1.8671 .3616 8096.7 1929.9 6113.4 1404.5 7550.5 9.352E+6 9.722E-15 1.4685 .3882 8380.9 2074.2 5720.8 1488.3 7650.5 9.722E-15 1.4685 .4463 7455.3 2226.5 5356.4 1577.8 7590.2 8.014E-65 2.679E+65 9.928E+65 1.3336 .4463 7425.3 2287.1 5018.0 1671.9 8167.8 7.514E-65 2.679E+65 1.0122E-66 1.2510 .5096 6593.0 2235.2 4411.1 1672.6 8420.4 7.349E-95 3.311E+65 1.020E-16 1.273 .5641 65016.8 223.8 4411.1 1672.6 8452.4 6.516.6 5.323.8 4411.1 1933.6 882.4 6.5212E-9 3.357E-05 1.056E-16 1.0645 .5604 5417.2 3352.8 3885.8 2244.9 8950.1 5.835.8 4.294.8 2332.0 9850.1 5.835.8 4.295.8 4.2950.1 5.835.8 4.295.8 4.2950.1 5.835.8 4.2950.1 5.835.8 4.2950.1 5.835.8 4.2950.1 5.835.8 4.2950.1 5.835.8 4.2950.1 5.835.8 4.2950.1 5.835.8 4.2950.1 5.835.8 4.2950.1 5.	_	35+16	2-125E+05	9.003E+35	-	.3364		1793.1	6536.4	1325.7		-3.176E-06	1.222E-0
9.1326-65 2.3856-45 9.4966-15 1.4863 .3882 8380.9 2074.2 5720.8 1488.3 7660.5 8.5536-4 1572.8 1488.3 7660.5 8.0146-45 2.6796-61 9.9266-15 1.085 4463 7884.4 2225.5 5356.4 1577.3 7930.2 8.0146-45 2.6796-16 9.9266-16 1.2518 4453 7402.0 2556.5 4703.5 1772.6 8427.8 7.5146-65 2.84.6-61 2.016-61 1.2518 4475.3 287.1 5018.0 1772.6 8427.4 7.416-61 2.918.2 2.84.6-61 2.2518.2 2.84.11.1 1879.6 8627.7 7.4496-45 3.1376-45 1.0266-16 1.0391 5.958.4 1391.1 1993.6 8627.7 5.836-61 2.144.9 8428.1 3.3376-61 1.0566-16 1.016-5 5.901.4 5841.9 3122.8 3865.8 2144.9 8950.1 5.4866-61 3.33446-16 1.01746-16 4.766 5476 568 5497.2 3354.3 3429.6 2382.0 91091.1 5.8566-61 4.2566-61 4		6E+65	2.251E+05	9.259E+05	-	.3616	8896.7	1929.9	6113.4	1404.5		-3.004E-06	1.104E-0
8.953645 2.5798465 9.9228475 14,085 4463 7884,4 2226.5 5356,4 157.3 79910.2 0.0148462 2.67798405 9.9228476 1.336 4465 7435.3 22877.1 5018.0 1571.9 0.137.8 0.0148465 2.67798405 1.0128405 1.336 4465 7455.3 2287.1 5018.0 1571.9 0.137.8 7.3148465 2.644884 7.3148465 2.64484 7.3148465 1.0128406 1.1571.9 7.012.0 2556.5 4703.5 1772.6 8420.4 7.3148465 3.137846 1.1028846 6.5441 2.2585.2 4411.1 1993.6 8625.7 7.314846 7.313784 7.31484 7.3		2E+05	2.385E+05	9.499E+05	-	.3882	8380.9	2074.2	5720.8	1488.3		-2.808E-06	9.9196-0
8.014E+65 2.659E+05 9.926E+05 1.336 .4458 7455.3 2287.1 5018.0 1671.9 8187.8 7.514E+65 2.64.E+15 1.012E+06 1.2610 .4769 7002.0 2556.5 4703.5 1772.6 8420.4 7.49E+15 3.131E+05 1.012E+06 1.2010 .4769 7002.0 2735.2 4413.1 1879.6 8657.4 6.516E+05 3.131E+05 1.056E+06 1.1273 .5441 6.206.8 2735.2 4413.1 1879.6 8655.7 6.516E+05 3.312E+05 1.045E+16 1.1273 .5441 6.206.8 2735.2 4139.1 1993.6 8802.4 6.212E+05 3.387E+05 1.055E+16 1.0647 .5186 5497.2 3332.7 3649.8 2244.2 9159.1 5.836E+05 3.344E+05 1.074E+06 .1047 .6186 5497.2 3332.7 3649.8 2244.2 9159.1 5.456E+05 4.249E+05 1.080E+06 .8933 .7011 4863.2 3788.3 3224.5 2522.0 9150.1 4.56E-05 4.567E+05 1.080E+06 .8933 .7011 4863.2 3788.3 3224.5 2529.1 9224.1 9224.1	_	3E+15	2.528E+05	9.723E+35	-	.4163	7.4687	5556.5	5356.4	1577.3		-2.585E-06	8.867E-0
7.1496-65 3.1116-65 1.0266-66 1.1273 .5441 6206.6 2735.2 4411.1 1879.6 8655.7 6.6166-65 3.1936-6 1.0266-66 1.1273 .5441 6206.6 2923.8 4139.1 1993.6 8802.4 6.2126-45 3.1936-65 1.0436-15 1.0645 .5804.9 33.22.8 3885.8 2114.9 8990.1 5.8366-65 3.5946-65 1.0656-66 5.904.7 .6166 5.904.9 33.32.7 3649.8 2244.2 9069.1 5.8366-65 3.3446-05 1.0566-66 1.004.7 .6166 5.904.3 3354.3 3629.8 2244.2 9069.1 5.4566-65 4.266-65 1.0566-66 3.907.8 3.354.3 3629.8 2382.0 9160.1 5.4566-65 4.266-65 4.266-65 3.324.7 272.6 8.324.2 9069.1 9224.1	• (45+65	2.679E+05	9.928E+05		.4458	7435.3	2387.1	5018.0	1671.9		-2.335E-06	7.875E-0
6.616E015 3.193E+05 1.043E+15 1.1273 .5441 6216.8 2923.8 4139.1 1993.6 8882.4 6.212E015 3.193E+05 1.055E+15 1.0645 .5604 5841.9 3332.8 3885.8 214.9 8960.1 5.836E+05 3.576E+05 1.056E+06 1.0047 .6166 5497.2 3332.7 3649.8 2244.9 8960.1 5.836E+05 3.534E+05 1.056E+06 .1047 .6166 5497.2 3354.3 3429.8 2282.0 9169.1 5.486E+05 4.249E+05 1.036E+06 .9476 .6588 5111.3 3554.3 3429.8 2382.0 9160.1 5.456E+05 4.249E+05 1.036E+06 .933 .7011 4863.2 3788.3 3224.5 2529.1 9224.1 9224.1 456E-05 4.567E+05 1.036E+06 .9476 .5686.0 4511.7 4035.4 3032.7 2588.0 9226.0		964.6	3-1116+05	1.028F+06	•	5006		2716.2	4411.1	1879.6		-1.755F-06	6.062F-0
6.212E+u5 3.387E+05 1.055E+16 1.0645 .5604 5841.9 3122.8 3865.8 2114.9 8950.1 5.358E+05 3.597E+05 1.065E+16 1.0647 .6586 5497.2 3332.7 3649.8 2244.2 90591.1 5.486E+05 3.5944.8 3.594.3 3554.3 3429.0 2382.0 9160.1 5.486E+05 4.349E+05 1.074E+06 .9476 .6588 5111.3 3554.3 3429.0 2382.0 9160.1 5.456E+05 4.349E+05 1.080E+06 .9933 .7011 48653.2 3788.3 3224.5 2529.1 9224.1 9224.1 4.586E+05 4.249E+05 1.083E+06 .9476 .945.4 243.2 2882.0 9228.0		5E+05	3.193E+05	1.043E+16	1.1273	.5441		2923.8	4139.1	1993.6		-1.422E-06	5.235E-0
5.836E*U5 3.594E*U5 1.006EF*U6 1.0047 .6186 5497.2 3332.7 3649.8 2244.2 90691. 5.486E*U5 3.814E*U5 1.0174E*U5 .00476 .6568 5111.3 3554.3 3429.8 2382.0 9110.1 5.458E*U5 4.49E*U5 1.008E*U6 .9933 .7111 8653.2 3788.3 3224.5 2529.1 922*.1 4.56E*U5 4.508E*U5 1.008E*U6 .00416 .7024 .70	•	2E+05	3.387E+05	1.055E+36	1.0645	.5804		3122.8	3885.8	2114.9		-1.060E-06	4.457E-0
5.486Ee05 3.884Ee05 1.074Ee06 .9476 .6588 5171.3 3554.3 3429.8 2382.0 9160.1 5.158Ee05 4.349Ee05 1.0480Ee06 .8933 .7011 4863.2 3788.3 3224.5 2529.1 9224.1 4.566Ee05 4.299Ee05 1.083Ee16 .0416 .7424 4556 4571.7 4035.4 3032.7 2686.0 9262.0		6E+05	3.594E.+05	1.066E+36	1.0047	.6186	•••	3332.7	3649.8	2544.2		-6.670E-07	3.726E-0
4.5662-05 4.5998-405 1.0838-20 .0350 .1141 .7056 4574.7 4035.4 3032.7 2686.0 9262.0 4.5662-0	ט ת	+ 0	3.8146+05	1.07 4E+06	9476	2044	5171.3	3554.3	3429.8	2382.0		-2.427E-07	3. U.1E-0
				1.00000	•	7456	671.7	210015	10107	2686.0		7.0555-07	1.70KF-D
			4.5675+05	1.0845405		7657		4296.4	2853.4	2853.7	9274.6	1.232F-06	1.231F-

THORNEL 330/EPOXY -SPACEMIND-FIBER COVERAGE RATIO = .375

	AY	40516-84	4963E-06	4920F-04	4881E-04	4827F-84	.4759E-04	.4678E-04	.4584E-04	4479E-04	.4364E-04	.4239E-04	**************************************	- 3 30 0 C - 0 4	16755-84	1574F-04	1170F-04	.3215E-04	.3059E-04	.2905E-04	.2751E-04	.2599E-04	22075-04	21605-04	.2020E-04	.1884E-04	.1752E-04	.1624E-04	.1501E-04	12685-84	.1158E-04	.1053E-04	.9518E-05	. 8554E-05	.7634E-05	.6758E-05	. 5924E-05	.51335-05	- 4505E-05	20000	2374E-85	17775-05	1220F-85	
	AX	30.378.T.	2955F-06	2561F-06	.1913F-06	1021F-06	9838E-08	1427E-06	2943E-06	4621E-06	6435E-06	6356E-06	103be -05	1241E-05	-1656-05	1860F-05	2058E-05	2248E-05	2428E-05	2595E-05	2748E-05	2885E-05	3005E-05	3180E-05	3246E-05	3283E-05	3297E-05	3286E-05	3251E-05	3103E-05	2989E-05	2847E-05	2677E-05	2479E-05	2251E-05	1994E-05	1706E-05	1386E-05	1035E-05	00-17-00-	21556-06	7007E-0		
	FXY	1476.8	1.569.7	1669.0	1775.3	1889.8	2010.9	2141.6	2281.7	2432.1	2593.6	2767.0	295305	3153.6	33000	1845.7	4110.7	4394.4	4697.5	5020.8	5364.7	5729.4	6115.	1.0269	7388.1	7845.9	8316.1	8795.0	9278.3	1078	10703.6	11151.9	11577.7	11975.8	12342.1	12673.0	12966.1	13219.9	134330	13507.	13/41.3	1 3000	1 1011.9	
ROPERTIES	FYCU	768.5	769.5	772.5	777.5	784.5	793.6				8-058	870.6	892.6	917.0	945.0	1.005.1	10101	1077.2	1117.6	1161.0	1207.7	1257.7	1311.2	130000	1495.1	1564.8	1639.2	1718.6	1803.3	1080.	2092.5	2202.0	2318.9	2443.7	2576.9	2719.3	2871.6	3334.4	32000	2333.5	30.00	20100	4280.1	1.000
COMPOSITE PROPERTIES RHO= 10197 FTU= 162500.0 FCU= 107500.0 FSU= 8000.0	FXCU	10 24 2 . E	40286.2	40205.7	40065.7	49858.4	39573.4	39198.9	38722.7	38133.5	37422.4	36583.7	35616.3	345640	22007	30614.3	20158.8	27662.8	26148.4	24636.7	23146.3	21693.3	23290.5	12671.7	16466.6	15334.4	14275.3	13267.9	12370.0	11210.0	100001	9326.6	8703.8	8128.5	7597.1	7106.1	6652.3	6232.6	2.4485	0.4040	5151.3	7.555.7	4288.7	
	FYTU		2.0	8.8	8.01	15.2	55.1	79.5	108.5	145.0	180.2	223.2	271.1	323.9	381.7	7 4 4	2 4 4 4	666.2	751.4	842.6	0.046	1043.7	1154.1	1205 8	1527.7	1667.4	1815.2	1971.5	2136.6	2495.3	2689.7	2894.9	3111.3	3339.7	3580.6	3834.7	4102.8	4385.7	1.000	1.666	5331.5	4 6 6 6 3 4	3 3	
84 = ,4705+06 A9 = ,4006-04 U9 = ,3503	FXTU	61017.6	60780.0	60 315.5	20554.3	58517.9	57233.1	55731.4	54047.3	52216.2	50273.2	48251.7	46182.2	1.26044	30001	37941.5	35045.2	34035.6	32195.4	30429.6	28741.0	27131.2	25600.1	22760 6	10		-	-		15957.4	4	-	-		-	10503.0	9889.5	9310.1	6.2978	1956	1306.7	6967 6	64444	
RTIES 0.9	UYX	7500	7500	5900	6200	8000	.0123	.0154	.0190	.0232	.0280	.0333	.0393		16531	0100.	787	.0886	. 1993	.1106	.1228	.1357	.1494	11041	1960	.2133	.2317	.2511	.2716	2467	3460	.3653	.3926	.4200	9674.	.4867	.5134	.5478	27846	0229.	0299.	0 40 / 2	1962	246
DESIN PROPERTIES VR = .5000 HAR = .3931 RHOR = .0412 FSU = .8000	UX¥	2863	2002	13197	6907	14937	.6127	.7459	7468.	1.0549	1.2217	1.3902	1.5552	1.7171	1.8565	0.0000	2 4 8 2 3	2.2492	2.2946	2.3192	2.3247	2.3128	2.2857	2 401.0	2.1354	2.0693	1.9981	1.9236	1.8468	1.693	1.6136	1.5373	1.4626	1.3398	1.3192	1.25.9	1.1850	1.1217	1.6669	1.0326	6946.	0000	7967	
340E+08 VR 134E+07 HR 356E+07 HR 2540E+07 RH -240E+05 FSI	GXY	9.49.101	19285450	1081010	20645406	210 17	-2345E+06	.25335+06	.27545+06	.3005E+06	.3286E+üb	. 3596E+06	. 3932E+36	. 4294E+UD	945/34-6	55125405	20101	. 6415E+66	.6888E+25	.7371E+66	.7863E+06	. 9361E+06	. 8862E+C6	. 9365E+UD	11365-117	.10865+67	.1134E+C7	·1181E+07	.12275+07	13175+17	1355-407	.1393E+07	.14295+07	. 146 35 + 67	.1494E+07	.1522E+07	.15475+07	.1569E+07	.15885+07	10145461	.1516E+07	131522010	16725407	1915564.
EF = .349 EFT = .130 GF = .250 AFT = .296	Ε¥	2036-196	12362406	12465456	90 - 30 - 31	9 4 5 9 5 4	12745+36	12922+06	.1313E+C6	.1338E+06	.1366E+36	.1398E+ G6	.14332+36	14/25+36	15155+06	12125436	91 4 20 99 1	17295+36	17945+66	.1863€+36	.19385+16	.23185+36	.21345+06	330354.6	25995+36	.25102+06	.26292+06	.27552+16	.28915+36	27.0014.00	33546+66	. 352 3€ +06	.37165+76	.39152+06	.41285+36	.43555+36	91+38554.	.4858=+36	.5136-+36	07+11+11	.5753:+16	90436660	90457649	00000
FIDER PROPERTIES VF = 5000 RHOF = 0606 FTU = 32500.0 CC = 2150.10 OF = 2250.0	ĘX	2 34 32 54 3	5453E407	64445407	20100119	6 34 35 46 7	.6333F+67	62696+67	.6158E+67	.6385E+07	.5969E+C7	.583 CE+C7	.5671E+67	.5432E+C	.5290E+17	70+11+0nc.	175001	43885+07	.4145E+17	.39.6E+67	.36705+67	.34405+67	.3218E+C7	30 . C. C. C.	26135 +67	.2435E+C7	.2267E+07	.2111E+07	.1966E+07	13325417	15925+07	.1465E+C7	.1386E+07	.1295E+C7	.1211E+07	.1133E+C7	.1.61E+C7	90+32+66.	.933ac+E5	.8759E+16	. 8229E+116	720.01400	272727	. 0027 ETTO
T T T T T T T T T T T T T T T T T T T	ALPHA			7.00			5.90	90.9	2.00	8.30	9.00	10.00	11.00	12.00	13.00		12.00	17.00							25.60											37.60	38.00	39.00	00.04	41.00	62.00	200		20.00

3.7146 3.6766 3.6766 3.6766 3.6766 3.6766 3.6766 3.7176 3.087E-07
2.988E-07
2.988E-07
2.593E-07
4.1529E-07
4.1529E-07
4.1529E-07
4.1529E-07
4.1529E-07
4.1529E-07
4.1529E-07
4.1529E-07
4.1529E-06
4.1699E-06
4.299E-06
4.299E 1007 1365.8
11365.8
11366.8
11366.8
11366.8
11384.7
11438.7
11438.7
11438.7
11438.7
11638.8
11638.8
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9
11638.9 COMPOSITE PROPERTIES RHO= .0262 FTU= 162500.0 FCU= 107500.0 FSU= 8000.0 53375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 0.0
55375 11.10 11 = 4.700E+05 = 4.000E-05 = .3500 A B B 0073 0075 0075 0075 00117 00117 00117 0020 00303 00300 PROPER TIES VR = .5000 WR = .3931 RHOR= .0412 FSU = .0010.0 RESIN 2.548E+05 2.5448E+05 2.5448E+05 2.4548E+05 3.4322EE+05 5.2528E+05 5.2528E+05 6.2532EE+05 1.1888EE+05 EFT= 3.400E+07 EFT= 1.300E+06 GF = 3.500E+06 AF =-2.400E-07 AFT= 2.960E-06 THORNEL 370/E OXY -SPACEMIND-FIBER COVERAGE RATIO = .500 2.194E+05
2.203EE+05
2 FIBER PROPERTIES VF = .5000 MF = .6069 RHOF = .6036 FU = 3250.0. FC = 21500.0. UF = .2200 X ALPHA

THORNEL 30C/EPOXY -SPACEWIND-FIRER COVERAGE RATIO = .625

	AY	.2971E-04	.2961E-04	.2948E-84	.2931E-04	.2909E-04	.2882E-04	. 2850E-04	.2814E-04	27285-04	2679E-84	.2625E-04	.2568E-04	.2507E-04	•	•	•	. 2231E-04	•	• •	.1913E-04				15/0E-04		.1308E-04	.1220E-04	.1134E-04	06765-04		.7989E-05	.7194E-05		. 5667E-15	50-30464°	. 4241E-05	.3570E-05	-2929E-05	. 2319E-05	11 005-05	
	AX	3087E-06	.2772E-06				.3175E-07		17 36E-UB	- 4249E-06	5648E-06	7127E-06	8670E-06	1026E-05	1189E-05	1353E-05	1517E-05	1679E-05	- 19905-05	2135E-05	2270E-05	2394E-05	2504E-05	2598E-05	26/3E-05	2769E-05	2783E-05	2771E-05	2733E-05	266/E-US	2446F-05	22 88E-05	2097E-05	1872E-05	1613E-05	1319E-05	9883E-06	-,6222E-06	2201E-06	. 217 9E - U6	90-34160.	10011
	FXY	2467.6	27.85.7	2963.6	3155.4	3362.5	3586.0	3827.4	1.88.1	4509.3	5001.0	5354.2	5734.4	6143.3	6582.2	7052.3	7.554.7	6390.1	9261.8	9895.7	10561.5	11256.6	11978.0	12722.9	13484.1	15040-1	15821.1	16594.6	17352.9	18088.4	19461.9	20086.7	20662.5	21185.0	21650.6	22056.6	22401.5	22684.1	22904.0	23051.0	2315501	
ROPERTIES	FYCU	2132.8	2137.4	2143.2	2151.3	2161.8	2174.7	2190.1	2220 7	2251.9	2277.9	2306.9	2338.9	2374.0	2412.4	5454.4	2500.0	2569.4	2661.0	2723.6	2791.1	2863.9	2942.4	3026.9	2216.0	3321.5	3435.2	3557.7	3689.7	3031.9	4151.0	4329.8	4523.0	4731.9	4 95 8 . 0	5202.7	5468.0	5755.6	6067.9	0.7040	7175.0	
COMPOSITE PROPERTIES RHO= .0328 FTU= 162500.0 FCU= 107500.0 FSU= 6000.0	Fxcu	67187.5	67011.2	66784.5	66455.4	66013.1	9.44459	64735.9	63016.0	61632.6	60237.8	58655.3	56888.5	54947.3	52847.9	50612.2	48267.0	45842.5	40883.2	38410.9	35981.3	33618.4	31341.8	29166.8	25467 0	23340.4	21643.2	20067.3	18609.0	1/265.4	14886.1	13841.2	12883.1	12005.3	11201.3	10465.1	6.0676	9173.3	8607.5	2613	7176.9	
	FYTU	3.7	14.6	33.0	58.7	91.8	132.5	180.8	2000	372.1	451.8	539.8	636.2	741.2	855.1	978.1	1110.4	1252.4	1 566.6	1739.5	1923.5	2119.0	2326.4	2546.2	3005	3285.8	3561.1	3851.8	4158.8	4486.8	5185.6	5566.2	5 967.7	6391.2	6838.1	7309.5	7806.9	8331.8	8885.9	0.000	100000	*******
ER = .470E+C6 AR = .460E-C4 UR = .3500	FXTU	131562.5	100525.9	99257.2	97529.8	95388.5	92885.7	90078.9	1.7700	90100	6976	73486.9	70008.7	66569.1	63195.2	28666	56725.9	55574.0	47961.7	45218.6	42666.8	40244.6	37949.4	35777.3	31784 2	29953.2	28225.5	26595.7	25058.6	22241.8	20952.4	19736.0	18588.2	17505.1	16482.5	15516.9	14604.8	13742.9	12928.2	1615/19	107675	
PROPERTIES 5000 3931 0412 8160.0	NAN	16091	.0102	.0116	.0135	.0160	.0191	.0228	1000	6750	.0434	.0501	.0574	1690.	.0740	.0833	.0934	11041	1279	.1410	.1543	.1697	.1854	.2019	2 88.0	.2576	.2783	. 3000	.3230	3775	3994	.4275	.4571	.4882	.5209	.5551	.5911	.6288	. 5683	7528	7080	
2 11 11 11	UXY	. 2934	.3183	.3596	.4164	.4880	.5730	0029.	2111.	1.0127	1.1360	1.2590	1.3790	1.4931	1.5985	1.6931	1.7749	1.8427	1.9331	1.9558	1.9643	1,9595	1.9428	1.9155	1.8152	1.7850	1.7303	1.6713	1.6099	1.483	1.4189	1.3551	1.2921	1.2363	1.1698	1.1110	1.0539	1866.	9455		7040	
7435-08 VR -1305-07 WR -3536-07 WR -2406-06 FSU	4×9	37145+06	.3302€+66	.34496+06	.3653E+66	.39145+06	.4230E+06	**60 JE + Co	01437776	60434646	.6578E+06	.7186E+06	.7832E+06	.85155+16	.9231E+06	99765+06	.1675E+07	12355407	13185467	.1401E+07	.1485E+07	.1570E+U7	.16545+07	.1738E+07	10115-07	. 1981E+07	.2058E+07	.21325+07	. 2204E+67	. 227 ZE+07	. 2398E+07	.2454E+07	.2506E+07	.2553E+67	.2595E+07	.26325+67	. 26645+07	. 2690E+07	.2710E+07	2734. 1407	27375407	
EFT = .340 EFT = .130 GF = .350 AFT = .250	FY	34286+06	.3435=+66	.34455+06	.3458E+16	.34745+36	.3495E+ 06	.3520E+06	20400400	36195+06	366,5+06	.37€ 6€ +36	.37582+16	.38145+36	.38752+16	.3342E+16	.4015E+36	90434604	42725+06	.4372=+96	.448UE+36	.4596E+06	.4722E+06	.4857E+36	51585406	.5327E+06	.55082+36	.5703E+36	.5313E+06	63855416	65485+116	.69335+06	.7240E+06	.7572E+ u6	.7932E+36	.8 321=+66	.8742E+36	. 91 99E+16	.9594E+06	11835437	11455407	
PROPERTIES -5100 -6469 -0636 3255400-0 -25540	X.3	.1075E+68	.13746+08	.107 JE+C8	.1064E+C3	.1356£+€8	.13466+68	.1345+08	*1019516	98166+67	95836+07	. 93215+67	.9u33E+07	.8713E+07		.8011E+C7		64625407	.6456£+07	.6065E+G7	.5681E+07	. 53. 8E+07	.4949E+07	.4607E+97	39775+67	.3691E+C7	.3424E+C7	.31775+67	.29485+67	25415407	362E		E+1.7	40 8E+07	781	99	25	9	37	12146+07	11455+17	
FIBER NHF = FTU = UF CU = UF	ALPHA	1.00	2.00	3.00	00.4	2.00	90.9	2.60			11.00	12.00		14.00	15.00	16.00	17.00	18.00	20.00	21.00	22.00	23.00	24.00	25.00	27.00	28.00	29.00	30.00	31.00	33.00	34.00	35.00	36.00	37.00	38.00	39.60	40.00	41.00	30.25	200	30.63	

THORNEL 330/E OXY -SPACEMIND-FIBER COVERAGE RATIO = .750

	AY	2-4765-05	2.474		2.461	2.450	2 4495-05	2.397E-05	2.173E-05	2.346E-05	2.315E-05	۶,	2.245E-0		2 44 8E - 05	2.370F-0	2.0196-05	1.965E-05	1.908E-35		1.7885-05	0-1471.1	1.591F-1	1.521E-0	1.450E-0	1.377E-05	1.30 3E - 05	1.1575-05	1.277E-0	1.J01E-0			7.734E-0	6.991E-0		5.546E-76	4.7495-06	4.17.35-00	3.52(E-06	2.294F-06	1 7265-06	1.1896-36	
	AX	3.0876-07					7 6975-07	-4-635F-09	-9.714E-08	-2.003E-37	-3.126E-37	-4.339E-07	-5.631E-07	-6.991F-07	-9.408E-07	-1.1365-46	-1.287E-06	-1.439c-06	-1.588E-06	-1.735E-06	-1.877E-36	-2.011E - 36	-2.2525-06	-2.3545-36	-2.441E-05	-2.511E-06	-2.562E-05	-2.591E-UB	-2.576E-0b	-2.528£-36	-2.451c-36	-2.343E-06	-2.202E-36	-2.027E-36	-1.816E-06	-1.570E-06	-1.65/2-05	-3.00.E-	-5.081c-0	2.1905-07	2 873	1.1905-16	
	FXY	2.964.7	3167.6	3345.3	3559.2	3790.7	4041.4	4607.0	4925.3	5269.8	.:	6.44.9	6478.7	2.0169	7088	8565.6	9181.6	9835.9	10531.4	11264.6	12335.2	7.14071	14546.9	15438.2	16348.0	17270.0	18196.9	19161.1	23928.1	21794.1	22624.1	23413.5	24146.3	24825.3	45442.5	25993.6	25 99 5 5			27677.3	27785 2	27823.8	
OROPERTIES0	FYCU	30.69.7	3070.8	3074.0	3079.4	3087.0	2100.1	3123.6	3140.5	3166.0	3182.1	3206.9	3234.6	3265.3	7.6625	3377.3	3421.9	3476.5	3523.5	3581.2	3643.8	3711.0	3865.6	3952.3	4.9434	4148.4	423	1.0051	4650.4	+833.8	4.976.5	5151.7	5348.9	5563.4	5797.1	6051.8	9.62.9	0025.00	6963.9	7.22.7	4 10 1 4	8629.2	
COMPOSITE PROPERTIES RHG= .0393 FTU= 16550.0 FCU= 10750C.0 FSU= 600.0	FXCU	A 0 62 5.0	80572.7	83414.1	80144.1	79754.4	7 6 6 6 6 6	: :		75565.1	74180.1	72585.5	70776.7	68755.5	4.0.7.6	61521.3	58789.6	6.94655	53028.1	53169.6	471.7.5	: .	38523.4	35850.5	33303.7	30894.5	28650.4	24546.6	22724.3	21342.7	7.9495.6	18075.6	16775.0	15585.5	1449900	1350 1.0	12003.2	111/00/	11327.2	17342.1		8628.4	
- 0 2	FYTU	0.	4.4	17.6	39.6	4.07	7.011	216.9	284.0	360.5	446.5	545.2	1.199	465.4	1.26.1	1173.7	1332.5	1502.9	1685.2	1879.9	2787.4	2.00.00	2791.6	3.55.5	3334.8	3630.4	3943.0	4673.7	4.993.6	5379.4	5789.7	6222.7	4.6499	7161.2	7669.5	1.512	977.0	9366.3	9998.2	11365.0	12116 3	12889.3	
ER = 4.7006 AR = 4.0006 UR = .3500	FXTU	121875.0	121561.8	120631.1	119108.7	117,35.8	7.004411	108094.6	104432.5	100546.5	96503.3	92364.3	66164.3	20000	75834.7	7189.4	68071.1	64393.8	60859.1	57482.1	54264.4	1.0000	45539.3	42932.7	43468.6	38141.0	23045.8	31914.8	33670.3	28330 . 8	26690.2	25142.8	23683.2	223.5.9	21006.1		17626 7	1.555.1	16491.5	14589.5	715	12887.9	
PROPERTIES .5000 .3931 .0412 .6000.0	UYX	9110.	.6112	. 1120	.6134	.0154		.0247	.029	.0339	.0393	.0454	. 0522	5650		.0856	1960.	.1065	.1181	.1305	.1437	1736	.1882	.2049	.2220	.2412	2000	3035	. 3265	.35.7	.3762	.4031	. 4312	8194.	4919	C#26.	1966.	233	1750.	7123	7552	.7999	
RESIN PROPER VR = .5000 MR = .3931 RHDR= .0412 FSU = .0000	UXA	.2850	.292	.313	.3476	. 3955	0000	.6111	.7.31	.8.28	.9:83	1.0174	1.1278	1.6371	1 . 5430	1.5351	1.6173	1.688.	1.7463	1.7914	1.8232	0740-1	1.8422	1.8259	1.8.62	1.7663	1.7255	1.5280	1.5736	1.5168	1.4582	1.3988	1.3396	1.2795	1.2255	1.1626	1.1056	0 0 0	1966	. 8947	846.7	.7998	
	A ×9	3.822E+05	3.857E+35	3.963E+35	4.14.E+05	4.38 6E+05	A . / U U E + U D	5.526E+35	635E+05	6.60 3E+35	7.229E+05	7.90.9E+05	8.647E+1.5	9.419E+U5	1.11.054.56	1.20 E+06	1.293E+06	1.388E+06	1.486E+05	1.586E+36	1.6865+36	1 90 05 4 00	1.991E+46	2.091E+66	2.191E+06	2.289E+36	2.384E+UD	2.56764 0	2.653E+; 6	2.735E+16	2.813E+36	2.886E+00	4.954E+06	3.617E+06	3.74E+.6	3.1645+00	3.109E+UD	2 27954 6	3.635E+10	3.2815400	7.291F+:0	3.295E+06	
EF = 3.400E+07 EFT= 1.300E+06 GF = 3.500E+06 AF ==2.400E-06	ΕΥ	4.936E+05		4.943E+65	4.952E+35	4.964E+05	4.9005+05	5. J22E+35	5496+05	5. JB. E+05	5.115E+05	5.155E+05	5.199E+05	5.248E+U5	5. 36 . F+f's	5.426E+05	5.497E+05	5.575€+35	5.659E+05	5.751E+05	5.851E+05	5 177540E	6.24E+05	6.342E+u5	6.49.E+05	6. E54E+05	7 215.05	7.228F+ 3	7.452E+05	7.690E+15	961E+C	249E+0	8.562E+05	8.902E+.5	9.2736+05	300000	1. 6 54.6	110000	1.11 E + 40	1.2326+36	1.3016+116	1.376E+06	
.5000 .5269 .0636 .0636 .0636 .215000 .2200	EX	1.2935+.7	1.2925+,7	1.489E+17	1.284E+07	1.2775467	1 25654.7	1.242E+C7	225E+L	1.2.5E+C7	1.181E+17	1.154E+17	1.124E+ 7	1.1915+17	1.115F417	9.729E+L6	9.4884.06	8.832E+[6	8.366E+15	7.895E+16	7.425E+16	200000	6.171E+16	5.651E+. 6	5.25.E+06	4.8735+06	4.217640	3.8786+66	3.592E+16	3.328E+06	3.385E+16	2.8635+16	2.659E+10	2.472E+16	2.501E+15	20113547.2	1.8735+66	1 75454 6	1./242+. D	1.548E+16	1.4585 + 16	1.3768+16	
T T T T T T T T T T T T T T T T T T T	ALPHA	3.0.	1.0			90.		7.0	8.0.	30.6	70.07	11.0	12.0	30.00	15.01				19.6		22.0					20.22									37.00							45.0.	

			AY	.2122E-04	.2121E-04	.2118E-04	.2112E-04	.2104E-84	2082F-04	.2068E-04	.2051E-04	.2032E-04	.2011E-04	.1987E-04	.1961E-04	19025-04	.1869E-04	.1834E-84	.1796E-04	.1755E-84	.1712E-04	.1667E-04	.1519E-04	1517E-04	.1462E-04	.1405E-04	1346E-04	.1222E-04	.1158E-04	.1092E-04	95785-85	.8882E-05	.8188E-05	.7493E-05	. 6800E-05	54.10F-05	4761F-05	.4107E-05	.3472E-05	.2858E-05	.2270E-05	.1179E-05	
			AX	.3087E-06	.3031E-06	.2862E-06	.2583E-06	.2194E-06	1094F-06	.3892E-07	4142E-07	1312E-06	2298E-06	3367E-06	4513E-06	7002F-06	8326E-06	9691E-06	1108E-05	1249E-05	1390E-05	1530E-05	-166/E-05	1924E-05	2041E-05	2147E-05	2241E-05	2379E-05	2420E-05	2439E-05	24335-05	2339E-05	2246E-05	2120E-05	1960E-05	1528F-05	1256F-05	9443E-06	5943E-06	?	.2201E-06	. 5825E-06	
			FXY	3463.1	3675.4	3905.7	4155.7	4427.3	5042.8	5390.7	5768.2	6177.5	6620.7	7099.9	7617.2	8773.4	9415.6	10101.9	10833.3	11609.7	12430.9	13295.6	14201.9	16127.7	17139.0	18175.4	19630.5	21367.1	22432.0	23482.6	25504.5	6457		28207.3	28989.9	30336.9	30894.3	31369.8	31761.2	32066.8	32285.7	32417.2	201010
	ROPERTIES		FYCU	4176.2	4177.1	4179.8	4184.3	4190.7	£.209.3	4221.6	4236.0	4252.7	4271.7	4293.1	4317.2	4377.9	4407.0	4443.5	4483.8	4528.0	4576.6	4630.0	4555.5	4822.7	4.899.5	4983.6	5175.5	5286.6	5407.3	5539.6	5864.5	6017.4	6208.4	6418.0	6648.2	7179.0	7484.5	7820.7	8190.8	8598.3	9047.1	10087.1	1
	COMPOSITE PROPERTIES	RHO= .0459 FTU= 1625CC. FCU= 1175CO.0 FSU= 8GCO.0	FXCU	94062.5	9400106	93817.1	93503.8	93053.6	91695.1	90758.5	89629.7	88293.3	86735.6	84946.1	82918-0	78149.0	75426.1	72501.4	69401.7	66159.5	62811.9	59398.7	55960.	49166.5	45880.5	42707.7	39070.6	34066.8	31518.5	29144.1	24942.5	23039.9	21325.1	19756.5	18324.9		14755.3	13776.0		12081.2	11350.2	10086.3	7.00001
	0		FYTU	6:1	5.1	50 .5	46.2	128.6	185.5	253.1	331.4	450.6	520.9	632.5	1.55.	1037.7	1197.1	1369.3	1554.5	1753.3	1966.1	2193.2	2435.3	2966.5	3256.9	3564.7	2030.0	4699.2	4985.5	5 392.6	5226.5	6754.7	7259.8	7.36.7	8354.8	9573.3	16233.3	16929.6	11664.5	12440.2	13259.2	15037.5	
		ER = .470E+06 AR = .400E-04 UR = .3500	FXTU	142187.5	141822.1	140736.3	138960-1	136541.8	130140.0	126110.4	121837.9	117304.2	112587.2	107758.4	132881.6	93196.7	88473.3	83872.2	79416.3	75122.6	71002.3	4.79679	69356	56342.5	53129.1	50088.2	47.213.4	41934.5	39515.6	37 234.0	13050.6	31138.6	29333.3	27631.3	26023.5	23075.5	21723.7	20446.7	192461	18399.5	17021.1	15035.9	
	RTIES	600 931 412 8000.3	UYX	.5127	.0130	.0138	.0152	.0198				.0358	.0413	5240.	2400.	2696	.0785	.3879	.0981	.1090	.1206	.1331	1403	.1753	.1911	.2079	2443	.2641	.2849	.3069	.3543	.3798	1904.	.4349	64949	5282	. 5623	.5980	.6353	.6743	.7151	9108	•
	RESIN PROPERTIE	VR = .5600 WR = .3931 RHOR= .0412 FSU = 8000	UXA	.2350	.2911	. 30 91	.3391	63865	6667	. 5682	.6491	.7371	. 8309	. 9288	1.0200	1.2274	1.3219	1.4104	1.4912	1.5628	1.6239	1.6736	7777	1.7514	1.7543	1.7467	1.7641	1.6712	1.6322	1.5880	1.4884	1.4348	1.3796	1.3236	1.2673	1.1556	1.1009	1.0473	. 9950	. 9442	. 6950	. 8316	•
	RE		GXY	. 445 3E+66	. 450 JE+06	.4624E+66	. +831E+6 c	54875406	59335+66	.6455E+06	.7050E+C6	.77:5E+C6	. 84485 +06	.9245E+06	.1010E+07	11986+07	.1298E+67	.1404E+07	.1512E+07	.16242+07	.17396+57	18355401	2002-407	.22115+07	. 23296+67	.2447E+C7	26746407	.2790E+07	.28998+67	. 3504E+07	32016+07	.3292E+07	.33786+07	.34576+07	35316+87	36575+67	37096+07	37546+67	.379 LE+07	. 38195+67	. 5840E+67	.3856E+07	
Y -SPACEWIND TIO = .875		EFT = .34CE+06 EFT = .13.E+07 GF = .35UE+07 AF =24CE-96 AFT = .296E-05	ΕΥ	.67192+36	.6720=+16	.67245+36	.6732E+16	67475476	.6771E+06	.6791€+06	.6813€+36	.68402436	•6870€+06	.6904E+06	*034CE+70	-7.32E+06	.7384E+36	.7142E+06	.7236E+36	.7276E+06	.7353=+36	20420420	76325416	.77435+46	.7865E+G6	.7 998E+36	8 30 4 5 4 0 6	.8478E+06	.8669€+46	.88795+06	93615436	.96365+36	.9938=+66	.1327E+37	11.635+67	11475+07	.11965+07	.1249E+07	.1317E+07	372	* 1 443E+07	.1561E+07	
HORNEL 300/EPOXY BER COVERAGE RAT	PROPERTIES	.5100 .6169 .1636 325300.0 21500.0	£X	.150 8E+08	.150 7E+08	.15.4E+68	.1493E+08	14795+08	14665+63	.1450E+03	.143.E+08	.14: 7E+C8	.1361E+08	.1351E+08	131/240	.1238E+68	.1193E+Ca	.1146E+08	.1396E+08	.1343E+08	.9899E+07	93555417	82575407	.7735E+£7	.7218E+67	.6724E+07	57915+07	. 5365E+07	.4360E+07	.4595E+C7	3932E+67	.364JE+07	.3371E+07	. 3120E +07	25975+07	.2510E+C7	.2341E+07	.2187E+07	.2047E+07	.1921E+07	.180 bE+07	.1600E+07	
FIBER	F1859	ARF RHOF FCC UF CF E	ALPHA	90.0	1.00	2.00	30.8		9.00	7.60	9.00	00.6	10.00	11.00	12.00	14.00	15.00	16.00	17.60	18.00	19.00	20.00	22.00	23.00	24.06	25.00	20.02	28.00	29.00	30.00	32.64	33.00	34.00	35.00	36.00	38.00	39.60	00.04	41.00	42.00	20.54	45.00	•

THORN	THORNEL 3'0/E OXY	-SPACEMIND-	1									
6.819	S		RESIN	IN PROPERTIES	TIES		0	COMPOSITE PROPERTIE	OPERTIES			
	. 500 . 606 3 25 2150	EFT= 3.400E+05 EFT= 1.300E+06 GF = 3.500E+06 AF =-2.400E=07 AFT= 2.960E=06	E+07 VR E+16 MHOR E+06 MHOR E-07 FSU	= .500c. = .3931 R= .0412	•	ER = 4.700E+05 AR = 4.000E-05 UR = .350		RHO= .0524 FTU= 16250.0 FCU= 107500.0 FSU= 8300.3	J 0 0			
	3727	<u>.</u>	¥ X 9	UXV	×An	FXTU	FYTU	FXCU	FYCU	FXY	AX	AY
ALPHA	2.4	,					•		. 65.63	1.062.7	13	1.857E-09
	1.7256+47	8.775€+25	356+	.2856	.0145	162500.0		107630.6	5452.7	t t		1.856E-05
	1.72254.7	8.776€+05	. 143E+1	.2903	.0148	162082.4	6.60	1 220	5454.6	0.991	2.891E-07	1.8546-0
	1.71 8: +0.7	8.7796+45	. 28 bE+3	.3063	.0150	160841.4	500	1.69637	5457.7	4753.2		1.850E-0
	1.712F+(/	8.784E+15	5.523E+15	.3567	. 6171	158811.6	25.0	1.0003.1	5462.2	90	2.3066-07	1.844E-0
	7. 45 + 6	8.7916+35	5.8532+65	.3692	.0191	156,47.7		1.5525	2.68	5465.2	1.8705-07	1.837E-0
	1.0916+67	8.80 E+05	6.2755+35	.4156	.0216	152621.6	200	1020701	2722	5775.5	. 341E	1. 429E-0
6.0	: .676E+L7	8.811E+05	6.780E+.5	.4714	.0248	148617.6	280.2	103771.8	54840	6178.5	7.197E-08	1.818E-0
7.5	1.058E+. 7	8.825E+15	_	.5357	. 0285	144160.5	378.7	102511.6	5494.3		1.008E-09	1.806E-0
30.0	1.6365+67	8.84.6+ 5		.6078	.6353	139243.5	4 5 6 7	101,24.9	5506.4		-7.853c-08	1.7936-3
9.0	1.61.E+C7	8.86 E+05		. 6600	. 6378	134001	5.995	99297	5526.3	7608.1	0	1.777E-0
20.01	1.581E+17	8.882E+05		. 1713	00000	120011	722.9	97315.8	5536.3		-2.618E-07	1.760E-0
11.0	1.547E+07	8.936E+15	1.15 AE+05	.0601	6647	117579.	863.6	95073.3	5554.4	8768.6	0	1.741E-0
12.00	1.57 9E+17	8.9352+05		. 477	638	1120140	1.17.9	92566.7	574.	9417.6	-4.741t-07	1.720E-0
.3.0.	46RE+[7	8.907E+U5		1.4557	0171	106510.6	1185.9		6.2655	10114.7	-5.897E-37	1.6985-0
70.97	1.422E+(7	9. 035.03	7.8.7	1.2248	08.7	101112.4	1368.1	~	5623.8	13861.3	-7.10/E-U/	1.67.55
15.6.	1.372E+17	9. 4364.5	1.50	1.3035	2060		1564.9	8353	5652.9		-8.301c-u	1.6176-0
16.0	1.3195+67	9.0020.00	1.73	388	.1004		1776.6	8008	5685.4		2000-6-	1.586F-0
30.71	1.2635+1	3.14 E	• -		.1114		2.03.8	m (5721.6	13404.0	-1.2295-06	1.553E-0
	1 16.55	9.26 5+115	1 .4	1.5217	.1231		2246.9	72692.1	1.2976		-1.362:-46	1.517E-0
2.0	1. 835 4. 7	9.331E+05	2	•	.1356	76642.8	2506.5	٠ ۵	5 697 3	16 390 . 4	-1.4935-06	1.480E-0
21.00	. J21E+C	9.409E+05		ä	.1489		2022	25019	5913	17474.0	-1.6218-06	1.440E-0
24.0.	9.5316+:6	9.497E+15		-	.1631		3393		5975.	18595.3	-1.745E-06	1.397E-0
23.0	8.3816+66	9.594E+65	(V	1.6673	.1781	60719	3722.2		6143.9	19748.9	-1.861E-05	1.353E-0
24.00	8.335E+Co	9.70364.5	•		2100		4073.9	49711	6125.4	20928.5	-1.969E-36	1. 30 be - u
.5.6	. d. Ac+.	9.8235+35	• •	1.6602	2281		4.9444	46181.	6235.2	22126.9	-2.00bt -ub	1.2965-1
0.07	7.2525+10	9.95/E+15	, w	1.6477	.2475		4840.5	42815.9	6299.5	235350	-2.2187-06	1.1516-0
28.0	6.23 F+LF	27E+36	3	1.6217	.2673	3	5257.3	59655.3	652	25750.6	-2.269E-06	1. 35E-I
29.60	5.7032+.6	1. 45E+06	M	1.5890	. 2882		6162.9	33848.2	6648.7	26937.0	-2.298E-05	1.038E-(
50.0.	5.327E+ 6	1 ofE + u6	m	1.5569	. 5102	7 .	6654.1	31254.	6791.5	28096.2	-2.334E-06	9.782E-
31.0.	4.922E+. 6	1. 88E+16		1.50001	35.78	, ~	7172.6	"	6.6469	29218.4	-2.284=-06	9.171E-
32.06	4.547E+. 6	1.113E+06	3.66 124.0	٠,	3834		7719.7		7:25.7	33293.9	-2.236E-36	8.54/E-
33.0.	4.207E+C6	1.1416+65		1.3615	.4163		8296.9	"	7320.7	31313.7		7 2675-
34.01	3.887E+16	1.1/cE+UD	0 10	•	4386		6.5068		7537	32269.4		6 648F
35.0.	3.598E+(6	1. 2000 + 00	2 -7	•	.4682	2	9548.3		1777.1	33153.3		5.96.7F-
35.01	6.195F+.6	: -	4-124E+C	-	. 4993		1,226.3		6045.5	33930.0	-1.4885-06	5.319E-
	2.878F+L6	1. 332E+u	,	1.1	. 5318		1094.		8667 3	35 31 3.4		4.676E-
20.02	2.58154.6	: :	4.252E+3	1.0961	. 5658		11695.2	10961	2.12.0	15454		4 4 3E -
	2.5.2E+LD	-	4.30 3E+6	-	.6614		12221	•	94.46	36299.8	-5.8095-07	3.425E-
41.0	2.3416+6		4.340E+		.6386	21980.0	16217.4	•	6.1886	36648.2	-1.990E-07	2.824E-
42.3.	.19	1.576E+0	4.379E+0	9436	7177		15153.3	12	10383.3	36898.1	2.212E-07	2.246E-
43.06	.364€+1	1. 054E+ 06	4.402E+J		7597	-	16141.7	1223.	10936.5	37.48.3	6.782E-37	1.69 3E -
0.44	1.945E+Cb	1.7415+06	4.41 /E+Ub	•	8.34	•	17185.7	11549.5	11556.5	17098.3	1.170 = -06	1.169E-
45.00	. 838E+C	1.9386+45	4.421E+	•								

 $\begin{array}{c} c_1 \\ c_2 \\ c_3 \\ c_4 \\ c_4 \\ c_5 \\ c_6 \\ c_6$ COMPOSITE PROPERTIES 1447474 1447 152500.0 3500.0 80.00.0 $\begin{array}{c} \mathbf{c} \cdot \mathbf{c} \cdot \mathbf{c} \cdot \mathbf{c} \\ \mathbf{c} \cdot \mathbf{c} \cdot \mathbf{c} \cdot \mathbf{c} \\ \mathbf{c} \cdot \mathbf{c} \cdot \mathbf{c} \cdot \mathbf{c} \\ \mathbf{c} \cdot \mathbf{c} \\ \mathbf{c} \cdot \mathbf{c} \cdot \mathbf{c} \\ \mathbf{c} \\ \mathbf{c} \cdot \mathbf{c} \\ \mathbf{c} \\ \mathbf{c} \cdot \mathbf{c} \\ \mathbf{c} \\ \mathbf{c} \cdot \mathbf{$ FTU= FCU= FSU= 4.700E+05 4.000E-05 .3544 E B B B 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0 PROPERTIES .500, .4402 .1412 8606.0 KHOK ... RESIN EFF = 1.90 CE + 00 GF = 3.00 CE + 05 AFF = 3.00 CE + 05 AFF = 3.00 CE - 06 AFF = 3.00 CE - 05 4 1 1 4 1 4 1 4 1 4 1 4 1 4 1 4 4 4 4 1 4 1 4 4 4 4 1 1 1 1 4 KEVLARZEPOXY -SPACEMIND-FIFER COVERAGE RATIO = .250 FIBER PROPERTIES VF = .5590 NF = .5598 HOFE .3524 FCU = .3550.0.0 UF = .220.0 X ALPHA

			*	.7895E-84	.7889E-04	.7846E-04	.7807E-04	.7758E-04	.7698E-84	.7546E-04	.7455E-D4	.7352E-84	.7239E-04	.7115E-04	. 6983E-84	.6687F-04	.6525E-04	.6354E-14	.6174E-04	57885-14	. 5583E-84	.5371E-84	. 51 52E-04	.4927E-04	.4461E-04	.4221E-04	3978E-84	.3484E-04	.3234E-04	.2985E-04	24ARF-04	.2243E-84	.2002E-04	.1765E-04	13035-04	.1066E-04	.8773E-05	.6749E-05	-4619E-05	.1263E-05
			AX	9861E-06	1008E-05	1184F-05	1336E-05	1530E-05	1765E-05	2349E-05	2694E-05	3072E-05	3479E-05	3912E-05	4368E-05	5333E-05	5834E-05	6340E-05	6847E-05	7349E-05	8316E-05	8769E-05	9193E-05	9581E-05	1022E-04	1047E-04	1064E-04	107 8E-04	1073E-04	1059E-04	10 35E-04	9574E-05	9021E-05	8354E-05	- 666 96-05	5645E-05	4500E-05	3235E-05	1851E-05	3496E-05
			FXV	505.9	537.9	61102	653.2	699.3	749.9	866.6	933.6	1007.3	1088.0	1176.6	1273.5	1495.1	1620.8	1757.2	1904.5	2023.1	2413.2	2604.0	2004.2	3012.3	3445.7	3666.6	3886.8	4314.5	4516.5	4707.6	5062.0	5196.6	5328.1	5443.1	2505.6	5694.2	5748.8	5790.3	5819.4	5842.2
	OPERTIES		FYCU	365.8	385.9	387.1	388.1	389.4	391.1	395.3	397.9	6.004	F. 404	0.00	412.1	421.7	427.2	433.2	439.7	0.044	463.0	472.1	482.0	492.7	517.0	530.7	545.5	579.1	598.1	618.7	665.5	692.1	721.0	752.5	8000	965.6	910.5	959.7	1313.7	1137.9
	COMPOSITE PROPERTIES	RHO= .0176 FTU= 162500.0 FCU= 35001.0 FSU= 6000.0	FXCU		13116.3	•	-		12774.4															5652.0			4066.3												1287.7	1137.8
		9)+3	FYTU	0	1.7	15.7	28.0	43.8	63.2	113.6	143.4	177.6	215.7	257.8	333.9	408.6	467.5	530.9	239.0	749.7	832.7	921.2	1015.2	1115.0	1333.2	1452.1	1578.9	1851.9	20002	2158.0	26.99.9	2685.5	2881.6	3088.7	1510.2	3783.8	4042.6	4316.4	1.606.0	5:28:5
		ER = .477E+C6 AR = .400E-C4 UR = .3500	FXTU	60937.5	60740.7	59208-0	57925.1	56350.2	54530.7	50358.6	48103.5	45794.5	43469.3	41159.6	36891.0	34552.8	32568.8	30558.5	28705.7	26296.3	23737.1	22271.3	20895.3	19604.8	17262.4	16201.6	15238.2	13406.9	12590.7	11825.9	111106.9	9815.4	9213.0	8656.5	7641.5	7178.7	6743.0	6332.5	7.446	5236.9
	RTIES		N.A.	.0384	.0087	.0110	.0130	.0155	.0187	.1268	.0318	.0374	.0436	*050.	. 0661	0 750	.0846	6460.	.1060	1179	1 440	.1584	.1736	.1898	.2252	.2444	2867	.3388	.3327	.3580	. 4126	.4421	.4731	.5059	5765	.6145	.6545	9969.	7787.	.8355
	ESIN PROFERIIES	VR = .5036 WR = .4432 RHOR= .0412 FSU = 8369.0	UXA	.2850	2222	3683	.4320										1.8843				2.1706	2.1758					1.9451				1.5198							6766.		.8354
	3.		GXY	.85815+05	. 8684E+05	. 950JE+05	.10215+06	.1112E+06	. 1222E+60	.1497E+06	.1661E+Cô	.1841E+06	. 2C 38E+66	90+36+22.	27115+66	.296CE+66	. 3219E+16	.34872+66	.3762E+C6	9945454	.4622E+06	.49152+96	.52082+06	.55012+06	.60785+66	. 6362€+66	. 66362+35	.71632+46	.74123+66	. 76495+C6	8 85 4 5	.8281E+06	.8462€+66	. 86255.	39015406	90112+68	. 9102E+LD	.91735+56	925232416	. 92645+00
KEVLARZEPOXY SPACEWIND- FIBER COVERAGE RATIO = .375		EFT = .190E+08 EFT = .100E+07 GF = .300E+16 AFT = .333E-04	ΕΥ	.1075E+36	.1076E+06	111795+66	.13825+06	.1,86E+36	1109621.6	.11025+06	.1109E+36	.1117E+36	.1127c+36	.1137=+36	11645456	11755+36	.119u E+06	.12575+-6	.1225E+ 36	12665496	12895+06	.13145+36	.1342E+06	.13726+05	14392+06	.1+776+36	15182+06	16105+06	.15632+36	.17205+06	13495436	.19226+36	.2.02£+36	.23895+36	9145867	.24.15+06	.25255+16	.2666.2+36	20426382	.315uë+06
RZEPOXY SI	BER PROPERTIES	.59.0 .5598 .0524 325600.0 76000	EX	.36515+07	36485+07	36265+67	.36062+07	.3576E+L7	35+36+67	.3+47E+G7	.3385E+07	.3311E+07	.3227E+67	. 31 31E+17	. 39 25E+U/	2783E+07	.2651E+07	.2513E+C7	.2371E+C7	2 8 45 + C 7	. 1943E+07	.1836E+C7	.1674E+C7	.1547E+[7	. 1316E+C7	.1212E+17	11156+07	94405+66	· BOSCE+C6	· 8 · . 4E + C 6	6411F+16	.6295E+16	.5827E+C6	.5432E+66	46666	.4349E+16	.4061E+06	.3799E+£6	3552E+U6	.31506+66
KEVLA FIBER	FIBER	RAHOF	ALPHA	0.00	1.03	3.00	4.00	5.00	0.00	60.0	9.00	10.03	11.00	12.00	14.00	15.00	16.00	17.00	18.00	23.00	21.00	22.00	23.00	24.00	26.60	27.00	28.00	30.00	31.00	32.90	34.00	35.00	36.00	37.09	00.00	49.00	41.00	42.03	200	45.00

FIBER	FIBER PROPERTIES		RES	RESIN PROPERTIES	RTIES			COMPOSITE PROPERTIES	201			
MF RHOF	. 5460 . 5598 . 6558 . 3550.0 . 74533.6	EF = 1.9002+07 EFT= 1.000E+06 GF = 3.000E+u5 AF =-2.006E-06 AFT= 3.30E-05	E+07 VR E E+06 MR E E-06 KHDR:	= .5660 = .4402 R= .0412		ER = 4.700E+05 AR = 4.409E-05 UR = ,3540	50 05	RHO= .0234 FTU= 162500.0 FCU= 35000.0 FSU= 8000.0	•••			
ALPHA	Ex	ΕΥ	GXY	UXA	XAN	FXTU	FYTU	FXCU	FYCU	FXY	¥	*
0.03	*** 867E* 65	1.9125.425	1.1446+65	.2856	. 6112	81254.0	3.		685.3	676.3	-9.861E-07	5.92
1.00	4.864E+.6	1.912E+15	1.158E+15	.2921	.0115	9.7961.8	2.3		685.4	718.4	-1.003E-06	5.918E
2.0.2	4.8536+66	1.9135+35	1.1996+05	.3132	.0123	80209.7	9.3		685.7	765.0	-1.053E-36	5.910E
3.6.	4.435E+C6	1.914E+05	1.c67E+J5	.3482	. 6130	78944.6	21.0		686.1	810.6	-1.135E-06	5.897E
	4.4.9E+16	1.916E+65	1.362E+65	.3967	.0158	77233.5	37.3	-	686.8	873.8	. 251E-0	5.878E
	72864.6	1.9105+05	1.4846+65	2654.	1216	72747 6	36.4	17193.1	997.0	937.0	-1.398E-UB	5.834E
7.5.7	4.673£+1.6	1.325E+05	1.00.46+05	6169	0520	70022.5	115.3		6.689	1084.4	-1.788F-06	5.78
3.00	4.6.7E+16	1.929E+05	2.00 JE+05	.7119	. 298	67144.9	150.6	-	691.4	1170.0	-2.028E-06	5.74
30.6	4.52AE+06	1.9336+45	2.223E+u5	.8155	.6348	64134.0	191.2	1637	693.2	1264.4	-2.298E-36	5.70
10.60	4.437E+.6	1.939E+u5	2.462E+05	.9258	.0465	61059.3	236.8	-	2.569	1368.6	-2.595E-06	5.64
11.00	4.3332+16	1.345E+C5	4.7262405	1.0439	.:467	57959.1	287.6	15710.3	697.5	1483.3	-2.913E-u6	5.5918
76.31	4.21764.0	1. 35.5.4.5	3 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1.1565	.0537	24879.4	2000		1.00/	1009.3	-3.20/E-UB	302606
14.00	3.4396+16	1.46964.5	3.57 MF+15	1.5963	2100.	48911.7	472.2	16359.1	706.3	E . 808 .	-4-030F-06	5.1775
15.30	3.783E+.5	1.3/35+05	3.362E+12	1.4997	.0785	46070.5	544.8		709.9	2362.8	-4.439E-06	5.292E
16.0.	3.616E+66	1.39.2.62	4.30 9E+35	1.00.14	. 4882	43345.1	623.3	-	714.1	2241.4	-4.865E-16	5.201E
17.0.	3.4 6	2.1032+35	4.66 dE+ US	1.6931	9860.	40744.7	707.3	-	718.6	434.	-5.302E-06	5.10 3E
33.65	3.2386+16	4 17E+55	5 38E+15	1.7731	.1398	_	798.6		723.7	2641.8	-5.748E-06	66.4
	3.3722+16	436E+.5	5.416E+.5	1.8398	.1217	35935.8	895.8	11241.5	759.4	2863.7	-6.198E-06	4.885E
21.00	2.5925410	2. 6.5.6.6	5.601E+05	7769.1		33766.5	1116.3	0026.8	74.5 7	3.99.0	7 0055	7. 6.795
22.3.	2.512E+06	2.9.E+.5	6.582E+L2	1.9538	1626		1228.2	92.2.2	756.4	3609.4	-7.532E-06	4.502E
23.3.	2.3315+.6	2.1146+05	6.4705+15	1.9633	.1780	27863.4	1353.6		759.0	3883.6	-7.953E-06	4.359E
20.47	2.159846	2.14.E+55	7.364E+C5	1.9595	.1943	26139.7	1486.7		768.5	4159.8	-8.352k-06	4.209E
25.66	1.992E+16	2.1096+05	7.728c+.5	1.9437	.2116		1627.9		779.0	2.9979	-8.722E-06	4.05
.0.62	1.9356+15	2.261E+15	8.142E+.2	9172	6627	23016.6	1777.6	0721.3	7.067	4732.5	-9.657E-06	3.88
28.65	1.55. 64. 5	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	0.52.64.5	1.8378	2642	20277.6	2103.9	567.3.5	818.	5 506.3	-9.549E-06	3.5336
29.00	1.4235+16	2.3196+05	9.2495+.5	1.7877	.2913	19037.3	2281.5	5234.6	633.9	5581.8	-9.77GE-36	3.347E
33.0.	3. 5E+Co	2.367E+05	9.597E+35	1.7326	. 3141	17875.7	2469.2	4772.5	851.4	5849.8	-9.883E-36	3.155E
31.00	1.1346+66	2.42.4.5	9.933E+35	1.6735	.3381	16787.6	4.667.6	4376.1	879		-9.9195-06	2.957E
32.00	1.10,E+C6	2.48.E+65	1.12554.6	1.6117	.3635	•	2877.4	4014.0	892.5	6345.7	-9.871E-35	2.754E
33.4	1.01. 54. 5	2.5405+05	155E+.0	1.5461	1062	811.	3099.0	3684.5	916.5	6569.3	-9.729E-06	2.547E
3	9 50 75 75 75	20175102	4035.60	1005.1	7014	13913.3	30000		340	200	904061	2 . 2 3 2 5
36	7.3875+12	2.19. 6.05	1.1346	1.3539	.4789	12284.2	3642.1	2874.1	1005.1	7125.2	-8.666E-16	1.909€
37.36	7.28 DE+ 5	2.484E+25	1.156E+06	1.29.1	.5115	11542.0	4118.3		1641.4	7272.2	-8.077£-36	1.695E
39.00	6.745E+.5	3.00.5+.5	1.1756+00	1.2274	.5459	13844.5	4411.3	8.	1081.6	7398.6	-7.363E-06	1.481E
30.65	6 41.45.45	3.122=+05	1.1936+36	1.1661	. 5819	10188.7	4718.9		1126.3		-6.5191-36	1.270E
, , ,	5.47 764.3	3.41 14.5	1.27 1.466	1.04.02	6610.	400 F	5342	1966.7	1231.2	7666.2	439F-0	8.601F
42.00	5.1692+45	3.5796+35	1.229406	. 4929	.7411	8443.4	5755.1	1836.8	1292.6		-3.203E-06	6.637E
45.0	4.7496+05	3.7606+35	1.4365+36	1626.	.7446	7.7267	6141.4	172	1360.9	1759.2	0	4. 748E
44.0	35.46	3.974E+US	1.24.E+16	.8874	7962.	441	6550.3	1615.4	1436.9	7782.1	-3.565E-07	2.945E
30.54	** 2655 + 65	4.260E+35	1.241E+36	.8377	.8378	6982.6	6983.3	-	1521.5		1.2426-06	1.240E

			AY	4737E-04	47355-04	なは一川からんな。	2017年日1日本で、		*4655E-04	* 4643E-04	4617E-B4	45546-34	.4516E-84	· 4475E-34	.4429E-04	* 4379E-04	40000000000000000000000000000000000000	.4198E-84	.4127E-04	*4049E-04	3966E-04	37785-94	.3673E-84	.3561E-04	34462110	. 3178E-84	.3035E-04	.2883E-B4	.2557E-06	.2382E-04	.2202E-04	. 20165-04	.1630E-04	.1433E-04	.1236E-04	.1038E-04	. 8436E-85	.4679E-05	.2903E-05	,1217E-05
			AX	9861E-06	000000000000000000000000000000000000000	110 SE-05	000000000000000000000000000000000000000	14545100	-,1635E-05	-,1831E-05	2052E-05	- 2566E=05	2858E-05	3170E-05	3503E-05	-,38555-05	4606F-05	5001E-05	-,5406E-05	5816E-05	-,6229E-05	7045E-05	7437E-05	7810E-05	8474F-05	8749E-05	8974E-05	9140E-05	- 92566-05	91868-05	9817E-05	-,8739E-05	7823E-05	7170E-05	6379E-05	- 544 9E-05	4379E-05	1830E-05	3633E-06	.1220E-05
			FXY	347.4	0.99%	1023.0	1095.7	1267.3	1367.9	1479.6	1503.5	1891.6	2057.8	5539.9	2438.8	2654.9	3140.6	3410.0	3696,6	3999.2	4316.5	4987.0	5335,0	5687.5	6 392.0	6736.8	7072.0	7394.2	7983.6	8256.3	8502.2	8725.3	9101.8	9255.4	9386.4	9.6546	9583.7	9699.1	9727.6	9737.0
	OPERTIES	500 * • • • • • • • • • • • • • • • • • • •	FYCU	1370.0	1070.0	1069.9	1069.8	1069.6	1069.5	1069.4	1069.4	1069.6	1069.9	1070.3	1070.9	1071.7	1074.3	1076.1	1078.4	1081.2	1084.6	1093.7	1099.6	1106.5	1124.7	1135,3	1148.1	1162.9	1199.6	1222.1	1247.8	12/102	1348.8	1392.2	1441.4	1497.2	1560.4	1712.8	1804.1	1907.2
	COMPOSITE PROPERTIES	RHO= .0293 FTU= 162500 FCU= 35000	FXCU	21875.0	21860.6	21743.4	21637.4	21318.2	21098.4	20833.4	20519.5	19731.6	19252.4	18714,8	18119.4	17468.5	16018.2	15232.2	14417.2	13583.1	12740.2	11069.3	10260.3	9479.8	8034.0	7365.1	6747.4	6175.6	5168.0	4729.5	4331.6	3972.0	3356.7	3095.6	2862.0	2653.4	2467.3	2154.3	2023.3	1967.0
			FYTU	0	2 * 2	26.2	46.7	105.4	143.8	188.3	239.0	359.5	429.6	506.5	530.5	681.0	384.8	998.3	1119.7	1249.5	1387.9	1692.0	1858.4	2034.9	2420.2	2629.9	2351.8	3086.5	3534.0	3873.8	4166.5	4412.0	5147.9	5512.8	5898.6	6336.4	7137.1	7676.7	8187.8	8729.1
		AR # .4470E+06	FXTU	111562.5	131234.5	98679.9	96541.8	95917 00	87528.1	93931.1	80172.5	3054608	5.8599.3	54818.4	61139.6	57588.1	5 TO 3 TO 5 S	47842.9	44919.7	42163.4	39561.8	34825.5	32674.6	30658.9	22002.6	25347.0	23796.6	2234407	19709.8	18514.9	17394.1	16342.4	1030000	13555.7	12735,9	11964.5	11238.3	9.6066	9301.7	8728.2
	RTIES	0.0	UYX	.C140	.0143	.0166	.0187	.0245	. 6283	.0328	.6379	00000	.0569	.0645	.0729	. 1819	1022	.1135	.1256	.1385	.1522	.1658	.1988	.2162	2546	.2747	*5864	* 3194	3689	.3957	. 4238	.4534	. 5172	. 5514	.5873	.6249	. 6643	7485	. 7933	.8401
	ESIN PROPERTIE	VR = .5000 WR = .4492 AHOR= .0412 FSU = 8500	UXY	.2850	2007	. 3361	*3754	* \$7.00	. 5551	.6334	* 7194	. 9091	1.0098	1.1118	1.2134	1.3124	1.4044	1.5737	1.6431	1.7014	1.7477	1.8032	1.8127	1.8107	1.7761	1.7454	1.7076	1,6638	1.5627	1.5073	1.4503	1.5915	1.2733	1.2147	1.1558					
	SE SE	*190E+08 ** *300E+08 ** *300E+08 ** *300E+08 **	SXY	.14302+06	*14475456	.15852+06	.17655+06	3.4254CF	.2259E+06	.25066+06	*2783E+16	34185+06	.3773E+L6	. 41522+f6	.45525+06	.49715+06	100000000000000000000000000000000000000	.632+E+06	99+36€19*	.72835+66	.77725+66	. 8763E+15	.92535+06	.97422+06	10713417	11175+07	.11525+07	.1205:+57	1787517	.13255+07	.13615+47	.13945 +07	14675417	.14775+07	.1498E+C7	.1517E+07	.19325+07	13515+67	19585+07	.15595+07
SPACEWING-		GF = 1000 AF = 1300 AF = 1300	¥	*2987=+36	.2987±106	.29875+56	.2387E+u6	2986240	.23855+36	.23852+36	29852+36	2485=+05	.2985E+56	.29862+36	*2987=+06	.29892+06	91417667	33005+06	.3Ju65+36	.3114E+16	.3.22=+16	31475416	.3362E+66	.3381E+36	31035+06	31586+06	.3193E+06	.32332+36	36735+36	.3394E+36	34645+36	.3544E+16	37 30 50 E + CO	.34582+06	.3992E+26	· 41445+06	.43172+36	.4733E+06	.4982E+06	.52635+36
KEVLARZEPOXY SPA	PROPERTIES	. 55244 32554 7250 7250 7250 7250	×	13434019.	*6385E+07	.60+36+67	.6JI1E+07	. 591 3F+17	. 5846E+07	.57668+07	.5673E+117	. 544:1407	. 53.0E+C7	*51456+67	19434264	.4789E+07	-4230E+07	.41605+67	. 3934E+07	.37.3E+C7	*3471E+67	.3240E+C/	.2793E+U7	.258JE+67	.23/8E+U/	.2007E+07	.1839E+C7	*16845+17	-14125+C7	.1293E+27	.1185E+C7	*1088E+67	. 933/E+LO	.8498E+16	.7863E+86	.7296E+16	. 67 89E+16	.5937E+C6	.558JE+06	.5263E+C6
FIBER	F1863	RAT RHOUND TO THE STATE OF THE	ALPHA	0.00	1.00	3,00	50.7	5.00	7.00	8.00	0.6	10000	12.00	13,67	14.50	15.30	17.00	18.00	19.00	20.02	21.03	23.00	24.00	25.00	27.00	28.00	29.60	30.00	32.60	33.00	34.00	35.00	37.00	38.00	39.00	40.00	41.00	10.54	20.44	45.00

3.99476 - 05
3.99476 - 05
3.99466 - 05
3.99466 - 05
3.99466 - 05
3.99466 - 05
3.99466 - 05
3.99466 - 05
3.99466 - 05
3.99466 - 05
3.99466 - 05
3.99466 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 - 05
3.9946 19.99.973E-07.11.031E-07.11.031E-07.11.031E-07.11.0331 1019.4 11230.3 1230.6 1319.0 1439.0 1455.7 1765.7 1765.7 1765.7 1765.7 1765.6 1775.6 1 COMPOSITE PROPERTIES 1539-7 1539-0 1539-0 1539-0 1538-5 1538-5 1538-5 1538-5 1538-5 1538-5 1538-5 1538-5 1538-5 1498-6 14 152506.0 35000.0 8000.0 FXCU F10= F20= FSU= 4.700E+65 4.000E-05 121475.0 112414.6 1126114.6 1126114.6 1126114.6 1126114.6 112612.2 112612.2 112612.3 12612.3 12612.3 12612.3 12612.3 12612.3 12612.3 1266.8 . . . CAR 01171 01171 01171 01171 01171 01171 01171 01171 01171 01717 PROPERTIES .5600 28958 330898 WR #R # RESIN 11.746F + 1.0746F + 1.0746F + 1.0746F + 1.07477 + 1.0747 EFT = 1.900E+06 GF = 3.000E+05 AF =-2.300E-06 AFT= 3.300E-06 KEVLARZEPOXY -SPACEWIND-FIBER COVERAGE RATIO = .750 PROPERTIES .5400 .0524 3250.4.6 73000.6 EX WF #F FIBER ALPHA

			AY	.3383E-84	.3383E-04	. 5562E-04	1	.3372E-04	.3367E-04	3350E-84				.3309E-04	.3293E-04	. 3276E-04	3234E-04	.3210E-04	:	.3150E-04	30765-04	:	-	-	. 2870E-84	.2730E-14	.2648E-84	2461F-04	.2354E-84	.2237E-14	.2112E-14	.1831E-04	.1678E-84		.1347E-04	.1172E-D4	84245-02	.6324E-05	.4548E-05	.2823E-05	.11736-15
			AX	9861E-06	9957E-06	1025E-05	1140F-05	1226E-05	1332E-05	1457E-05	1765F-05	1947E-05	2148E-115	2368E-U5	2606E-05	2862E-05	3425E-05	3731E-05	4051E-05	4384E-05	50 A 2F - 05	5442E-05	5804E-05	616 5E-05	6521E-05	7192E-05	7493E-05	7986F-05	8157E-05	8263E-05	6291E-05	8 06 3E - 05	7781E-05	737 0E-05	6820E-05	6123E-05	- 55 1 2 E - U 5	3112E-05	1811E-05	3762E-06	.1176E-05
			FXY	1192.2	1263.8	1545.4	1543.6	1662.7	1796.9	1947.5	2303.8	2512.1	2742.1	5394.9	3271.3	3571.9	4246.2	4619.1	5014.6	5431.1	6448.9	6782.6	7256.8	7736.5	8217.6	9167.1	9627.0	100011.7		11282.0	11635.5	12257.5	12524.5	12761.8	12969.4	13147.8	13697.4	13512.4	13578.9		13631.9
	ROPERTIES	000	FYCU	2094.2	2093.9	2602	2088.2	2084.8	2080.7	2075.8	2064.1	2057.3	2049.9	2041.9	2033.4	****	2005.3	1995.3	1985.1	1974.9	1954.6	1944.8	1935.5	1926.8	1919.0	1906.9	1983.2	1901.5	1985.7	1912.5	1923.2	1958.8	1985.2	2010.6	2059.8	2170.1	2242	2328.9	2429.8	2547.8	2685.1
	COMPOSITE PROPERTIES	RHO= .0410 FTU= 162500. FCU= 35000. FSU= 8000.	FXCU	33625.0	30604.9	30 244 .4	30296-4	30104.6	29863.4	29569.3	28806.3	28329.3	27783.8	27166.7	26476.3	25,12.0	23967.9	22995.9	21966.2	20867.6	19627.8	17471.6	16315.2	15171.5	12969.1	11930.5	10944.1	9148.6	8345.3	7606.2	6930.5	5761.8	5262.9	4816.5	4418.7	4065.7	27.30	3237.9	3027.3	2843.9	2684.9
			FYTU	0.1	4.1	16.3	65.4	132.3	147.5	201.3	334.6	414.5	503.4	601.5	709.0	826.3	1090.8	1238.8	1397.6	1567.6	94.3.1	2149.4	2368.8	2 601.7	2 8 4 8 . 8	3388.2	3681.9	3992.6	4.668.4	5035.4	5423.3	6266.1	6723.6	7207.1	7718.0	8258.0	0.6290	10071.5	10747.4	11463.0	12220.8
		ER = .47CE+06 48 = .400E-C4 UR = .350C	FXTU	1,2187.5	141728.2	140 567.0	135158.6	131483.8	127238.3	122539.3	112241.5	106853.9	101428.4	96039.0	90745.7	85595.5	75853.9	71303.2	66980.0	62887.6	55386.6	51966.5	48755.7	4.5744.4	42922.4	37803.6	35485.8	33315.3	29378.3	27593.8	25 920 . 8	22879.3	21497.0		18978.0	17830.2	16727	14775.9	13873.4	13022.4	12219.5
	RITES	· ·	×¥n	.0196	.0199	. 0 2 0 8	.0243	.0270	.0303	. 1342	0630	2640.	.6562	.0633	. 0711	9670.	0000	.1095	.1210	.1333	1041.	.1752	.1910	.2377	22253	.2638	.2846	3798	.3541	.3797	1964	9494	14957	. 5282	. 5623	6365	.6330	.7141	.7560	*662	. 8444
	RESIN PROPERTIES	WR = .5330 WR = .4432 RHOR= .0412 FSU = 8300	UX¥	.285.	.2892	.3016	3569	.3876	. 4318	.4833	6162	.6763	.7511	.8296	. 9167	. 9931	1.1562	1.2341	1.3075	1.3752	1.4558	1.5323	1.5662	1.5906	1.6054	1.6068	1.5945	1.5479	1.5152	1.4775	1.4356	1.3428	1.2933	1.2425	1.1911	1.1396	1.0002	4286	.9385	1068.	. 8443
	RE	.190E+08 VR .100E+07 WR .300E+06 RH0 200E-05 FSU	6×¥	.2132E+66	.2027E+06	.210.5+66	23915+05	. 26975+06	.2869E+36	.3175E+06	39165406	43475+66	.4815E+06	. 53196+66	. 58545+60	.642 E+00	76315+06	.82715+56	.89282+06	.960 LE+06	1.985417	11665+67	.12385+07	.1307E+07	.1377E+C7	15125+07	.1578E+07	15425407	.1763E+07	.1820E+07	.1873E+67	. 1970E+67	.2L13E+67	.2053E+07	.2087E+07	.21185+07	21666407	. 2183E+C7	.2195E+07	.2202E+07	. 22758+67
SPACEWIND- RATIO = .875		GF = .190 GF = .333 AF =200 AFT = .333	£Y	.5855€+36	.58545+66	.58512+36	54386416	.5428₹+36	.58162+36	.58.2E+06	57695+36	57495+16	.5727£+36	.57045+36	. 5680E+66	.5654E+36	5598 + 16	.5569E+36	.55392+06	.5509€+36	54675466	.5421E+66	.53932+36	.5367E+36	53442+56	.53062+36	.52946+06	5287E+36	.5293€+16	.53162+06	.53362+06	.54292+36	.54995+66	.5588E+16	. 5698E+36	.5833E+06	410454.6	64236+36	·6696E+06	.7.15E+16	.73862+06
KEVLARZEPOXY SP IBER COVERAGE RA	PROPERTIES	.550.0 .0524 32560.0 70.00.0	EX	. 8518E+67	.8512E+07	.6493E+67	. 8416F+C7	.8356E+07	.8282E+67	.8192E+67	7962F+07	7319E+07	.7657E+C7	.7475E+07	.72735+67	.7.52E+1.7	.6352E+07	.6277E+C7	.5387E+C7	.5685E+07	5374E+U7	.474CE+07	.44235+07	.4111E+07	3867E+67	.3232E+07	.2965E+C7	2481F+07	.2265E+C7	. 2066E+07	.1884E+67	.1569E+07	,1435E+07	.1314E+07	12L 7E+C	.1112E+67	10201	.8381E+66	312E+0	816E+C	.7386E+06
KEVL FIBER	FIBER	A M M M M M M M M M M M M M M M M M M M	ALPHA	3.00	1.00	2.00		5.00	00.9	7.00	00.0	10.00	11.00	12.00	13.00	14.00	16.00	17.00	18.00	19.00	21.00	22.30	23.00	24.00	25.00	27.00	28.00	20.02	31.00	32.00	33.00	35.03	36.00	37.00	38.00	39.00		42.00	43.00	00.44	33.54

FIBER	FIBER PROPERTIES		ď	ESIN PROPERTIES	RTIES			COMPOSITE PROPERTIES	ROPERTIES			
AF RHOF		EFF = .10 GFF = .30 AFF = .33	.190E+08 .100E+07 .330E+06 .230E-05 .33LE-04		969 412 8699-0	ER = .470E+06 AR = .400E-64 UR = .3500	9 4	RHO= .0468 FTU= 162500.0 FCU= 35006.0 FSU= 8000.0	•••			
ALPHA	EX	ËY	£x9	UXA	UYX	FXTU	FYTU	FXCU	FYCU	FXF	×	A
9.00	.9735E+£7	.76405+36	. 22 8 8 2 + 6 6	•	.0224	162530.0	0	35000.0	2733.5	1365.9	9861E-06	.2961
1.00	.9728E+67	.70462+06	.23162+66	•	.0227	161975.1	4.7	34977.1	2732.8	1446.9	9946E-06	.2960
2.00	.9766E+07	.76415+06	. 24JCE+06	. 2996	.0236	160419.4	18.6	34908.1	2730.9	1540.2	1020E-05	.2960
3.00	.967CE+07	.7631E+36	.25412+65	.3179	.0251	157887.9	45.0	34791.7	2727.7	1647.2	1062E-05	9562.
• •	95185467	. (618E+Jb	20835+06	2000	2/200	154466.9	1.4.1	34626.1	2763.6	1,09.	1121E-05	2054
90.9	94675+07	75825+36	12845+06	6414	0333	145415.2	168.6		2718.5	2065.9	-12916-05	2962
7.06	. 9366E+07	.7558E+06	36366+06	4606	0372	140044.9	230.0		2782.3	2243.2	1401E-05	2948
8.03	.9246E+07	.7531E+36	.46 38E+66	.5124	.0417	134289.7	301.2		2692.9	2442.1	1528E-05	.2964
9.00	.9106E+C7	.7501E+06	.4488E+06	.5703	0240.	128276.0	382.4		2682.3	2663.9	1673E-05	.2939
10.00	.89472+07	.7467E+36	.49832+06	.6328	.0528	122118.7	473.7		2671.5	2910.2	1835E-05	.2933
11.00	. 8766E+C7	.7436E+06	.5521E+06	.7000	.0593	115918.1	575.3		2657.7	3182.1	2014E-05	.2926
12.60	.8563E+07	.7390E+06	90+36639.	•	.0665	109758.8	687.4		2643.8	3480.6	2210E-05	.2919
13.00	.8339E+07	.7347E+06	.6715E+0b	.8445	.0744	103709.4	810.3		2628.9	3606.4	2423E-05	.2909
14.63	.8393E+07	.7301E+36	.7365E+06		.0630	97.823.4	944.3	-	2613.0	4159.9	2652E-15	.2899
15.00	.7825E+07	.72525+06	.8047E+06	. 9957	.0923	92140.9	1089.6		2596.2	4541.1	2898E-05	.2887
16.00	.7537E+67	.7202E+06	. 8756E+06	1.0709	.1023	86690.1	1246.7	27586.9	2578.6	6969	3161E-05	.2873
17.00	.723uE+67	90+3647.	. 94 91E+06	1.1442	.1131	81489.3	1415.7		2561.3	5383.6	3438E-85	.2857
18.00	.6967E+67	.7.94E+ UD	.1025E+07	1.2143	.1247	76548.6	1597.2		2541.4	5842.4	3731E-05	.2838
19.00	.6569E+C/	.7438E+06	.11026+07	1.2798	1371	71871.5	1791.6	24160.7	2521.9	6323.6	4036E-05	182.
20.02	. 6 CCIE+U/	.69816+35	1191811.	1.3397	.1503	1.96470	2.6661		1.2842	4.4.29.0	4354E-05	6/2
23.50	. 5365E+L/	97457769	12696+67	1.3929	1044	698789	7.0222	2017	2462.1	1341-1	4083E-89	1912.
24.00	5145E+07	9045406	10435575	1.4750	1063	59390.2	2707.2		2442	10110	-2619E-05	27.
24.0	LZARE+07	67495466	150.6417	1.5.146	2121	52279.1	7-1100		2422.4	0.500	5786E-05	2661
25.00	.4+38E+67	.6693€+96	15805+67	1.5245	.2299	49054.2	3255.8	16415.8	2483.5	6.96.9	6048E-05	.2617
26.00	.4099E+07	.6640=+36	.1659£+07	1.5355	.2487	46033.2	3555.2		2385.4	10035.3	6384E-05	.2566
27.00	.3773E+07	.659 E+16	.1736E+C7	1.5379	.2686	43204.1	3872.3	-	2368.6	10564.3	670 8E-05	.2509
28.00	.3+63E+67	•6545E+36	.18125+07	1.5321	.2896	40555.1	4207.9		2353.3	11079.7	7012E-05	.2445
00.62	. 31/LE+U/	. 6505E+06	18852+67	1.5186	.311/	38374.5	4562.9	11/23.0	2340.1	11577.5	7288E-05	.2373
24.00	25415407	504/25430	13505411	1.4965	2005	336751.5	4938.4	10/03.4	2329.4	12054.0	/528E-U5	226
32.00	24C6F+C7	54477 + 16	200.5+67	1.4403	3 851	31525. A	5754.8	SARO. 6	2317.8	12021	7855F-05	2107
33.00	.2190E+67	64296416	21516+07	1.4040	.4121	29623.8	6198-1	80.79.1	2318.1	13326.7	7917F-05	1998
34.03	13955+67	.6446 =+36	. 220 9£+07	1.3639	1011.	27830.5	6666.4		2323.6	13691.5	7894E-05	.1880
35.00	.1817E+67	.64682+06	. 2263E+L7	1.3208	.4791	26147.8	7161.3		2335.1	14024.4	77770E-05	.1752
36.00	.16585+07	.65155+06	.23125+17	1.2754	.5111	24568.0	7684.2		2353.7	14324.7	7533E-05	.1613
37.00	.1516E+07	•6584€+36	.23575+07	1.2284	.5336	23083.9	8236.7		2380.3	14592.2	7167E-05	.1465
38.03	. 1389E+C7	.06782+36	. 23972+67	1.1803	.5676	21689.1	8820.6	5095	2416.5	14826.7	6661E-05	.1307
39.00	.1276E+C7	.6863=+66	.24335+67	1.1315	.6030	20377.4	9437.7		2463.4	15028.6	6005E-05	.1143
00.64	.117 de +C7	.6961E+16	.2463E+17	1.0 326	66290	19143.2	16396.3	4311.3	2522.8	15198.3	5190E-05	.9724
11.00	. 1031E+L/	411905119	73438242.	1.6339	1879.	17981.3	11,780.3		2596.5	15136.3	4216E-05	2867.
43.00	90436500	76915+06	252:6+07	1989	7596	15885.8	11210.5		2796.9	15445	- 3084E-05	2279.
44.06	. 8934E+G6	86396+16	25296+67	8918	9607.	14882.7	13100.5	3256.7	2000	15564.2	3824F-05	2786
45.00	84535+66	84515+06	.25325+[7	1948.	. 8465	13965.2	13966.6		3077.3	15579.3	1155F-05	1152
									,			

			AY					4.863E-05																															
			AX	4.394E-06	4.3836-06	4.296E-06	4.221E-06	4-125E-06	3.872E-06	3.716E-06	3.5426-05	3-1435-06	2.9215-06	2.685E-06	2.437E-36	1.9146-06	1.6435-06	1.370E-06	1.696E-06	8.256E-97	3.674E-07	6.75LE-08	-1.541E-07	-3.538E-07	-6.631E-07	-7.644E-07	-8.3316-07	-7.899E-07	-6.881E-17	-2.887E-07	1.797E-08	4.013E-07	8.6456-07	2.04LE-96	2.754E-06	3.5546-36	4.43/2-05	6.4436-96	7.560 - 06
			FXY	1300.3	1371.7	1530.9	1619.5	1714.6	1926.2	2043.3	2168.4	2443.6	2594.0	2753.0	2929.7	3281.3	3473.5	3673.0	3879.2	4.991.3	4529.5	4753.3	4978.8	5204.4	5650.9	5868.8	6287.1	64849	6673.3	7018.0	7172.4	7313.8	7 441.5	7654.3	7738.6	7867.8	7661.7	1000	7931.3
	ROPERTIES	900	FYCU	1857.5	1857.8	1858.6	1861.7	1864.1	1876.7	1875.0	1879.9	1891.9	1899.1	1907.3	1916.3	1977.7	1956.2	1964.1	1979.4	1996.3	2035.6	2058.3	2583.4	2112.9	2174.6	2211.3	2251.7	2345.1	2398.7	2522.7	2594.1	2672.6	2002	2957.5	3671.8	3197.3	3535.0	365:06	3833.1
	COMPOSITE PROPERTIES	RHO# .0166 FTU# 137500.0 FCU# 92500.0 FSU# 8000.0	FXCU	23125.0	<u>.</u>	22995.9	:	22760.2	: .:		21881.9		20816.5	20377.9		1937 6.3	18219.7	17590.5	16933.3	16252.1	14843.0	14126.8	13411.1	12701.6	11322.7	2	10026.9	8839.	8292.	7292.	6840.	6419	6279	5334	5027.	4745.	44.8		3832.8
			FYTU	•	2.0	18.1	32.2	50.4	99.1	129.8	20.7	247.4	295.4	348.0	465.2	533.9	6.5.6	682.5	764.6	952.1	1044.6	1148.7	1259.6	1376.8	1631.1	1768.8	2056.4	2227.6	2395.9	2759.9	2 955 . 8	3161.5	4.7.50	3841.9	4391.4	4353.1	407 704	5217.5	5534.1
		ER = 4.700E+05 AR = 4.000E-05 UR = .3500	FXTU	34375.1	34321.5	33 889.9	33520.7	33056.3	31876.8	31166.6	30400-4	28719.5	27 82 3.4	25 90 1.9	25963.2	24063-1	23114.5	22174.1	21246.3	19443-1		17727.5	•		14 60 8 4	• • •	13214.5		325.9		9 66 8 . 4	9163.7	3 661.4	7 781.1	7 361.2	9.7969	6578.3	1 6	5533.6
	ERTIES		UVX	.0230	.0233	. 0255	.0274	.0298	.0363	1040.	1640.	0562	.0626	.0697	.6773	5460	1041	.1143	.1252	.1369	1623	.1762	.1968	. 2063	.2397	.2575	2963				•	•	•	•	•	.5787	•	•	•
	RESIN PROPERTIE	WR = .3093. RHOR= .0412 FSU = .8030.	UXY	.2850	. 2881	.3127	. 3340	3610	4309	.4730	•	•	•	•	•	•	•										1.2048		1.1487										
	RE		GXY	•	6.613E+04	6.8962+04	7.142E+04	7.456E+04	8 - 28 2E + 04	8.791E+04	9.359E+04	1.0675+05	1.140E+05	1.218E+05	1.300E+05	1.4765405	1.5695+05	1.664E+05	1.762E+05	1.861E+05	2-0636+05	2.165E+65	2.266E+05	2.3675+05	2.564E+05	2.660E+05	2.753E+05	2.929E+05	3-0116+05	3.162E+05	3.233E+05	3.293E+05	3.3492405	3.4456+05	3.483E+05	3.514E+05	3.5596+05	3.5676+05	3.571E+05
SPACEWING-		EF = 1.050E+07 EFT = 1.050E+07 GF = 4.000E+05 AFT = 2.000E-06 AFT = 2.000E-06	EY	1-10 9E+05	1. 10 85 + 05	1.1095+05	1.1116+05	1-11 25+05	1-11-6E+05	1.1185+05	1. 121E+05	1.1285+05	1.132E+05	1.137E+05	1.1426+05	1.1545+05	1.1615+05	1. 169E+05	1.17 8E+05	1.188E+05	1. 21 1E+05	1. 224E+U5	1. 238E+05	1. 25 45 4 15	1.2915+05	1.3126+05	1.3352+05	1.389E+05	1.4215+05	1. 4925+05	1.534E+05	1.5795+05	1.62 42 + 45	1.744E+15	1.810E+05	1.883E+05	1.96 3E+05	2. 14 6E+05	2.25 DE+05
E GLASS/EPOXY -SP FIBER COVERAGE RAT	FIBER PROPERTIES	.6907 .6907 .0926 275000.0	EX	1.3716+06	1.370E+06	1.3636+66	1.356E+G6	1.347E+06	1.3236+06	1.30 8E+06	1.290E+06	1.248F+0E	1.223E+6E	1.196E+66	1.166E+06	1.1346+06	1.064E+06	1.026E+66	9.863E+05	9.457E+05	8-624E+05	8.203E+05	7.784E+05	4.370E+05	5.569E+05	6.18 EE+05	5.819E+05	5.1346+05	4.8196+05	4.243E+05	3.983E+65	3.7416+65	3.5166+65	3-116E+05	2.939E+65	2.777E+05	2.6275+05	-	2.250E+05
FIBER	FIBER	RAPPERSON UP	ALPHA	00.0	1.00	3.00	00.4	2.00	7.06	30.0	30.6						17.06	18.00	19.00	20.05	22.00	23.00	24.00	25.00	27.05		29.00									41.00	00.24	90.99	90.54

COMPOSITE PROPERTIES RHO= .0250 FTU= 137500.0 FCU= 92500.0 FSU= 8000.0 34666663 34666663 34666663 34666663 34666663 34666663 34666663 34666663 3466663 3466663 3466663 3466663 3466663 3466663 3466663 346663 . . . C R R RESIN PROPERTIES VR = .5000 HR = .3093 RHOR= .0412 FSU = 8000.0 EF = 1.050E+07 GF = 4.06iE+05 AF = 2.860E-06 AFT = 2.800E-06 E GLASS/EPOXY -SPACEMIND-FIBER COVERAGE PATIO = .375 PROPERTIES .5035 .6937 .0920 275004.0 185106.0 × WF = RHOF= FIBER ALPHA

E GLASS/EPOXY -SPACEWIND-FIBER COVERAGE RATIO = .500

	A	2.4265-15	2.4255-35	2.425E-05	2.425E-35	2.4235-35	2.422E-35	2 4425-22	2.414F-P5	2.4136-35	2.40 6E-35	2.401E-05	2.3956-15	2.38AE-05	2.381E-05	2.372E-35	2.3625-95	2. 351E-05	2.324E-15	2.307E-65	2.289E-95	2.2635-05	2.2455-55	2.1835-35	2.155E-05	2.113E-35	2.0785-05	2. C3 4E-05	1.9275-05	1.867E-05	1.80 1E-0F	1.7295-05	1.652E-35	1.5695-05	1.481E-75	1.293F-05	1.1936-05		9.967E-06	8.697E-36	7.908E-05	6.954E-06
	AX	4.394E-06	3895	4.374E-JE	4.35CE-06	4. 316E-06	4.272E-06	4.6165-00	L. PA1F-116	3.9995-06	3.966E-06	3.805E-06	3.6945-16	3.574E-06	3.446E-06	3.369E-36	3.164E-06	3. C13E-UB	2.69.E-06	2.521E-06	2.349E-06	2.176E-06	2.003E-06	1.6526-06	1.511E-06	1.366E-06	1.238E-06	1.1316-06	1.6025-36	9.926E-07	1. C 28E-26	1.117E-06	1.265E-06	1.4795-16	1.767E-36	2.58(F-06	3.1126-06	3.729E-06	4.428E-06	5.204E-96	SLE	6.956E-06
	FX¥	2644.2	2778.6		3088.7	3266.6	3461.0	30000	4153.1		4701.3	:	5325.7	:	6019.2	6389.7	4.77.9	7581.2	8000.1	8426.9	6.6598	9296.9	9735.9	101/4.8	11043.5	11468.9	11885.4	12296.8	1 3050.0	13419.7	13766.3	14085.2	14377.5	14653.9	14899.1	15161.0	45683.	15617.4	15724.3	15861.6	15847.2	15862.5
ROPERTIES	FYCU	7392.6	7391.1	7386.0	7377.6	7365.9	7356.8	7356.5	7286.3	7258.6	7227.9	7194.3	7157.9	7118.9	7077.5	7633.7	6987.9	5.0469	6.1489	6789.1	6737.1	6685.C	6633.3	6532.6	6486.7	6445.9	6403.1	6358.3	6118.1	6305.4	6302.8	6312.2	6335.3	6374.2	6431.1	66000	6736	6.891.9	7686.2	7304.6	7568.7	7876.4
COMPOSITE PROPERTIES RHG= .0333 FTU= 137500.0 FCU= 92563.3 FSU= 8400.0	FXCU	46256.0	46221.9	46137.3	4.5995.7	45796.2	45537.7	45610.5	4403009	43679.3	43299.4		:	41135.5	40269.4	39336.7	320.	37 24 1 - 1		33624.9	2	30959.1	29573.8	26166.6	25329.2	23921.0	;	21179.2	: 0	17393.1	16248.0	15176.0	14162.4	å	12364.2	11574.0	10204.6	9620.6	9899.3	8637.4	8230.9	7875.8
10.10	FYTU	9.	1	16.1	36.2	94.4	100	1.00	259.6	329.3	467.7	8.464	6.069	0.969	810.4	934.2	1067.8	1211.3	1529.2	1704.2	1890.3	2087.9	2237.4	2519.1	3061.1	3262.2	3537.6	3827.6	4136.4	4791.8	5146.8	5519.9	5911.6	6323.0	6754.9	1.5057	8182.7	A 706.2	9255.3	9831.1	10435.0	11068.2
ER * 6.700E+05 AR * 4.306E-05 UR * .3566	FXTU	68 75 Co.	68641.0	68315.8	÷	67041.5	66112.6	650000	62444.4	60 86 5 8	59163.1	57 439.0	22646.7	53863.8	51926.3	50029.3	48126.3	46229.1	42492.6	6.699 04	38886.2	37146.6	35 455 . 1	33814.6	30 69 4.4	29216.8	27 794.8	26428.0	22067.6	22651.9	21497.5	20 39 3.1	19336.9	18327.4	17362.9	16441.	122051	13921.2	13156.5	12427.0	11731.0	11067.1
13.0	UYX	.0461	10464	. 3472	.0487	.0567	.0534	9000	6196	1070	.0757	.0820	.0889	.0965	.1048	.1137	.1233	1336	1564	1689	.1821	.1961	.2109	. 2265	2602	.2782	.2971	.3169		3814	9404	.4287	. 4535	.4793	.5658	. 5330	2000	. F. B.	6249	.6777	.7076	.7376
RESIN PROPERTIES VR = .5003 WR = .3093 PHOR= .3412 FSU = .8033.0	UXA	.285C		•	•	•	•	•	3896	14163	.4455	.4771	.5107	.5461	.5830	.6269	. 6595	. 6983	•		•	•	٠	-9372	9813		÷	1.0194							.9520				8257	1968		.7376
	Α×9	1.316F+65	1 - 32 35 + 6 5	1.345E+05	1 . 38 2E+65	1.434E+C5	1.500E+05	1.58UE+35		A SOPE + 15		2.174E+05	2.327E+05	2.491E+05	2 • 66 3E+05	2.844E+05	3.033E+65	3.228E+65	3.6335+05	3.842E+05	4.053E+05	4.266E+65	4.480E+05	4.693E+05	5.11 3F+05	5.318E+05	5.518E+05	5.7136+05	2 34 25 4 05	6.255E+05	6.4195+05	6.572E+C5	6.715E+05	6.846E+G5	6.966E+05	7.67.2E+05	7 2466405	7.1126465	7.364E+05	7.461E+05	7.4235+05	7.430E+05
EFF = 1.050E+07 EFF = 1.050E+07 GF = 4.000E-05 AF = 2.800E-06 AFT = 2.800E-06	Ε¥	414444	4. 432F+35	4. 4282+05	4. 423E+35	4.4165+05	4. 40 62+05	4.3945+65	4. 36 15 + 45	4. 34.75+05	4.328E+05	4. 30 6E+05	4. 28 35+05	4.2585+35	4.232E+05	4. 20 45+05	4.17 SE+05	4.1445+05	4-1135+05	4. 2485+05	4. 3145+05	3.98JE+05	3. 94.7E+65	3. 914E+05	3.85 ZE+35	3.8225+35	3. 7952+05	3.7716+65	2 721.5406	3.722E+05	3.7176+05	3.718E+05	3.727E+05	3. 745E+05	3.774E+65	3.8155+45	3 9475406	4. 62 3F + 11 5	4. 127E+65	4. 252E+05	4-40CF+05	4.57 2E+05
FIBER PROPERTIES WF = .5005 WF = .6937 RHOF= .0920 FTU = 27500 FCU = 18510 UF = .2230	K Z	7475+66	7415+06	2.735E+66	3.726E+GE	2.712E+06	2.695E+06	2.674E+46	2.6195+06	5865 +06	.548E+06	.516E+C6	.46GE+36	2. 439E+06	2.355E+06	.296E+06	. 233E+CE	2.16 (E+06	3-321F+0F	9455+16	. 8 6 6E+06	735E+G6	1.732E+06	1.619E+06	1.25 TE + 06	1.371E+06	1.291E+66	1.213E+06	2012/2101	9.96JE+05	3.30 7E+05	8.694E+05	8 . 122E+05	7.592E+05	7.103E+05	5.656E+05	2012000	1. 55 3F + 0.5	5.260E+05	4.999E+05	77 1E+05	57 2E+0 5
FIBER WF =	AL PHA	0.06		2.00											14.00 2			17.00 2					23.00 1		•		-	29.00		32.00					37.60 7				42.00			

FY = 10056007	E GLASS/EPOXV -SP FIBER COVERAGE RAT FIBER PROPERTIES	ACEWIND- 10 = .625		RESIN PROPERTIES	RTIES			COMPOSITE PROPERTIES	PROPERTIES			
. 28560576 . 85937.5	EF = 1.050E 6F = 4.050E AF = 2.805E AFT = 2.80E			WR = .5000 WR = .3093 RHOR= .0412 FSU = .000			0 E = 0 5	RHO= .0416 FTU= 137501 FCU= 92501 FSU= 8006	000			
2050 1976 1976 1976 1972 <th< th=""><th>EY</th><th></th><th>GXY</th><th>UXA</th><th>XAO</th><th>FXTU</th><th>FYTU</th><th>FXCU</th><th>FYCU</th><th>FXY</th><th>×</th><th>AY</th></th<>	EY		GXY	UXA	XAO	FXTU	FYTU	FXCU	FYCU	FXY	×	AY
2916 1959 95364.3 5.0 57777.5 1152.3 1 375.6 4.339E D6 5.2975 1053 9772.5 1152.3 1 375.6 4.339E D6 5.2975 1053 9772.5 1152.3 1 375.6 4.339E D6 5.2975 1053 9772.5 1152.5 1 375.6 4.339E D6 5.2975 1053 9772.5 11572.3 1 375.6 4.339E D6 5.2975 1053 9772.5 11495.1 3773.1 37			1.644E+0		9250.	85937.5	•		1152	3331.5	4.394E-06	1.9416-3
2916 1058 9334.7 24. 1572.4 11912.6 346.3 4.335E.06 11. 2917 10524 9301.9 10.6 5724.4 1197.6 4100.9 4.335E.06 11. 2197 10524 9301.9 10.6 5724.9 1147.0 4100.9 4.335E.06 11. 2197 1052 1052 1052 1052.1 126.0 5622.9 11439.4 436.3 4.22.E-06 11. 2197 1052 1052 1052 1052 1052 1052 1052 1052			1.654E+0	•	. 6579	85861.3	5.0		1152	3494.9	4.396E-06	1.941E-0
. 1972			-730F+0		.056	89394.0	1.02		1151	3675.6	4.379E-06	1.9416-0
1996 1662 1266 1266 1366 114394 43164 43166 43166 43167 43166 43167 43167 43167 43167 43167 4317 43167 4317 43187 43		• -	796E+0		4290	83 801.9	909		1167	4100.9	4.335F-06	1.9415-0
3327 10725 7916.6 95534.9 111401.3 4916.3 4.2666.10 3327 10725 7916.6 324.5 9516.6 11104.5 952.5 4.276.6 3724 1072 7916.6 324.5 9516.2 11104.5 952.5 4.177.6 4754 1072 7916.6 94.78.1 11116.2 952.5 4.177.6 4751 108.1 7798.7 518.6 5250.3 11116.2 522.5 4.177.6 4751 108.1 7798.7 518.7 518.7 518.7 518.6 5250.5 11116.2 56.6 6.10.8 6		-	. 88 0E+0	•	.0652	82646.8	126.0			4346.0	4.301E-06	1.9435-0
. 3724		-	.983E+0	•	.0665	81259.1	181.8			4614.3	4.260E-06	1.940E-0
4754 1717 <th< td=""><td></td><td>~</td><td>16 2E+6:</td><td>•</td><td>.0725</td><td>79677.6</td><td>247.9</td><td></td><td></td><td>4966.3</td><td>4.212E-36</td><td>1. 939E-0</td></th<>		~	16 2E+6:	•	.0725	79677.6	247.9			4966.3	4.212E-36	1. 939E-0
4496 1083 73953 509.6 54178.0 11181.5 5926.5 4.028E-06 4796 1084 73953.9 509.6 54178.0 11116.2 672.6 3.95E-06 4756 1089 7399.7 158.8 5338.4 11116.2 672.6 3.95E-06 5774 1189 747.2 1101.6 672.6 3.95E-06 5784 1289 1713.6 547.7 1107.6 672.6 3.95E-06 5784 1287 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.7 1187.8 1187.8 1187.8 1187.8 1187.8 1187.8 1187.8 1187.8 1187.8 1187.8 1187.8 1187.8 1187.8 1187.8 1187.8 1		50	392F+0	•	1080	76001-0	411.7			5562.6	4-15/E-06	1.9395-0
4464 10948 71798.7 518.5 5258.4 31111.2 6333.4 3945E-0 4751 1020 6956.4 773.6 5258.5 11032.7 6722.6 3766E-0 5157 1102 6754.7 670.6 5559.5 11032.7 7653.0 3766E-0 577 1105 6407.9 113.6 69487.3 1105.7 7653.0 3766E-0 574 127 62536.7 135.7 4421.9 1064.2 856.6 3.466E-0 6736 1463 576.4 155.4 1641.9 1066.2 856.6 3.466E-0 6736 1463 576.4 155.4 1641.9 1666.2 856.6 3.466E-0 6736 1463 462.1 1611.9 1611.9 1611.6 3.466E-0 3.466E-0 6736 157.4 1641.9 1641.9 1641.9 1641.9 1641.9 1641.9 1641.9 1641.9 1641.9 1641.9 1641.9 1641.9 1641.9 1641.		N	560E+09		.0863	73953.9	509.6			5926.5	4.023E-06	1.9375-0
. 5055 . 1020 05584, 778.6 52965.3 11032.7 6722.6 3 5595E OF 67254 . 11020 05584, 778.6 52965.3 11032.7 6722.6 3 5595E OF 67294.7 11020.5 64907.9 1133.6 50487.3 11054.6 8556.6 3 4466E OF 6736 . 11027 6535.7 1157.8 4934.7 11054.6 8556.6 3 4466E OF 6736 . 1163 57766.4 1554.1 46611.9 11558.7 9556.5 3 3466E OF 6736 . 1163 57766.4 1554.1 46611.9 11558.7 9556.5 3 3456E OF 6736 . 1163 57766.4 1554.1 46611.9 11558.7 9556.5 3 3456E OF 6736 . 1163 57766.4 1554.1 4641.9 110558.7 9556.5 3 33556.0 1064.2 1064.8 11002.7 3 10576.0 1064.2 1064.8 11002.		Ň	743E+0	•	9760.	71798.7	618.5			6313.4	3.945E-06	1,935E-0
574* 1109 6/294.** 1010.** 10154.** 10164.**		'n	939E+0	•	.1020	49 55 8 . 4	738.6			6722.6	3.859E-06	1.934E-9
6784 1377 6157.8 1334.7 1661.9 1664.2 8556.6 3.456E.06 6536 1463 157.8 1334.7 1661.9 1664.2 8556.6 3.456E.06 6536 1557.8 1334.7 1661.9 1664.2 8556.6 3.456E.06 6536 1557.8 1516.3 1456.1.9 11654.2 8556.5 3.456E.06 1463 157.4 1516.3 1456.1.9 11654.5 1656.5 3.456E.06 1463 1567.4 1516.3 1456.1.9 11654.5 1666.5 3.456E.06 1664.2 1666.5 3.456E.06 1664.2 1666.5 3.456E.06 1664.5 1666.5 3.456E.06 1664.5 1666.5 1666.5 3.456E.06 1664.5 1666.5 16			148E+0:	•	.1199	64 207 9	1317	51539	10949.1	7152.9	3.766E-06	1.9325-0
.6389 .1377 61157.8 1334.7 48121.9 11664.2 8566.6 3.446E-D6 65389 .1483 57786.4 1554.1 46811.9 11664.2 8566.6 3.446E-D6 65389 .1597 8545.1 1766.4 1554.1 46811.9 11658.7 9966.5 3.1355E-D6 65736 .1597 8645.4 1215.9 11032.7 3.105E-D6 7751 .1984 48617.4 2130.3 4244.4 1 11015.9 11654.8 2.9316.0 6 7751 .1984 48617.4 2130.3 4244.4 1 11015.9 11654.8 2.9316.0 6 7751 .1984 48617.4 2316.9 1034.1 11015.7 3.105E-D6 8865 .2128 48617.4 3.2569.9 3153.7 9972.4 1175.6 2.646E-D6 8865 .2260 44613.3 2.669.9 3153.7 9972.4 1175.6 2.646E-D6 8865 .2260 44617.5 3168.9 33453.7 9972.4 1175.6 2.646E-D6 9869 .2669 40.264 13.875.6 3346.9 33453.7 9972.4 1175.6 2.646E-D6 9869 .2669 40.264 13.875.0 3346.2 3441.9 3346.6 3346.1 14391.4 19494.2 1946E-D6 9976 .3365 3345.3 4446 2646.3 1164.3 1227.4 1946.2 1635E-D6 9974 .3375 29821.9 5667.6 2867.4 1999.7 1637.6 11764.0 11762.6 1776			60 1E+09		.1277	62536.7	1157.8	49347	10764.6	8071.5	3.559E-06	1.925E-JE
. 6736 .1597 55435.3 17664 1554.1 10611.9 10558.7 95695.5 3.1556.7 6736 .1597 55435.3 17664 1595.9 10334.1 1002.7 3.1676.06 .7751 1096.			84.2E+0	•	.1377	63157.8	1334.7	4812	10664.2	9.9558	3.4465-06	1.9236-0
7081 1719 531158 1911.5 443952.9 10334.1 10192.7 3.067E-06 7721 1904 46673.8 2300.9 40124.9 10215.9 10334.1 11092.7 3.067E-06 7721 1904 46673.8 2300.9 39153.7 997C.4 11175.6 2.646E-06 8643.8 2218 464318.9 2317.3 7915.7 997C.4 1175.6 2.646E-06 8643 2318.9 3315.3 7 997C.4 1175.6 2.646E-06 8643 2318.9 33713.3 32286.5 994C.4 12229.5 2.75618.6 90.6 25619.0 3341.9 33954.3 999C.1 13332.0 2.75EE-06 90.6 25619.0 3771.3 3728.5 996C.1 13332.0 2.213E-06 90.7 3164 3136.8 1422.0 2.0676.3 999C.1 13332.0 2.213E-06 90.7 3164 3136.8 1422.0 2.0676.3 9910.0 14930.2 1109C.2 1109C.2 1109C.6 1009C.1 3355 3139C.6 12567.0 3910.0 1493C.2 1109C.2 1109C.2 1109C.2 109C.2 10			192E+0	•	.1597	57.786.4	1514.1	4681	10558.7	9656.5	3.325E-16	1. 9196-75
7421 .1847 508374 2130.3 42414.1 10215.9 10564.8 2 931E-06 6643.3 2352.9 40811.5 10694.5 111634.2 2-6789E-06 6643.3 2569.9 3945.1 11654.6 2 6461.3 2.6789E-06 6643.3 2669.9 3945.1 11755.6 2 6461.0 2 6464.3 2 6699 3945.1 11755.6 2 6461.0 2 6464.3 2 6699 3945.1 11755.6 2 6461.0 2 6461.0 2 6491.0 2 6491.0 3741.0 3741.0 3741.0 3741.0 3741.0 3741.0 2 6491.0 1777.7 1772.5 2 2.7566.0 6989.0 2 6491.0 1777.7 1772.5 2 2.7566.0 6989.0 2 6491.0 1772.6 2 6461.0 1772.6 2 6461.0 6989.0 2 6491.0 1772.6 2 6		;	611E+09	•	.1719	53115.8	1911.5	4395	10334.1	13092.7	3.067E-06	1.9075-09
8856 - 2283 44318-9 2871.6 3745.5 11775.6 2.646E 05 8856 - 2283 44318-9 2871.6 3745.5 11775.6 2.646E 05 8856 - 2283 44218-9 3245.3 9745.4 11775.6 2.646E 05 8859 - 2263 1828.4 3741.3 33286.2 9463.6 13372.1 2.245E 05 9871 - 2371 35521.1 3741.3 33286.2 9463.6 1372.5 2.245E 05 9872 - 2265 3858.4 3751.3 33286.2 9463.6 1372.6 1372.6 1944.2 10.645.6 10.665.6		;	878E+0	•	.1847	50 837 .4	2130.3	42414.	10215.9	10 624.8	2.93(E-06	1.9035-0
8367 -2281 44318.9 28713.5 9717.3 1229.9 2.356E.0 846 -2241 42268.2 318.9 35713.5 9717.3 1229.5 2.356E.0 848 -2619 4836.2 9463.6 1332.0 2.356E.0 356E.0 9123 -278 36521 4477.8 3642.2 9463.6 1385.2 1.94E.0 947 -316 3473.4 3622.3 9320.1 1490.2 1.94E.0 950 -336 3473.4 2567.6 2367.1 1490.2 1.94E.0 960 -357 3139.8 516.1 2367.4 1991.7 1596.0 974 -379 2912.6 2367.4 4991.7 1639.7 1639.7 974 -379 2912.8 5567.6 2367.4 4991.7 1639.6 1726.0 974 -379 2912.8 5567.6 2367.4 4991.7 1639.6 1726.0 974 -475 2417.1 2433.6 <td< td=""><td></td><td>2</td><td>140E+U</td><td>•</td><td>2128</td><td>1000</td><td>2669.9</td><td>19151</td><td>9975.4</td><td>11163.6</td><td>2.5465-36</td><td>1.8815-3</td></td<>		2	140E+U	•	2128	1000	2669.9	19151	9975.4	11163.6	2.5465-36	1.8815-3
************************************	'n		694E+09	•	.2260	44318.9	2871.8	37456.	9944.4	12249.5	2.501E-06	1.9695-0
8893 -2569 4028440 334119 33354.3 9590.4 13782.0 2.213E-10 69127 -2971 3652.1 4477.8 30422.9 9339.1 14390.4 13782.0 2.2475E-10 6917 -2971 3652.1 4477.8 30422.9 9339.1 14390.4 13782.0 2.2475E-10 6917 -2971 3652.1 4477.8 30422.9 9339.1 14390.4 1368.2 1.0475E-10 6917 -2971 36521.9 6917.7 12867.8 13677.1 15888.2 14575E-10 6917 -2971 36521.9 6917.7 15888.2 17219.8 1575E-10 6917 -2971 36521.9 6917.7 15888.2 17219.8 1575E-10 6917 -2971	4		96 6E+0	·	.2441	42268.2	3148.9	35713.	9717.3	12792.5	2.356E-36	1.855E-0
9317		٠,	237E+0	Ī	. 2669	40 28 4 • J	3+41.9	33954	9596.6	13332.0	2.213E-36	1.839E-0
9478 3164 347434 44220 28676.3 9218.0 14904.2 1.024E-06 9504 3164 347434 44220 28676.3 9218.0 14904.2 1.024E-06 9504 3575 31394.8 5167.4 1999.7 15087.2 1.624E-06 9765 4425 28014.9 5567.6 22424.4 8790.8 1.0575.2 1.6275.2 1.6275.0 1.6275.2 1.6275.0 1.6275.0 1.6275.2 1.6275.0 1.6275.2 1.6275.0			767E+0		2971	36 55 6 5	6.77.8	30422	9465.6	14390.4	1.9445-96	1.7995-1
9604 .3355 31355.0 4784.5 526961.4 9101.6 15404.3 1.72[E-16 9504 .3557 31394.8 5166.1 22890.1 991.7 15085.2 1.635E-16 9747 .3793 29821.9 5567.6 22824.4 8791.7 15085.2 1.635E-16 9747 .3793 29821.9 5567.6 22824.4 8796.8 1277.7 15085.2 1.675E-16 9745 .4456 25491.3 6899.8 19257.4 8756.8 1721.4 1759E-16 1757.7 15085.9 1505E-16 9694 .4496 25491.3 6899.8 19257.4 8656.8 17614.4 1559E-16 9493 .5209.8 19257.4 8656.8 17614.4 1559E-16 9493 .5209.8 19257.4 8656.8 17614.4 1759E-16 17616.9 17616.			023E+0		.3164	34743.4	4422.0	28676.	9218.0	14904.2	1.824E-06	1.7745-0
9747 3793 298219 55676 23874.3 8897.1 15357.5 1.575E-06 9745 4.622 28314.9 5567.6 23874.3 8897.1 15357.5 1.575E-06 9745 4.622 28314.9 5989.8 12224.4 8790.8 17237.7 1556E-06 9608 4496 25491.3 6899.8 19257.4 8556.8 17237.7 1556E-06 9695 4496 25491.3 1839.5 14953.6 86114 17926.6 1764.4 1556E-06 9692 5011 22910.2 27926.6 1134.5 18321.5 1856E-06 9777 15261.2 1857.5 1857.5 1857.6 1556E-06 9777 1945.7 1945.7 1945.7 1945.7 1945.7 1945.7 1945.7 1945.7 1945.7 1945.8 194			51 4F+0		3365	33635.2	5166.1	26961	9101.6	15404.3	1.7206-36	1.74 35-0
9765 .4626 28314.9 5989.8 22124.4 8798.8 1677.7 1.546E-U6 9746 .4496 25491.3 6893.8 12677.4 1771.8 1.555E-U6 9694 .4496 25491.3 1899.8 12677.4 8656.8 1764.4 1.668E-U6 9694 .4496 24171.1 7389.5 17953.6 8611.4 17982.6 1.714E-U6 9492 .5014 22019.2 7791.8 17953.6 8611.4 17982.6 1.714E-U6 9492 .5014 22019.2 7791.8 16742.4 8657.1 1879E-U6 1.714E-U6 9492 .5014 22019.2 7791.8 1662.3 8697.1 1879E-U6 1.714E-U6 9477 .5534 28554 1912.5 1.8681.2 8676.4 19146.2 2.116E-U6 9477 .5534 1899.8 2.414E-U6 9477 .5533 1899.8 1328.4 12885.1 11456.5 9891.9 1952.5 3.754E-U6 98539 .6569 1644.5 11589.1 11456.5 9891.9 1952.5 3.754E-U6 98539 .6569 1548.2 13288.9 1146.8 9891.9 1952.5 3.754E-U6 98539 .6569 1548.8 1348.7 1348.8 9912.9 1965.9 4.424E-U6 98539 .6569 1348.3 1348.3 1348.3 9973.9 19828.2 5.8028-U6 973.8 7493.9 19828.2 6.698E-U6 97493 .7768 .7768 .7768 .7769 .776		. ~	.746E+0		3793	29821.9	5567.6	23674.	8896.1	16353.5	1.575E-06	1.675E-0
9694 .4496 25491.3 5899.9 1227.4 6551.2 1751.6 1.595E.Pr 9608 .4745 24171.3 5899.9 12677.4 6551.6 1764.4 1.668E.Pr 9492 .5011 2290.2 7993.8 12677.4 6551.6 17.14E.06 9492 .5012 2290.2 7993.8 12677.4 6551.6 1.715.6 1.714E.06 9492 .5014 2290.2 7993.8 1267.4 1662.6 1669.4 2.116E.06 9492 .5014 2290.2 7993.8 1662.4 1869.2 2.116E.06 9492 .5014 2290.2 7996.7 1662.9 1690.8 2.116E.06 9492 .5014 1945.7 1945.7 1946.5 1690.8 2.796E.06 8599 .6569 1644.5 11559.1 11456.5 909.8 1952.7 3.625E.06 8693 .6569 1645.6 11559.1 11456.5 909.8 1965.9 4.424E.06 8704 .7214 1465.8 13.877 10393.4 9621.4 1980.2 5.822E.06 8709 .7214 1465.8 13.835.2 9973.3 9973.9 1982.5 6.696E.06		-	.966E+0		. 6626	28314.9	5989.8	22124.	8798.8	16797.7	1.5465-06	1.635E-0
9608 .4776 24174.7 7393.6 17742.4 6555.6 17742.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 17742.6 9508.6 177401.6 177401.6 9708.6 9708.6 177401.6 177401.6 9708.6 9708.6 177401.6 177401.6 9708.6 9708.6 177401.6 9708.6 9708.6 17742.6 9708		0	17 bE+0.	•	4524	25871.9	5433.6	5004 9	872F.2	17215.8	1.5555-06	1.584-1
9992 5011 22909.2 7903.8 16742.4 6587.0 1831.5 1.879E-06 9377 5534 21773.6 8443.6 15626.3 8587.0 1831.5 1.879E-06 9377 5534 2170.6 8443.6 15626.3 8587.0 1831.6 2414E-06 8983 5567 19452.7 19452.1 16036.2 8676.0 19146.2 2.796E-06 8678 5669 1894.8 13228.4 12856.1 8772.9 19522.7 3.258E-06 8679 6669 16445.6 11569.1 11456.5 9109.1 1952.7 3.612E-06 8678 5669 16445.6 11569.1 11456.5 910.9 1952.7 3.612E-06 8678 724 19653.9 13035.2 9973.3 9973.9 19828.2 6.698E-06 8698E-06 87493 77494 14663.8 13035.2 9973.3 9973.9 19828.2 6.698E-06			555E+05	•	4446	25491.3	389	: :	8611.4	17982.6	1.7145-06	1.5355-3
9347 .5264 21773.6 8443.6 15626.3 8587.2 18629.4 2.11(E-CE .9937 .5533 21952.1 9.10.1 14616.0 8615.5 18994.8 2.41EE-UE .8993 .5587 1945.7 13616.0 8675.0 19146.2 2.41EE-UE .8770 .6085 18403.1 11228.4 1285(.1 8772.9 1932.5 3.258E-UE .8539 .6569 1645.6 17401.5 11392.7 12109.8 9916.9 1952.7 3.802E-UE .8539 .6569 1645.6 12228.9 10865.3 9329.7 1972.5 3.258E-UE .8768 .7214 14653.8 13228.9 10885.3 9973.9 19655.9 5.802E-UE .7768 .7214 14653.9 13835.2 9973.3 9973.9 19825.2 6.698E-UE			723E+0		.5061	22969.2	7903.8	: .:	8587.0	18 321.5	1.879E-06	1.4146-
.917 .5533 20552.1 9110.1 14606.0 8615.5 18904.8 2.414E-06 .8983 .6167 19452.7 9664.7 13861.2 8675.4 19156.2 3.796E-06 .870 .6065 18403.1 10284 12850.1 872.9 19352.7 3.254E-06 .8539 .6569 16445.6 11569.1 14456.5 9104.8 19552.7 3.602E-06 .8035 .6569 16445.6 11569.1 14456.5 9104.8 19552.7 3.602E-06 .8035 .6569 15645.6 11569.1 14456.5 9104.8 19655.9 4.424E-06 .7768 .7214 14653.8 13.837 10393.4 9621.4 19809.2 5.802E-06 .7493 .7494 13833.9 13835.2 9973.3 9973.9 19828.2 6.698E-06		80	876E+C		.5264	21703.6	443		8587.2	18629.4	2.11CE-C6	1.7455-3
.8933 .5807 19452.7 9564.7 13681.2 8676.6 19165.2 2.796E-06 .8770 .6085 17401.5 1328.4 12856.1 8772.9 19352.5 3.258E-06 .8539 .6366 17401.5 11852.7 12109.8 9916.9 19522.7 3.62E-06 .8293 .6649 16465.6 11569.1 11456.5 9194.8 19655.9 4.424E-06 .8135 .6649 15533.7 13288.9 10886.1 9129.7 19754.5 5.212E-06 .7768 .7214 14663.8 13.437 10393.4 9621.4 19899.2 5.862E-06 .7494 13833.9 13835.2 9973.3 9973.9 19828.2 6.698E-06		σ	.012E+C		. 5533	20 55 2 . 1	.10	•	8615.5	18904.8	2.414E-06	1.271E-0
.8570 .6085 1846341 1022844 12256.1 8772.4 19525.5 3.254E-06 .8539 .6356 17401.5 103827 11249.8 8911.9 1952.7 3.062E-06 .8293 .6649 1644546 11569.1 11456.5 9094.8 19655.9 4.424E-06 .8135 .6649 1644548 112288.9 10886.9 19329.7 19754.5 5.121E-06 .7768 .7214 14663.8 134.87 10393.4 9621.4 19699.2 5.882E-06 .7493 .7494 13833.9 13835.2 9973.3 9973.9 19828.2 6.698E-05			9.132E+0	•	. 5867	19452.7	9664.	13661.	8676.6	19146.2	2.796E-56	1.1915-0
.8539 .6586 17401.5 10852.7 12109.8 6911.9 19522.7 3.0CZE-U6 .8293 .6669 16445.6 11559.1 11456.5 9094.e 19655.9 4.424E-U6 .8035 .6932 15533.7 122889 1086.1 9329.7 19751.5 5.121E-U6 .7766 .7214 14663.8 1343.7 10393.4 9621.0 19809.2 5.882E-U6 .7769 .7294 13633.9 13835.2 9973.3 9973.9 19828.2 6.698E-U6			9.234E+0	•	. 6085	18463.1		1285C.	8772.9	19352.5	3.258E-06	1.1085-0
.0135 .6932 15533.7 12209.1 117505.1 9194.c 19555.9 4.4.4.4.2.00 .0135 .6932 15533.7 12209 10006.1 9329.7 1971.5 5.1212.0 .7766 .7214 14663.6 13343.7 10393.4 9621.(19809.2 5.802E-06 .7493 .7494 13633.9 13635.2 9973.3 9972.9 19025.2 6.698E-05			9.319E+C		.6366	17401.5		12109.	6916.9	19522.1	3.862E-U6	1.721E-J
.461E405 .7768 .7214 14.663.8 133.3.7 10393.4 9621.4 19809.2 5.882E-06		. 0	432E+0		6932	15533.7		: :	9329.7	19751.5	5.1215-06	P. 434E-0
.470E-05 .7493 .7494 13833.9 13835.2 9973.3 9973.9 19828.2 6.698E-16			461E+0		.7214	14 663.8		10393.4	9621.6	19809.2	5.882E-16	7.552E-G
	5.753E+05		9.470E+0		1641.	13833.9	13835.2	9973.3	9973.9	19828.2	6.698E-16	6.695E-0

			N.	1-619E-05	1.618E-05	1.618E-05	1.618E-05	1.6185-05	1.619E-05	1.619E-05	1.619E-05	1.623E-05	1.62JE-05	1.624E-05	1.621F-05	1.62:E-3F	1.623E-C5	1.6196-95	1.6186-35	1.617E-35	1.6155-15	1.60 8F-15	1.6646-75	1. 598E-15	1.5915-95	1.582E-15	1. FS9F-05	1. 5435-05	1.5256-75	1.4795-35	1.4505-05	1.416E-05	1.377E-05	1. 5545-05	1.2296-25	1.169E-05	1.10 3E-05	1.C 32E-05	9.5745-06	8.801E-36	8.C14E-06	7.229E-06	0.4025-00
			×	4.394E-86	4.391E-06	4. 382E-86	4.368E-06	4.3216-16	4.289E-16	4.251E-06	4.207E-06	4.157E-06	4.101E-06	4.039E-05	3.8975-06	3.817E-06	3.7316-36	3.6396-06	3.542E-06	3.4365-06	3. 331E-06	3.2195-36	2.9826-36	2.86LE-06	2.736E-06	2.6135-36	2.377F-36	2.268E-96	2-171E-06	2.025E-06	1.9875-06	1.9795-06	2.0105-06	2.2145-06	2.402F-06	2.657E-06	2.984E-06	3.387E-16	3.867E-06	4.4215-06	5.C45E-06	5.736E-05	6.4555-05
			FXY	4028.6	1219.7	****	4674.9	5238.9	5564.7	5923.5	6336.2	6721.	1165.5	8135.2	8657.8	9263.4	9769.7	10354.8	11956.3	11571.9	12199.1	13478.2	14124.8	14772.5	15418.5	16659.9	17317.5	17927.8	18521.9	19650.0	20178.5	20679.5	21150.6	21903.5	22366.8	22689.6	22978.0	23224.6	23428.2	23587.5	23702.0	23770.8	23795.0
	ROPERTIES	•••	FYCU	16567.1	16561.3	16543.7	16514.4	15425.4	16356.6	16286.9	16193.7	16695.2	15965.5	15654.	15596.8	15438.6	15275.2	15132.5	14926.5	14729.6	14530.3	14109-5	13889.	13663.6	13434.1	13261.7	12734.3	12502.7	12275.2	11842.1	11642.0	11457.1	11291.1	1114	13947.3	10900.2	10895.7	10939.6	11038.9	11199.6	11428.9	11733.8	12121.5
	COMPOSITE PROPERTIES	RHO= .0499 FTU= 137568.0 FCU= 92500.0 FSU= 8000.0	FXCU	69375.3	69333.3	6920 7.9	68998.4	68322.4	67854.1	67295.9	2.94999	65903.3	40000	64120.5	61958.4	60722.1	59384.7	57947.9	56410.8	54779.0	53056.1	49361.5	47406.3	45392.7	43332.7	41239.8	37014.1	34912.6	32845.0	28843.1	26947.8	:	23425.5	202012	18945.6	17687.9	16551.1	15534.1	14634.7	13849.7	13172.0	12598.1	16166.0
	٠		FYTU	•	9.9	24.1	54.3	151.2	218.1	297.4	389.4	0.464	0110	886.3	10440	1215.6	1401.3	1601.7	1816.9	2:47.5	2293.8	2835.5	3131.9	3446.1	3778.7	4130.3	6803.4	5306.3	5741.4	6681.1	7.187.7	7720.3	8279.8	0000	10132.3	19812.2	11525.6	1227 4.1	13059.3	13882.9	14746.7	15652.5	1000.00
		ER = 4.780E+09 AR = 4.00GE-05 UR = .35G0	FXTU	103125.0	102961.5	102473.7	101669.6	99168.9	97 516.9	95 612.4	93499.9	27 20 1.5	0.447.00	A1 47 E. 1	80 765.6	77 889.5	75644.5	72189.4	69343.6	66 522.3	63739	58329.3	55719.9	53162.6	50721.9	48346.8	43825.2	41692.1	39642.0	35786.3	33977.8	32246.3	30589.6	27 401.1	26644.3	24 662.5	23343.2	22083.7	20881.8	19734.8	18640.5	17596.5	Toon
	RTIES	:	N.X					0220	.0805	. 1845	1690.	6460.	. 1003	1151	.1233	1321	.1417	.1519	.1629	1747	2781.	.2165	.2294	.2450	.2614	.2787	3156	. 3353	.3558	3991	.4223	.4455	8694	2000	.5462	.5727	.5995	.6265	. 6535	.6868	1707.	266.2	71010
	RESIN PROPERTIES	VR = .5000 WR = .3093 RHOR= .0412 FSU = .000.0	UXA	.2850	•	•	•	3150		•	•	•	•	•			•	•	•	•	•	•	•	•	•	•	. 8807	•	.9142	•	•	•	.9418	2020		•	•	.8737	. 8540	. 8325	.3096	* 1007	700,0
	2		GXY	1.973E+05	1.985E+05	2.020E+65	2.678E+05	2.263E+05	2.369E+05	2.536E+05	2.704E+05	2.691E+05	3.0905405	3.5635+05	3.820E+05	4.092E+05	4.3762+65	4.672E+65	4.979E+65	5.294E+05	5.616E+35	6.27 7E+05	6.611E+05	6.947E+05	7.281E+05	7.614E+05	8.264E+65	8.579E+05	8.886E+05	9.4665+05	9.738E+05	9.995E+05	1.024E+06	1.067F+06	1.485E+06	1.102E+r6	.117E+ù	+	+	1.148E+06	1.1245+05	1.157E+06	1.1705400
SPACEWIND- 1710 = .750		EFT = 1.050E+07 EFT = 1.050E+07 GF = 4.00E+08 AF = 2.00E-06 AFT = 2.000E-06	Ε¥	9.973E+05	9.970E+05	9. 95 8E+0 5	9.9435+55	9.88 (E+1) 5	9.8392+05	9.79CE+05	9.735E+05	9.672c+05	9.65.ZE+05	9-2625+63	9. 5CE+05	9. 25 35 + 05	9-1495+35	9. 639E+05	8.924E+35	8.83 2E+05	8.67.52+05	8 43 8E + 05	6.2682+05	8-125E+05	7.9792+05	7 49 3E+05	7.5355+05	7.387E+35	7. 2435435	6.966=+25	6.837E+05	6.7175+05	6. 60 8E+ 45	6.435405	5.3722+35	6. 332E+45	6.318E+05	5.3315+05	6.3762+05	6.456E+J5	6.575E+35	5 - 7382 + 62	0.74/6102
E GLASS/EPOXY -SP FIBER COVERAGE RAT	PROPERTIES	.5906 .6937 275200.6 185303.0	EX	4.114E+06	** 111E+06	4.132E+06	4.088E+6E	4-6436+06	4.011E+66	3.9746+06	3.9312+06	3.882E+6E	3.0255	3.6985+06	3.624E+06	3.5+5E+06	3.4592+66	3.358E+06	3.271E+66	3.169E+6E	3.0635+06	2.837E+06	2.71 8E+66	2.597E+GE	2.474E+06	2.35(E+0b	2.1336+06	1.981E+CE	1.861E+06	1.6325+66	1.524E+06	1.422E+06	1.325E+06	1.1505+06	1.3736+66	1.0336+06	9.395E+05	8.829E+05	8.330E+05	7.895E+65	7 30 3E + US	6.947F+05	
FIBER	FIBER	AR RHOTTU	AL PHA	0.00	1.00	2.00	3.00	20.5	9.00	7.00																			29.00														

COMPOSITE PROPERTIES 2225333 222533 222533 222533 222533 222533 222533 222533 222533 22253 137550.0 92500.0 9300.0 609337. 600937. 600937. 600506. 600 . = 4.760E+05 = 4.966E-05 = .3500 120131 11190131 11190557 111190557 11119057 1119057 VR = .5000 WR = .3093 RHOR= .0412 FSU = 8090.0 RESIN 1. USGE+07 1. USGE+07 1. USGE+07 1. USGE+05 2. 800E-06 2. 800E-06 1. 35 7E + 1 6
1. 35 E GLASS/EPOXY -SPACEMIND-FIBER COVERAGE RATIO = .875 FIRE PROPERTIES WF = .5000 WF = .6917 RHOF= .0920 FTU = 2.5500.0 FCU = 185.00.0 UF = .2200 EX AL PHA

FIBER	SSZEPOXY -	SPACEWIND-										
FIBER	PROPERTIES			RESIN PROP	PROPERTIES			COMPOSITE	PROPERTIES			
TARE TO SERVICE TO SER	275	EFT = 1.05JE+07 EFT = 1.05CE+07 GF = 4.00GE+05 AFT = 2.0CUE-C6 AFT = 2.0CUE-C6		VR = .5006 WR = .3093 RHOR= .0412 FSU = .0036.0	9 8 8 8	AR = 4.700	.356. .356.	RHO= .0666 FTU= 1375 00.0 FCU= 92550. FSU= 8033.5	970			
AL PHA	×	£	A X 9	AXO	NA.	FXTU	FYTU	FXCU	FYCU	FXY	AX	A
0.00	5.495E+06	1.7735+06	2.631E+09	•	.0921	137560.0	•	-	29365.1	5451.6	4.394E-06	1.213E-
1.00	5.481E+46	1.7725+06	•	•	. 1925	137282.0	3.0	92445	29352.7	6.4695	4.392E-06	1.21 3E-
30.2	5.470E+66	1.766F+06	2. 69 6E+05	2585	.0952	135559.5	32.6	92279.8	29254.4	62903.7	4.377E-0F	1.214
	5.425E+66	1.760E+06			.0975	134683.0	128.9	91616.	29168.5	6648.7	4.363E-06	1.214E-
20.6	5.391E+06	1.7535+06	3.335E+05		. 1065	132225.2	201.6	91115	29058.0	7046.9	4.346E-06	1.2155-
200	5.299F+06	1.7345+06			1000	127483.2	396.6	89776-1	28753.8	7977.6	4.301.5-06	1.216E-
9.00	5.242E+16	1.7225+06			.1138	124666.5	519.1	68921.1	28585.2	8505.3	4.271E-u6	1.217E-
9.00	5.177E+06	1.709E+06	3.911E+0		.1196	121 601.6	658.7	87952.3	28372.5	9073.4	4.238E-05	1.2195-
10.00	5.134E+06	1.6945+36	4 - 200E+05		1321	118 326 2	015.4	86666.8	28146.6	10121	4.200E-06	1.220E-
12.30	4.935E+0E	1.6595+06	4 . 84 9E+05		.1412	111293.5	1181.7	84304.3	27605.7	11000.0	4.114E-06	1.222E-
13.00	4.839E+06	1.64CE+06	5 . 2L 8E+05		.1499	107667.5	1392.C	82835.8	27 30 3. 0	11707.9	4. C64E-06	1.224E-1
15.00	4.735E+36	1.59E+06	5.586E+05	5 .4658	1593	103852.6	1620.7	81239.2	26977.3	12444.1	4.010E-06	1.225E-
16.00	4.534E+06	1.57 2E+06	6.396E+05		.1863	96252.5	2135.6		26258.6	13989.3	3.89CE-06	1.228E-
17.00	4.378E+06	1.547E+06	6.824E+05		.1920	92 458.2	2422.6		25866.7	14792.3	3.823E-06	1.229E-
19.00	4.13FF+CF	1.4935+06	7 - 71 LE+05		2176	84 985.3	2050-0	71359.3	25.221.2	16443.9	3.6775-06	1.232E-
20.02	3.961E+06	1.4645.06			.2316	81339.8	3408.4	69025.	24569.6	17286.3	3.599E-06	1.233E-(
21.00	3.810E+66	1.434E+06	8.635E+05		.2464	77 77 2.4	3760.7	66586.	24100.1	16135.4	3.517E-06	1.233E-
23.60	3.496E+66	1.3715+06	9.5696+05		.2783	70916.2	4175.9	61432	23113.6	19841-1	3.3435-06	1.233E-
24.00	3.335E+06	1.3396+06	1.004E+06		. 2955	67 629.1	5030.2	58742	22599.9	20690-9	3.253E-06	1.232E-
25.00	3.171E+06	1. 30 5E+06	1.05CE+06		.3135	64454.4	5507.0		22075.4	21534.1	3.162E-06	1.230E-
27.00	2.841E+06	1.23 85+06	1.096E+06	. 8078	.3523	58433.6	6524.5	53215.1	21004-0	23367.0	2.982E-36	1.223E-
28.00	2.678E+06	1.2032+06	1.18 5E+0		.3721	55589.5	7075.1	47611.	20463.1	23988.0	2.896E-36	1.217E-
30.00	2.360E+06	1.1365+06	1.269E+06		. 3932	50231.8	8265.7	44831.5	19389.2	25524.6	2.745E-06	1.201E-
31.00	2.23 7E+06	1.10 3E+06	1.30 8E+0		.4374	47715.1	8968.1		18864.9	26252.0	2.686E-06	1.1895-
32.00	2.050E+66	1.0405+06	1 . 346E+06	6 . 8861	. 4665	45363.8	9583.7	36827 . 4	18355.7	256947.5	2.643E-06	1.174E-
34.00	1.786E+CE	1. G10E+06	1.416E+0	•	. 50 84	40786.1	11039.7		17406.3	28228.5	2.628E-06	1.1345-
35.00	1.6616+06	9.8326+05	1.44.7E+C6	•	. 5331	38673.8	11823.3	29745		28837.3	2.668E-06	1.109E-
37.00	1.439E+06	9.3696+15	1.502E+06	•	.5834	36725.7	13509.7		16259.6	29825.6	2.8755-16	1. P. 6. 2E -
38.00	1.342E+06	9.188E+35	526E+0	•	. 6089	32 86 3.4	14416.2	23997.	15984.0	30261.5	3.656E-06	1.0015-
30.65	1.255E+Ub	8.950F+05	546E+0	66.89	. 6344	31124.2	15367.5	22421.6	15777.0	30643.4	3.290E-75	9.0516-
41.00	1.111E+06	8. 90 6E+05	1.5785+06	• •	.6850	27842.3	17412.4	19796.6	15616.0	31239.9	3.977E-06	8.487E-
42.00	1.053E+06	8.919E+05	589E+0	•	2002.	26313.0	18516.5	18744.5		31451.3	0	7.898E-
43.00		8.996E+05	1.597E+0	•	.7339	24.653.9	19662.2	17860-1	15843.9	31603.2	4.914E-36	7.286E-
15.00	9.3646+85	9.3646+65	1.6046+06	4622. 9	.7795	22134.3	22136.4	16565.7	16566.5	31725.1	6.053E-06	6.353E-

			AY	4.701E-05	4.699E-05	4.693E-05	4.684E-05	4.0/1E-05	4.633E-05	4.509E-05	4.583E-05	4.6116-05	4.473E-05	4.424E-05	4.374E-05	4. 323E-05	4.261E-05	4. 129F-P5	4. (55E-05	3.976E-05	3.892E-15	3. 80 SE-15	3. / USE - US	3.503E-05	3.3935-15	3.2775-05	3.331E-05	2.991E-05	2.7665-35	2.4856-05	2.3436-35	2.192E-35	2.0475-05	1.6925-05	1.5016-05	1.4625-35	1.295E-05	1.1536-05	1.013E-35	8.792E-76	6.289E-06	
			A×	3.5596-96	3.548E-06	3.515E-06	3.460E-06	3.284F-06	3.164E-06	3.C24E-C6	2.864E-06	2.488F-16	2.273E-06	2.043E-06	1.798E-06	1.540E-66	1.2/CE-Ub	7.6675-07	4.17CE-07	1.256E-07	-1.642E-D7	-4.492E-07	-0.8026-07	-1.236E-06	-1.461E-06	-1.659E-06	-1.955E-06	-2.042E-06	-2.080E-0F	-1.9865-66	-1.843E-06	-1.629E-C6	-1.339E-06	-9.6885-07	2.7 455-08	6.581E-07	1.3795-06	2.193E-0E	3.0895-06	4.075E-0E	6.291E-06	
			FXY	1305.9	1382.5	1461.3	1548.5	1766.8	1854.9	1973.7	2101.6	2386.7	2544.8	2713.5	2893.2	3084.6	3265.6	3721.B	3955.4	4198.4	4450.2	2000	5247.3	5522.4	5799.7	6077.3		6893.7								6913.3		9113.3			9274.6	
	ROPERTIES		FYCU	1864.6	1864.2	1864.9	1866.0	1869.5	1872.6	1875.1	1878.6	1887.6	1893.1	1899.3	1906.3	;	1923.1	19461	1956.4	1970.1	1985.4	2002	2041.9	2065.0	3036.6	2118.9	2185.0	2223.4	2265.6	2364.7	2422.1	2485.6	2555.7	2633.2	2811.6	2918-1	3033.6	3161.2	330 2.1	3457.3	3817.6	
	COMPOSITE PROPERTIES	RHO# .0164 FTU# 162500.0 FCU# 107500.0 FSU# 6300.0	FXCU	26875.0	26858.1	26807.2	26721.4	26639.3	26239.0	25996.1	25708.0	24985.7	24547.2	24055.0	23508.5	22908.0	24 65 2 4	20803.1	20013.8	19189.8	18338.6	17466.1	16700.7	14823.7	13958.3	13113.1	11506.4	10754.0	10039.9	930000	8143.0	7593.5	1084.4	6614.3	6784.1	5420.0	5087.2	4783.4	4506.5	4524.5	3817.3	
			FYTU	•	2.0		18.0	0.00	72.1	98.4	128.8	202.4	245.7	293.5	345.7	402.7	****	662.5	679.2	761.2	9.8.6	7.10	10.00	1256.6	1374.5	1498.9	1769.1	1915.5	2069.8	26026.5	2583.7	2773.4	2973.0	3183.0	2646.2	3880.6	4137.5	4407.7	4691.8	9.0664	5304.8	
		ER # 4.760E+05	FXTU	40625.0	40548.3	40 31 9.7	39943.8	38781.7	38017.2	37147.4	36186.7	34651.6	32904.9	31 724.7	30 522.9	29 316 - 7	1.06.002	25765.3	24538.5	23398.6	22289.4	241212	601107	18269.9	17285.5	16399.8	14742.9	13976.2	13233.4	11 862.6	11 22 6.1	10626.4	10044.3	9496.5	0.000	8009.6	7562.3	7136.6	6732.2	6347.7	5 634.7	
	RTIES		X	.0199	. 0 20 1	.0210	*220	. 0268	. 0299	.0335	.0377	6240	.0539	.0665	.0677	.0755		11011	1136	.1249	.1369	1641.	. 1033	.1928	. 2088	. 2258	. 2 623	.2821	.3028	3642	3711	.3961	. 4222	***	25.70	5382	.5762	.6034	.6378	.6734	.7478	
	RESIN PROPERTIES	VR = .5000 WR = .3140 RHORE : 0412 FSU = .0000	UXA	.2850	.2887	.2999	. 3183	3763	.4153	. 4603	.5110	6266	.6895	.7551	.8223	. 6693	1666.	1.0415	1.1388	1.1909	1.2371	1.2766	1.3092	1.3520	1.3622	1.3653	1.3514	1.3355	1.3144	1.2500	1.2264	1.1908	1.1531	1.1138	1.07.04	9066	6946.	.9075	.8665	.8261	747	
	RES		GXV	6.578E+04	6.621E+04	6.752E+04	5 - 96 8E+04	7.6555+04	8.122E+04	8.669E+04	9.292E+04	1.076F+05	0	1.249E+05	1.344E+05	1.445E+05	1.5512405	1.7755+65	1.892E+05	2.012E+05	2.134E+05	2.25 BE+U5	2.56 75405	2.631E+05	.755E+C	2.877E+05	3.114E+85	.227E+0	.338E+0	544640	3.640E+05	3.729E+05	3.813E+05	3.890E+05	4 .022E+05	4.976E+05	4.123E+05	4.162E+05	4.192E+05	4.213E+05	4.231E+05	
PASEMINO- TIO = .250		EFT = 1.260E+07 EFT = 1.260E+67 6F = 4.000E+05 AFT = 2.200E-06 AFT = 2.200E-06	£	1.139E+05	1.1396+05	1.1406+05	1. 14 CE+05	1.14.25+05	1.144E+05	1.1465+05	1.148E+05	1.1536+05	1. 156E+05	1.1602+05	1.164E+05	1. 16 9E+05	101745405	1.186F+05	1.19 JE+05	1.2015+05	1.2105+05	10 26 15 4 45	1.2446405	1.258E+05	1.27 35+45	1. 29 SE+05	1.3296+05	1. 352E+35	1. 37 7E+05	1.4465405	1.47 CE+05	1.508E+05	1.549E+05	1.595E+05	1.7035+05	1.765E+05	1,8345+05	1.909E+05	1,9936+05	2. 38 5E+05	2.299E+05	
S GLASS/EPOXY -SP.	PROPERTIES	.5000 .6866 .0900 325006.0 215900.0	×	1.634E+06	1.633€+06	1.629E+06	1.623E+06	1.6045+66	1.591E+06	1.575E+0E	1.556E+06	1.5095+06	3	1.449€+66	1.4146+66	3	1. 5555 + 65	1.2455+06	1.196E+06	1.14 95+06	1.694E+06	1.0412+06	9.07 /2+05	8.819E+05	8.3036+05	7.799E+05	6.8466+65	6.430E+65	5.978E+05	5.2366436	4. 85 7E+05	**533E+05	4.232E+65	3.9546+05	3.654F+05	3.24 BE+05	3.051E+05	2.872E+05	2.708E+05	2.558E+05	2.299E+05	
FIBER	FIBER	PART DE DE LE CONTRE LE CO	ALPHA	0.00	1.00	2.00	3.00		00.9	7.00	8.00	10.01	11.00	12.00	13.00	14.00	15.00	17.00	18.00	19.00	20.60	22.00	200.22	24.00	25.00	26.00	28.00	29.00	30.00	32.00	33.00	34.00	35.00	35.00	38.00	39.00	20.04	41.00	42.00	43.00	45.00	

			AY	3.134E-05	3.133E-05	3-1295-05	3.125E-05	3.120E-05	3.114E-05	3.107E-05	3.098E-35	3.1765-05	3. 16 3F - 0 5	3.3485-05	3.032E-05	3.0135-05	2.992E-35	2.969E-35	2.9435-05	2.884F-C5	2.850E-C5	2. #12E-05	2.771E-05	2.7256-05	2.622E-55	2.563E-05	2.500E-05	2.4315-05	2.275E-05	2.191E-05	2. 199E-05	Z. 25.25.2	1.7925-05	1.683E-05	1. 5635-35	1. 444E-65	1.322E-05	1.1985-05	1. 57 5F - US		7.165E-05	54E-0
			AX	3.5596-06	3.552E-05	3. 495F-06	3.446E-06	3.382E-06	3.305E-06	3.213E-06	3.106E-06	2. 4585-05	2.7135-06	2.556E-06	2.386E-36	2.206E-06	2.0146-96	1.813E-06	1.603E-06	1.16:5-06	9.334E-07	7.031E-97	4.730E-37	2.458E-07	-1.866F-07	-3.841E-07	-5.629E-07	-7.18:E-97	-9.339E-C7	-9.819E-17	-9.807E-07	-9.235-07	-6-125E-07	-3.421E-97	9.64CE-19	4.4946-07	9.807E-07	1.605E-06	2.324E-75	4.0795-66	5.007E-26	6. CSEE-26
			FXY	1972.8	2081.7	2331.6	2474.4	2630.3	2800.1	2984.5	3184.2	3631.6	388	10	4427.1	4725.4	5039.7	5369.4	5713.7	5441.7	6822.8	7213.1	7610.9	8014.2					10823.2								13373.8	13536.7	13671.6	13851.4	13896.8	13911.9
	ROPERTIES	969	FYCU	4184.1	4183.6	4182.1	4176.1	4171.6	9	6	4152.B	• 4	3		4106.7	9.9604	4285.1	4074.1	4063.2	4042.5	4033.1	;	4011.4	4011.6	7.0004	4038.5	4013.5	402204	4035.8	4079.3	411101	4150.9	1259.0	4329.6	4413.5	4512.2	4627.4	4761.3	4915.9	5296.9	5528.7	5791.8
	COMPOSITE PROPERTIES	RHO= .0246 FTU= 162500.0 FCU= 107500.0 FSU= 8000.0	FXCU	40312.5		40684.0	3990 3. 8	39668.9		-	38612.3		36971.1	36282.3	35519.9	34 66 3.4	33773.5	32792.2	31742.7	29.66	28241.6	26983.0	25694.7	24387.8	21763.8	20469.6	19201.6	17969.4	15644.7	14565.0	13546.3	12591.6	10878.3	10119.3	9423.7	8789.0	8212.7	7691.4	68000 7	6424.2	6.88.9	5791.3
	5		FYTU	9.	3.6	12.0	6.7.	75.0	138.2	147.6	193.2	3.5.75	36.8.6	460.2	518.6	9.4.19	6969	796.4	963.7	1161.7	1272.9	1412.6	1560.9	1718.4	2061.7	2248.4	2445.6	2653.7	3144.6	3348.5	3605.3	3875.6	4 150 . 6	4774.6	5165.9	2454.4	5820.8	6216.2	6611.5	7485.8	7957.1	8+52.8
		ER = 4.700E-05 AR = 4.000E-05 UR = .3560	FXTU	60937.5	60 822.4	5994 6.5	59141.8	58172.6	57025.8	55 721.2	54286.1	5.076.6	10367	47587.0	45784.3	43966.3	42147.2	40 341.6	38557.9	35 67.8	33434.2	31821.2	30 262.4	28759.8	25 92 8.2	24599.7	23328.7	22114.4	19850.3	18796.8	17793.8	1563941	15930.0	14244.8	13463.4	12724.6	12014.4	11 34 3, 1	10754.9	9621.6	8973.3	6452.
	ERTIES		VAN	.0298	.0301	01310	946	.0370	.0402	.0439	.0463	2000	2000	0718	.0793	+180.	. 1962	.1657	.1159	1185	.1569	.1640	.1780	.1928	1992	.2422	.2615	.2797	3263	3648.	.3661	. 3963	.4154	7694	. 4973	.5267	.5571	.5865	. 6219	5864	.7233	.7568
	RESIN PROPERTIES	WR = .5000 WR = .3140 RHOR= .0412 FSU = .8000	UXA	.2850	.2876	5662.	. 3258	.3484	.3757	. 4075	. 4435		2725	6226					.8847						1.1861	1.2912			1.2054		1.1769		1.1325					•				•
	œ		4×9		9.933E+0+	1.013E+65	1.0936+05	1.152E+05	1.223E+85	1.36 7E+05	1.4C2E+05	1.5035405	1.754641.5		2.038E+05	2.192E+05	2.354E+05	2.523E+65	2.697E+05	1.0605405	3.247E+05	3.4366+05	3.626E+05	3.817E+05	4.30 FEFUS	4.384E+05	4.567E+05	4.7462+05	5.089F+05	5.251E+05	5.466E+05	5.55 ZE+05	5.847E+05	5.935E+05	6.0415+05	6.137E+05	6.221E+05	6.292E+05	6.351E+05	6.4705405	6 -450E+05	6.457E+05
PACEMINO- TIO = .375		EFT = 1.250E+07 EFT = 1.250E+07 6F = 4.400E+05 AFT = 2.200E-06 AFT = 2.200E-06	£.4	2.563E+05	2.563E+05	2.562E+05	2.5585+05	2.5555+35	2.5515+35	2.547E+05	2.5425+05	2 55 75 4 15	2012760	2. 51 95 + 15	2.5125+05	2.5052+05	2.4975+05	2.49 CE+05	2.4835+35	2.46.85 +05	2.4625+45	2.4556+05	2.4505+35	2.446E+35	2.46(5405	2.44.05+05	2. 44 2E+05	2.446E+05	2.4525405	2.4765+05	2.493E+05	2. 51 55 + 05	2.543E+05	2.617E+05	2.6665+05	2. 7235+35	2.790E+35	2.8682+05	2. 95 8E+05	2 18 15 40 F	3. 31 75+05	3.4715+05
COVERAGE RAT	PROPERTIES	.6850 325000.0 215000.0	EX	2.4515+06	2.4+9E+66	2.4446+06	2. 42 JE + 06	2.437E+06	2.387E+66	2.364E+06	2.336E+06	2 36 95 436	2. 22.85 4.66	2.18 TF + 6.F	2.1346+36	2.3805+46	2.023E+C6	1.961E+66	1.895E+36	1.75 15 + 06	1.67 8E+C6	1.632E+06	1.5236+06	1.445E+06	1.385E+UE	1.21 F+ 66	1.135E+06	1.062E+0F	9.917E+65	8. £12E+05	8.014E+65	7.454E+65	6.9335+65	6.0355+05	5.598E+05	5.22 EE+65	4.889E+05	4.584E+05	4.379E+65	3.8415+05	3.6452+05	3.4.06+65
FIBER C	FIBER	A MARKATON DE LA CONTRACTOR DE LA CONTRA	AL PHA																										30.05													

			*4	2.353E-05	2.357E-05	2.350E-05	2.349E-05	2.348E-35	2.34.55-35	20-30-72 6	201100100	2.3475-05	2.333E-05	2. 328F+05	2.323E-05	2.318E-05	2.3115+05	2.3r3E-05	2.2945-05	2.284E-15	2.272E-05	2.25 3E-US	2.226Fe 05	2.207E-05	2.185E-05	2.161E-05	2.131E-05	2.043E-05	2.0235-05	1.9785-05	1.9285-05	1.873E-05	1.6125-05	6 674F-05	4. RG 25-05	1.506F=05	1.4155-05	1.3185+05	1.217E-05	1,1135-05	1.0005-05	8.978E-06	7.905E-05	6.853E=36	5.840E=05
			AX	3.5595-06	3.5546-06	3.5395-06	3.5136-06	3.478E-05	3.432E-16	3 3005-06	20225-00	7.146F-06	3.0495-05	2.9435-06	2.826E-36	2.699E-06	2.563E-36	2.418E-05	2.264E-06	2.102E-06	1.931E-CE	1.7545-06	1.37725-00	1.1946-06	1.002E-06	8.115E-07	6.247E-07	4.45(E-97	1.22CE+07	-1.176E-08	-1.197E-37	-1.955E-37	-2.3225-37	10-00-00	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.6955-07	404565107	8.076E-07	1.259E-06	1.8048-06	2.44.2E-06	3.172E-06	3.988E-06	4.882E-06	5.842E-06
			FXY																						6808.5			12410-1																	
	PROPERTIES	0.00	FYCU	CI	7420.6	7415.2	40	7393.8	7377.8	722000	10000	1.0102	7246.8			7130.3		8	6	å	;		+ 1		'n		S	6459.7	M	S		å	· .	4 4		9 4	0	٤	m	ò	on on	e,	10	ci	60
	COMPOSITE PE	RHO= .0328 FTU= 162530. FCU= 107500. FSU= 8665.	FXCU		53716.5	.0			52900.4	٠.	•											39833.5		34967.5		31525.6	29765.9	28053.0	24665.1	23036.7	21467.6	19967.9	18545.4	Trenen a	100000	18/200	12747.5	11850.2	11055.1	1033405	9692.2	9123.4	8 52 3 . 1	8186.2	7697.7
	Ö	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	FYTU	9.	4.6	16.6	35.9	63.9	100.0	1000	19000	200	454.9	7 404	586.9	691.5	805.4	928.7	1061.8	1204.9	1358.3	1522.3	1697.2	2003.4	2291.2	2513.6	27.49.0	2997.9	25.00	3831.0	4139.5	446406	4807.5	2106.5	00000	2000	6 80 7 . B	7070.6	7761.1	8275.0	8615.3	9363.5	9961.1	0 80 9	11270.6
		ER = 4.700	FXTU	25	81096.6	63	79887.5	78 855.7	77563.5	****	٠.	76363.5	68402.4	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	63449	61645.7	58621.4	56196.2	53787.7	51416.5	49077.0	46797.1	44578.9	4.034.24	38346.4	36419.3	34571.0	32799.6	204.85.8	27 940.5	26466.8	25062.5	23725.1	1,24,52	5000000	0000000	47054.2	46.06.04	16019.2	15124.1	14273.2	1366404	12695.4	11964.4	11269.3
	TIES	e.	UYX	7950.	0340.	6340.	.0424	6449	.0472	* 020 *	54000	0000	2090		0832	6 160	.0993	.1084	.1182	.1287	.1399	.1519	.1647	1026	02078	. 2238	1342.	. 2585	2000	.3172	.3387	.3611	3.00.5	6004.	つまつかっ	0 2 0 0 0 0	0 4040	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5755	6000	6376	96999	,7024	. 7355	.7695
	RESIN PROPERTIE	R = .5000 IR = .3140 HOR= .0412 SU = 8000	UXA																									1.0884																	
	RES	260E+07 WR 260E+07 WR 110E+65 RH(260E-06 FS(GX¥	1.3165+05	1.3256+05	1.352E+05	1.397E+05	1.460E+U5	1.540E+05	1.637 2+65	1.751E+05	1.881E+05	2 4 9 5 6 4 0 5	C013001.2	2 54 76 405	2.746.405	2.456E+05	3.17 6E+05	3.4052+05	3.643E+05	3.887E+05	4.136E+05	4.391E+05	4 * 04 95 4 5 5	5.167 F+115	5.426E+05	5.683E+05	5.937E+05	6 434545	6.668E+05	6.897E+05	7.118E+05	7 . 32 8E+05	7.527E+85	7 . 713E+05	7.887E+U5	6 - U4 / E+ U5	0 122C 10	8 - 47 A F + D B	A 1775405	8 - 51 kF + 0.5	8.6775405	8 .722E+05	8.749E+05	8.758E+05
PASEWIND- TIO = .500		EFT = 1.26 GF = 4.06 AFT = 2.26	¥ 3	4.5575+05	4.555E+05	4.552E+05	4. 54 6E+05	4.5382+65	4.528E+35	4.515E+05	4. 50 1E+35	4.4841465	** ** ** **	1000	4.42054.4	1 16 PE 4 75	4. 3405+05	4.3095+05	4. 27 7E+uS	4.2442+05	4.213E+05	4. 17 4E+05	4.1385+05	4. 10 15 + U5	1.027F+05	3.9902+05	3.9542+65	3,919E+05	200000000000000000000000000000000000000	3.8265+05	3.80 2E+05	3. 781E+05	3.7665+05	3,7575405	3.756E+05	3.752E+05	3.77 9E+05	2000000	2 00 4 1 4 10 5	1.97 2F 405	4.06.25.90.5	4. 17 3E+05	4.307E+05	4.457E+05	4.654E+05
SSZEPOXY -SP	PROPERTIES	.5000 .0906 32506.0 21506.0	×		2	9	0	0	4		3	3	3 (3 0	36	3 0	9 3	0	.3	C	O	0	.31	3 4	3 6	3	(3	1.650E+06	3 (3 0	C	9	0	0	ω,	9	0, 0	3 0	36	3 6	2 0	, 0	C	-	4.654E+05
S GLA FIBER	c36I4	RHOF==	ALPHA																																										72.00

FIBER	PROPERTIES		•	RESIN PROPE	PROPERTIES			COMPOSITE !	PROPERTIES			
A TARENTAL	.5336 .6860 .0900 325300.6 215300.6	EFT = 1.260E GF = 4.060E AF = 2.20E AFT = 2.20E	7669	WR = .5680 WR = .3140 RHOR= .8412 FSU = .8600		ER = 4.700E+65 AR = 4.666E-69 UR = .3506		RHO= .C410 FTU= 162500.0 FCU= 16750.0 FSU= 6919.3	030			
AL PHA	EX	£¥	GXY	UXA	X AO	FXTU	FYTU	FXCU	FYCU	FXY	AX	A
0.00	4.084E+66	7.12uE+65	644E+0	•	1640.	101562.5	•	67187.5	11574.5	3332.8	3.559E-16	1. P. 1. E.
1.00	4.082E+66	7. 11 7E+05	556E+0	•	.0560	101 376.7	5.0	67145.9	11576.9	3505.5	3.555E-06	1.884E-0
30.5	4.058E+06	7. 19 9E+05	1.748E+05	2998	. 1524	3.66,001	6.44	66811.4	11561.6	3916.2	3.524E-06	1.88CE-0
4.05	4.0385+66	7. CB 2E+05	328E+8	•	.0546	96569.6	6.62	66516.3	11516.4	4157.8	3.497E-36	1.980E-3
20.6	4.012E+06	7. 06 1E+05	31E+0	•	.0573	96954.3	125.0	66133.8	11483.8	4425.7	3.462E-06	1.889E-0
7.00	3.9416+06	7. 30 SE+05	DO DE + D		1990	92868.6	246.6		11397.3	2044.6	3.368E-36	1.880E-9
9.00	3.897E+06	6.9716+35	165E+0	•	1690.	6.99406	322.0		11343.4	5397.6	3.3096-06	1.8796-0
8.6	3.846E+06	6.9315+05	551E+0	•	.0747	87 87 4.3	108.7	63679.1	11282.6	5778.5	3.242E-96	1.8798-0
11.00	3.7246+06	6.84[E+05	376E+0	• •	. 0872	62262.2	614.3		11146.6	6627.8	3.LA4E-96	1.877E-0
12.06	3.654E+0E	6.788E+65	14E+0	•	960.	79311.7	733.6	60786.3	11059.7	1.4607	2.993E-06	1.876E-0
	3.57 EE+06	6. 732E+05	3.468E+05	•	.1025	76 30 7-1	964.4			7587.8	2.894E-06	1.874E-0
	3.4925+66	6.671E+05	36E+0	. 5516	1111	78276.7	1366.7	56319.0	10878.8	8106.6	2.787E-36	1.8735-0
	3.305E+06	6.539E+05	4.369E+05	•	1366	67234.6	1327.3		10674.1	9214.6	2.549E-06	1.8675-0
	3.232E+66	6.4685+05	4.612E+09	•	.1616	64 263.1	1506.2	53798.6	10563.5	9600.1	2.4196-06	1.864E-0
	3.093E+06	6.394E+65	4.923E+65	•	.1530	61346.2	1697.9	52082	10447.8	10403.9	2.282E-06	1.8598-0
20.00	2.861E+06	6. 236F+05	5.565E+05	•	1784	55723.6	1962.9	50209.	10203.0	11657.5	1.9896-06	1.8476-0
21.00	2.739€+06	6.153E+05	5.893E+05	•	.1924	53035.4	2354.3	46388	10074.9	12362.4	1.834E-06	1.840E-0
22.00	2.613E+06	6. 369E+05	24E+0	•	.2071	50437.3	2601.6	44342	9943.8	12955.6	1.675E-06	1.931E-0
24.00	2.485E+66	5.98 3E+05	355E+0	• •	. 2327	47933.1	3142.0	42242.	9810.4	13614.5	1.5135-06	1.819E-0
25.00	2.22 EE+06	5.808E+05	13E+0		.2564	43213.7	3436.2	37 9.8.	9540.1	14937.1	1.187E-06	1.791E-6
25.00	2.09 6E+66	5.72(E+05	7.537E+05	1.0061	.2745	40999.5	3747.4	35786.9	9405.2	15594.5	1.027E-96	1.77.36-0
28.00	1.8435+06	5.549E+05	67E+0	: ::	.3135	36857.3	4422.8	31522	9141.6	16885.0	7.297E-07	1.729E-0
29.60	1.721E+06	5.467E+65	69E+0		.3344	34 92 5.6	4788.7	29454.	9015.9	17511.3	5.997E-07	1.701E-0
30.00	1. 50 4E+06	5. 38 9E+05	162E+0		.3562	33683.5	5174.4		8896.5	18120.4	4. 886E -07	1.6685-0
32.00	1.384E+66	5.248E+05	31 0E+0		.4025	29656.4	6:08.8	23688.	8684.3	19273.3	3.47CE-07	1. 589E-0
33.00	1.283E+06	5.188E+05	264E+0	÷	.4271	28165.1	6459.3	21953.	8596.2	19810.4	3.363E-07	1.5425-0
34.00	1.188E+06	5. 138E+05	30 2E + D		. 4525	26 551.1	6933.6	20327.	8523.6	26317.2	3.6C2E-07	1.488E-1
36.00	1.0206+66	5.072E+05	123E+0		.5061	23741.3	7957.6	17419	8637.3	21227.6	5.937F-07	1.362E-1
37.00	9.461E+05	5. 061E+05	.041E+0	9866	. 5341	22439.6	8519.8		8430.6	21625.8	8.1465-07	1.289E-0
39.00	8.793E+05	5. 067E+05	1.058E+06	•	. 5629	21200.9	90006	14986.	8453.6	21982.9	1.115E-06	1.211E-0
20.64	7.657E+05	5. 14 35 405	1.07 2E+06	•	6263	10024.0	9701.4	13944	8516.6	22296.7	1.5025-06	1.126E-0
41.00	7-184E+05	F. 21 9F + 05	1.09 SF + 0.6	•	6531	17841.5	11019.1	12194	8746.7	22787.2	2 . 549F-06	9-4-395-0
42.00	6.770E+05	5. 32 3E+05	1.10 3E+06	•	.6641	16630.4	11729.4	11475	9936.6	22961.2	3.267E-06	100
43.00	6. 41 2E +05	5.461E+05	1.109E+06	•	.7155	15869.3	12476.4		9182.3	23086.1	3.950E-06	7.522E-0
00.44	6.10 EE+05	5.635E+05	1.112E+06	•	.7469	14 955.5	13251.9	10317.7	9.0646	23161.4	4.767E-06	6.569E-0
20.00	20000000	20035182	1.113578	•	+0110	1+000+1	1 +000 •	966	20000	2310002	20000-000	20000

r 18EK	COVERAGE	067. = 01TA										
FIBER	PROPERTIES			RESIN PROP	PROPERTIES			COMPOSITE	PROPERTIES			
ARE STANDER IN THE ST		EFT = 1.26 GF = 4.00 AFT = 2.20 AFT = 2.20	1.260E-07 1.260E-07 4.000E-05 2.200E-06 2.200E-06	VR = .5000. WR = .3140 RHOR= .0412 FSU = .0000	9.000	ER = 4.760E+09 AR = 4.900E-09 UR = .3500	10.10	RHO= .0492 FTU= 162500.0 FCU= 107500.0 FSU= 6000.0	999			
AL PHA	¥	Ę	6XY	UXA	XAO	FXTU	FYTU	FXCU	FYCU	FXY	AX	AY
90.0	4.901E+06	02 5E	.973E+0			121875.0	•	80625.0	16637.5	4025.6	3.5596-06	1.567E-05
1.00	4.898E+06	1.025E+06	1.967E+0			121644.9	0.9		16631.5	4228.2	3.556E-06	567E-0
2.00	** 887E+66	1.624E+06	2.030E+0			120959.1	23.9	80426.	16613.4	4458.1	3.547E-06	1.567E-05
	4.846E+46	1.019E+06	2.198E+0			118283.6	6.00	79824	16540.9	5009.8	3.510F-06	1.568E-05
2.00	4.815E+06	1.015E+06	2.323E+05			116345.2	150.0		16486.6	5335.3	3.482E-06	
9.00	4.776E+06	1.0115+06	2.475E+0			114051.5	216.4	78808.	16420.4	5695.7	3.447E-06	1.569E-05
	4.677E+06	1. 00 0E+06	2.856E+0			108560.2	386.4	77357	16252.3	6523.7	3.3665-66	
9.00	4.617E+06	9. 937E+05	3.082E+05			105 449.2	7.064	76461.	16156.7	6991.3	3.366E-66	1.573E-05
10.00	4.548E+06	9.864E+05	3.332E+0			102153.1	607.2	75448.	16037.4	7493.9	3.246E-06	1.571E-05
12.00	4.473E+66	9. 78 35 + 65	3.50.32+0			98714.6	737.1	74314.4	15912.6	8030.6	3.179E-06	1.5726-05
13.00	4.298E+06	9. 60 CE+65	4.205E+0			91 568.6	1037.2	71675	15629.4	9200.6	3.026E-06	1.57 3E-05
14.00	4.199E+06	9.4985+05	4.533E+0			332.	1208.6	70166.3	15471.3	9830.5	2.9396-36	1.5736-35
15.00	4.092E+06	9.389E+05	4.877E+0			84294.4	1393.1	69529.6	15302.7	10487.6	2.8465-06	1.573E-05
16.00	3.978E+06	9.27.36+05	5 . 234E+0			50 661.5	1592.7	66766.8	15123.8	11169.9	2.746E-06	1.5736-05
18.00	3.729€+06	9. 0235+05	5.965E+0			73615.5	2037.5	62872.4	14737.	12600.2	2.527E-06	1.571E-05
19.00	3.595E+06	8.890E+05	6.375E+0			70195.7	2283.5	60750.6	14536.6	13343.1	2.408E-06	1.573E-05
20.00	3.4556+06	8.751E+05	6.771E+0			65868.3	2545.8	58522.4	14314.7	14100.8	2.283E-06	1.568E-05
22.00	3.162E+06	8.4605+05	7.577E+0			60524.8	3121.9	53789.1	13862.5	15649.0	2. 619E-06	1.561E-95
23.00	3.010E+06	8.30 8E+05	7.982E+0			57 51 9.7	3436.8	51310.9	13627.2	16433.3	1.881E-06	1. 556E-35
24.00	2.856E+06	8.153E+05	8.387E+0			54 62 9.8	3770.4	48779.5	13387.3	17 220 .0	1.74CE-06	1.553E-05
26.00	2.5465+06	7.839E+05	9.184E+0			51856.4	4123.5	46213.1	13144.0	18085-5	1.599E-06	1.5426-05
27.00	2.393E+06	7.68 CE+05	9.574E+0			46657.5	4891.2	41054.3	12653.2	19558.4	1.321E-06	1.52)E-05
28.60	2.241E+06	7.523E+05	9.955E+0			44228.9	5337.4	36502.9	12409.2	26318.3	1.190E-06	1.505E-35
30.00	1.95 CE+06	7. 21 62+05	1.06 8E+06		3733	39760-1	6209.3	33558.2	11934.7	21785.2	9.6056-07	1.467E-05
31.66	1.813E+36	7.07CE+05	1.1C3E+0			37 593.7	6.9699	3126 3.1	11709.3	22484.4	8.719E-07	1.442E-05
32.00	1.557E+06	6.931E+05	1.135E+66	6 1.0192	. 4261	35587.7	7210.5	26948.9	11,495.7	23155.4	8.083E-07	1.412E-05
34.00	1.44 15+06	6. 68 3E+05	1.196E+0		•	31861.3	8320.3	24798.5	11118.1	24397.5	7.8435-07	1.339E-05
35.00	1.333E+06	6.57 8E+45	1.223E+0		•	30 133.0	8919.1	22923.4	10962.2	24961.4	8.399E-07	1.292E-05
35.00	1.233E+06	6. 49 1E+05	1.248E+06		•	26489.5	9549.1	21191.4	10834.3	25462.5	9.523E-07	1.2475-05
38.60	1.059E+06	6.37 9E+05	1.291E+0		•	25 441.1	10968.7	18169.7	10683.9	26384.0	1.3835-36	1.117E-15
39.00	9.852E+05	6. 3615+45	1.30 8E+0		•	24028.8	11641.7	16886.2	10673.3	26759.0	1.716E-06	1.046E-05
00.04	9.197E+45	6.3745+35			•	.999	12412.4	15735.1	10714.5	27080.2	2.136E-06	9.696E-05
42.00	8.125E+C5	6.5595+05	1 - 35 6E+0		• •	21459.8	13223.0	13857.4	10814.7	27545.7	2.644E-06	8.8835-05
43.00	7.700E+C5	6.6402+05			•	043	14971.7	13111.4	11223.7	27753.6	3.9166-06	7.172E-06
90.44	7.3456+65	6.8192+05	1.35 7E+06	6 .8159	•	4	15914.3	12483.6	11548.9	27793.7	4.663E-0E	6.309E-06
10.64	7.05 ZE+05	7. U5 3E+05	1 . 35 9E+D		•	:	16905.6	11965.5	11966.3	27823.8	5.467E-06	5.465E-36

					1.3436-05																																						5.300E-0	
			×A	3.5598-06	3.557E-06	3.5495:00	3.53/E=05	200000000000000000000000000000000000000	3.468E-06	3.435E-06	3.396E-06	3.352E-06	3.303E-06	3.248E-06	3.1005-00	3.1225.00	2.973E-06	2.8905-06	2.861E-06	2.707E-06	2.507E-06	2. 392F-06	2.277E-36	2.159E-06	2.0375-06	1.914E-06	1.668E-06	1.55LE-05	1.438E-06	1.2545-06	1.185F-06	1.1456-06	1,1385-05	1.1745-06	1.2595-06	1.404E-05	1.9665-06	2.276E-06	2.731E-06	3.269E-36	3.884E-36	4.567E-06	5.302E-06	
			FXY	4726.7	4.958.0	5223.5	22220	20000	667945	7149.3	7662.2	8217.2	8813.3	94480	10121.	10829.6	12341.9	13140.8	13964.6	14816.3	15675.1	16555.4	18352.1	19260.8	20171.5	21086.5	22877.1	23756.1	24616.4	25,655.0	0-09020	27780.4	28479.7	29133.8	29738.6	30290.5	31,000.0	34505.5	31904.5	32146.9	32321.1	32426.0	2461.	
	ROPERTIES	000	FYCU	22639.4	22630.4	22573.4	22528.3	2040200	22285.2	22156.4	22033.8	21881.6	2171108	21524.6	21326.2	21098.6	20606.3	20336.0	2005001	19749.4	19434.4	19105.9	18412.5	18049.7	17678.2	17299.6	1691507	16141.3	15756.1	15376.4	15053	14309.1	13992.7	13705.	13452.3	13241.6	13060.5	12940.6	12980.3	13106.2	13328.8	13658.9	14107.6	
	COMPOSITE PR	RHO= .0574 FTU= 162500. FCU= 107590. FSU= 8900.	FXCU	94062.5		93831.4	93541.6	902000	94957.7	91183.4	0282.	89250.2	:				82029.5	78164-1	75988.3	73695.0	71269.8	68720.7	645000	60444.2	57525.8	54558.3	51563.1	45581.2	42642.0	39768.7	36983.	31760.6	29357.3	271111.6	25033.6	23130.3	21405.5	1 20001	17007.8	16270.5	15402.5	14684.6	14106.7	
	O	E + 0 %	FYTU	8.	7.5	57.9	65.9	111.9	1/5.1	344	450.9	572.1	708.4	960.0	1027.1	1210.1	14(9.4	4858.2	2108.6	2377.1	2664.0	2970.1	36400	9.6104	4398.8	4810.7	5246.3	6192.0	6704.2	7244.1	7813.1	9063.1	9737.0	10405.7	11140.6	11913.7	12726.8	13501.9	14070	16421.2	17466.9	18566.7	19723.2	
		ER = 4.760 UR = 4.060	FXTU	142187.5	141919.0	141118.9	139803.2	137997.5	135736.1	1300001	126653.5	123024.1	119178.7	115167.1	111036.4	106836.3	102587.4	903838	899669	8588407	81895.0	78013.1	70 642 2	67106.3	63 734.8	2.66409	57 399.3	51 600 2	48895.8	46316.8	43859.3	19291.2	37171.5	35155,2	33237.8	31414.6	29 681.3	2003300	20.070	23562.6	22 217 . 9	20937.6	19721.3	
	RITES		NAN	9080	6690	61/0.	.0725	0 1 1 0 0	. 0777	9 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	. 0905	. 4961	.1624	.1094	.1171	.1256	01347	244	1667	.1789	.1919	.2057	225.0	. 2520	.2692	.2872	.3060	3464	.3678	.3962	. 4133	. 4573	.4876	.5139	.5408	.5682	. 5962	9479.	2550.	7168	7393	.7675	.7952	
	IN PROPER	3140 R3140 8000	UXY	2850	. 2862	.2900	. 2962	. 3049	3161	3630	3637	.3841	.4067	. 4 312	.4577	. 4859	. 5156	1000	6120	. 6456	.6795	.7133	1942	. 4186	4048	. 8683	8939	6416	.9539	.9674	.9775	1400	9863	. 9822	8416.	2496.	.9506	5456	9616.	8775	. 8476	.8219	1964	
	RESIN	E+07 WR = 15+05 RHOR= 16-06 FSU = 16-06	£ × 9		2,3195+15			2.570E+05	2.719E+05	2 4416405	3 45 25 40 F	3.621E+05	3.918E+05	4.241E+05	4.587E+05	4.957E+15	5.347E+05	5 . 7 5 5 5 6 10 5	6.621F+05	7.07 4E+05	7.538E+05		8.487E+05	0 450F+05	9.931E+05	1.0416+46	1.388E+06	1.1846406	1.224E+06	1.266E+06	1 . 30 7E+06	1.346E+06	1.4185+06	.450E+0	0480E+0	1.507E+06	1.531E+06	.552E+0	. 57 0E+0	1.5855405	- ACREAN	610E+0	611	
TIO = 0875		EFT = 1.2600 GF = 4.000 AF = 2.260	X 3	3055406	1.3955+16	1.3935+66	1.390E+06	1,386E+06	1. 38 1E+66	1, 3/ 45+06	1 25 25 40 6	1.3485+06	1.3375+36	1. 325E+36	1. 31 2E +G6	1.297E+06	1.282E+06	1,265E+36	1.2295416	1. 21 06+06	1.189E+06	1.168E+06	1.146E+06	1.100F+06	1. 07 6E+06	1.0516+06	1. C2 7E+06	1.0025405	9.522E+05	9. 27 85+35	9. 039E+05	8 80 9E + 05	4. 38 LF + 05	8.196E+05	8.029E+05	7.888E+05	7.776E+U5	7.699E+05	7.661E+05	7.669E+05	7.8446405	A. 01 9F + U.S	8.266E+05	
SS JEPOXY -SP COVERAGE RAT	(Jean	.5600 .0600 325000.0 .215000.0	K X		5.7146+16	5.732E+0E	5.682E+0€	5. 654E+06	5.617E+CE	5.572E+06	505196+05	5.38 7F+06	5.30 8E+06	5.221E+66	5,124E+06	5.019E+06	4.905E+06	4.782E+06	4. 651E+06	4.3655406	4.211E+66	4.351E+U6	3.884E+16	3.713E+UE	3.359E+06	3.179E+06	2.999E+06	2.820E+06	2.469E+66	2.306E+66	2.138E+06	1.982E+06	1.6355.466	1.567E+06	1.447E+06	1.338E+06	1.240E+06	1.152E+G6	1.074E+06	1.00 EE+06	8 08 0F 4 0F	A - 58 7F +05	8.265E+05	
FIBER	FIBER	WF WF RHOF FTU FCU FCU	AL PHA		1.00																		-									0		0		0	,			,		, ,		

FIBER	FIBER PROPERTIES		ď	RESIN PROPERTI	ERTIES			COMPOSITE	PROPERTIES			
TARRED DO L	. 5000 = .6000 = .0900 = 325000.0 = 215000.0	EFT = 1.260 GF = 4.000 AF = 2.200 AFT = 2.200	1.250E+07 II 1.260E+07 II 4.00E+05 R 2.200E-06 F 2.200E-06	VR = .5000 WR = .3140 RHOR= .0412 FSU = .0000	0.0 %0	ER = 4.700E-05 AR = 4.000E-09 UR = .350	E+05	RHO= .0656 FTU= 1625(0.0 FCU= 107500.0 FSU= 8003.0	906			
AL PHA	EX	ΕY	4×9	UXA	XAO	FXTU	FYTU	FXCU	FYCU	FXY	AX	AY
0.00	6.535E+06	1.823E+06	631E+0	•	.0795	162560.0	•	107500.0	29489.2	3	36E	1.175E-05
1.00	6.530E+06	1.822E+06	651E+0	•	0	162193.1	9.0		29476.7	5695.0	37E	1.175E-0
2.00	6.517E+06	1.819E+06	70 9E+0	5682.	.0808	161278.8	31.9	107237.2	29439.0	5995.5	31E	1.175E-0
	6.494E+66	1.815E+06	867E+0	•	.0825	159775-1	71.8	06907	29376.2	6341.0	9 0	1.175E-0
	6.461E+16	1. 80 9E+06	116640	• •	0 4 4 0	155126.9	2002	: .:	29175.4	7177	77	1.1776-0
9.00	6.369E+06	1. 7936+06	327E+0		.0916	152068.7	288.6	05109.	29037.5	7671.9	36	1.178E-0
	6.33 8E+C6	1.782E+36	573E+0		6360.	148589.8	393, 6	.:	28874.6	8216.8	36E	1.179E-0
00.0	6.238E+36	1.77 JE+36	3.854E+05	.3561	.1010	144747.0	515.3	163212.0	28686.8	8811.7	3.424E-06	1.180E-05
	6.153E+U6	1. /5 bE + Ub	1555+0	•	.1066	140296.9	0000	: .	204/402	1455.5	2 7 2	1.102E-U
1000	5. 96.9E+0.6	3 6	AA GE + D	• •	1266	131619.5	0.000	: :	27975.3	10880.6	100	1.1856-0
12.00	5.860E+06	1.7055+06	293E+0		.1284		1173.8	: :	27689.4	11657.3	50E	1.186E-0
13.00	5.741E+06	3	.723E+0		.1371		1363.0	:	27 37 9.4	12473.0	95	1.188E-0
14.00	5. 612E+06	1. 66 3E + 0 6	.177E+0	1464.	.1465	117242.7	1610.7	93909.0	27045.7	13324.9	3.134E-06	1.190E-0
15.00	5. 12 55 + 06	1.64 55 4 16	2	•	1676		2123.7			15124.7	ם מ	1 1945-
100	5 16 8 E 4 0 6	1. 50 95 106	043647	•	201.		5,6045	•	25906.7	16166.5	2 FF - 3	1 4 9 5 5 - 1
18.00	5.002E+66	1.561E+06	E+0	• •	1918		2716.7	84546.6		17032.0		1.197E-0
19.00	4.828E+06	1.5326+06	E+0	•	.2051		3344.6			18017.9	2.76uE-06	1.1995-0
20.00	4.646E+06	1.50 2E+06	9.279E+65	•	.2192		3394.4	78957.3	24574.3	19020.8	2.67CE-06	1.20CE-0
21.00	4.458E+06	1.471E+06	9.835E+05	•	.2341		3766.8	: .	٠.	20137.2	2.576E-36	1. 201E - 0
22.00	4.254E+16	1.4385+06	1.0435+06	•	9642.		4162.5		23591.1	22005.4	2.4/85-35	1.202E-U
24.00	3.8635+66	1.37 15+46	1.1525+06	• •	. 2840		5027.2	66333.5	22545.1	23129.7	2.271E-36	1.202E-0
25.00	3.659E+06	1.336E+06	1.207E+06	•	.3623		5498.0	62971.1		24161.6	2.163E-06	1.201E-0
26.00	3.4546+06	1.30 0E+06	1.262E+06	•	.3215	65599.1	5995.8		21452.2	25186.7	2.054E-0E	1.198E-0
30 00	3.2495+06	1.2645+06	A STOEFUG	•	.3415	6.67279	0.1260		:.	22400.5	1.946E-JB	1.1955-0
20.02	2.847E+06	1. 1925 + 06	1.4235+06	• •	3861	55886.9	7661.9	49372		28174.7	385-0	1.1836-0
30.00	2.653E+06	1. 157E+06	.47 0E+0		.4067	, ic	8279.0	46667.	19216.8	29125.1	0-3549	1.1745-05
31.00	2.465E+GE	1.1225+06	517E+0	•	. 4360		6	42852.	.:	30044.3	1.563E-96	1.1635-0
32.00	2.235E+0E	1. 987E+06	563E+0	•	.4541	4	96	39753.	18138.	30927.1	1.497E-06	1.148E-0
33.00	2.114E+66	1. 0555+06	. 60 6E+0		0624.	3	20	36794.		31768.6	. 453E-J	1.1295-0
200	1.9935406	1.0232+00		•	40040	\$ 3	7 0	33394		222	1,505	1. 1. 20E-1
36.00	1.663E+06	9.6815+05	-718E+C	• •	55573		27	28941	0	3 6 8	. 525E-0	
37.00	1.536E+06	9. 44 9E+05	. 750E+0	•	. 5844	35902.	361	26712.	č	4 62	.643E-0	1.208E-0
38.00	1.421E+06	9. 25 4E+05	1,77 8E+0		.6119		454	24691.	15639.3	35188.7	.824E-0	9.628E-0
30.6	1.319E+C6	9. 10 3E+05	1 . 8C 3E+0		.6397	32038.	22	22883.		5 68	. 075E-C	9.118E-
00.	1.2285+06	9. 00 1E+ 05	. 824E+3	•	.6676	30248	65	21287.	\$	611	. 402E-0	8.543E-0
1000	1.150E+06	8.956E+U5	. 841E+0		46954		17630.6	1990	15240.9	35453.5	2066-0	7 95 55-0
3 6	1 - 1 - 2 AF + 0 F	0.0646405	. 864F40		75.00	25 700	000			200	. A 5 5 5 1 1 2	6.9575-0
00.9	9.8335+05	9. 2326+05	. 87 GE+D		7769		21219.0	16921	* e	705	4.478E-06	5.848E-C
S		9.4862+05	. 872E+0	6 .8027	. 8327	2253	22540.9	16289.5	16290.4	37098.3	.1496-0	5.148E-0

##